

**TRAINING COURSE**

**ON**

**SOFTWARE FOR GROUNDWATER  
DATA MANAGEMENT**

**UNDER**

**WORLD BANK FUNDED HYDROLOGY PROJECT**

**LECTURE NOTES  
ON**

**GROUNDWATER  
MODELLING SOFTWARES  
(UNIT-4)**

**BY**

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# BLOCK LEVEL WATER BALANCE

## 1.0 INTRODUCTION

Some times it is required to carry out water balance of a block which may form part of a groundwater basin. Part of the block boundary may be comprised of (i) a river conforming to a constant head boundary, (ii) an impervious zone conforming to a no-flow boundary and (iii) a pervious zone conforming to a flow boundary. If the block happens to be at the central region of the groundwater basin it is possible to carry out water balance analytically considering the subsurface inflows and outflows.

## 2.0 METHODOLOGY

The aquifer is hydrologically decomposed into a number of circular zones as shown in Fig. 1. The centre of the each circle defines a local origin of a polar co-ordinate system. Let the radius of a circular zone be 'R'. Let 'i' be an abstraction point whose polar co-ordinates are  $(r_i, \theta_i)$ . The cumulative inflow to the aquifer from the adjacent area across the circle upto time 't' due to continuous withdrawal at unit rate at point 'i' is given by

$$K(r_i, \theta_i, R, t) = \int_0^{2\pi} \int_0^t \frac{R[R-r_i \cos(\theta_i-\theta)]}{2\pi[R^2 + r_i^2 - 2Rr_i \cos(\theta_i-\theta)]} \exp\left\{-\frac{R^2+r_i^2 - 2Rr_i \cos(\theta_i-\theta)}{4\beta\tau}\right\} d\tau d\theta \quad (1)$$

in which

$\beta = T/\phi$ , the hydraulic diffusivity of the aquifer,  
 $T =$  transmissivity of the aquifer, and  
 $\phi =$  storage coefficient.

Integrating with respect to  $\tau$

$$K(r_i, \theta_i, R, t) = \int_0^{2\pi} \frac{R[R-r_i \cos(\theta_i-\theta)]}{2\pi[R^2 + r_i^2 - 2Rr_i \cos(\theta_i-\theta)]} \left\{ t \exp(-C_i/t) - C_i E_1(C_i/t) \right\} d\theta \quad (2)$$

in which,

$$C_i = \frac{R^2 + r_i^2 - 2Rr_i \cos(\theta_i - \theta)}{4\beta}$$

$$E_i(C_i/t) = \int_{C_i/t}^{\infty} \frac{e^{-u}}{u} du = \text{an exponential integral.}$$

A numerical integration has to be carried out to evaluate the integral appearing in eq.(2).

If unit withdrawal takes place at the first unit time at the  $i^{\text{th}}$  abstraction point, and no withdrawal after that, the cumulative flow at the end of the  $n^{\text{th}}$  time step across the circle is given by,

$$\delta_{Ii}(n) = K(r_i, \theta_i, R, n) - K(r_i, \theta_i, R, n-1)$$

and,

$$\delta_{Ii}(1) = K_i(r_i, \theta, R, 1)$$

The cumulative inflow at the end of  $n^{\text{th}}$  time-step across the circle,  $CUMI_i(n)$ , due to varying abstraction from the  $i^{\text{th}}$  well is given by

$$CUMI_i(n) = \sum_{\gamma=1}^n QP_i(\gamma) \delta_{Ii}(n-\gamma+1)$$

in which,

$QP_i(\gamma)$  = Quantity of water pumped during  $\gamma^{\text{th}}$  time-step at  $i^{\text{th}}$  well.

If there are 'M' abstraction points, then total inflow up to the end of  $n^{\text{th}}$  time-step,  $CUMI(n)$ , due to all withdrawal is expressed by

$$\text{CUMI}(n) = \sum_{i=1}^M \sum_{\gamma=1}^n \text{QP}_i(\gamma) \delta_{I_i}(n-\gamma+1)$$

Similarly total outflow from the circular zone at the end of  $n^{\text{th}}$  time-step due to recharge  $\text{QR}_j(\gamma)$  occurring during  $\gamma^{\text{th}}$  time-step at  $j^{\text{th}}$  recharge point,  $j=1,2,\dots,N$ , and  $\gamma=1,2,\dots,n$ , is given by

$$\text{CUMO}(n) = \sum_{i=1}^N \sum_{\gamma=1}^n \text{QR}_j(\gamma) \delta_{O_j}(n-\gamma+1)$$

$\delta_{O_j}(n)$  and  $\delta_{I_i}(n)$  are identical.

If the number of abstraction points and recharge points inside the circular zone are  $M_C$  and  $N_C$  respectively, then the amount of draft and recharge at the end of  $n^{\text{th}}$  time-step will be,

$$\text{CUMQP}(n) = \sum_{i=1}^{M_C} \sum_{\gamma=1}^n \text{QP}_i(\gamma)$$

$$\text{CUMQR}(n) = \sum_{j=1}^{N_C} \sum_{\gamma=1}^n \text{QR}_j(\gamma)$$

The groundwater availability in that particular zone at the end of  $n^{\text{th}}$  time-step can be expressed by,

$$\text{GW}(n) = \text{CUMQR}(n) - \text{CUMQP}(n) - \text{CUMO}(n) + \text{CUMI}(n)$$

or

$$\begin{aligned}
 GW(n) &= \sum_{j=1}^{N_C} \sum_{\gamma=1}^n QR_j(\gamma) - \sum_{i=1}^{M_C} \sum_{\gamma=1}^n QP_i(\gamma) - \sum_{j=1}^N \sum_{\gamma=1}^n QR_j(\gamma) \delta_{Oj}(n-\gamma+1) \\
 &+ \sum_{i=1}^M \sum_{\gamma=1}^n QP_i(\gamma) \delta_{Ii}(n-\gamma+1) \tag{3}
 \end{aligned}$$

Similar equations for all the circular zones, by which the area is hydrologically decomposed, is obtained and algebraic addition of all these availability of groundwater will give the groundwater storage available for the district. A software for block level water balance is given in Appendix I.

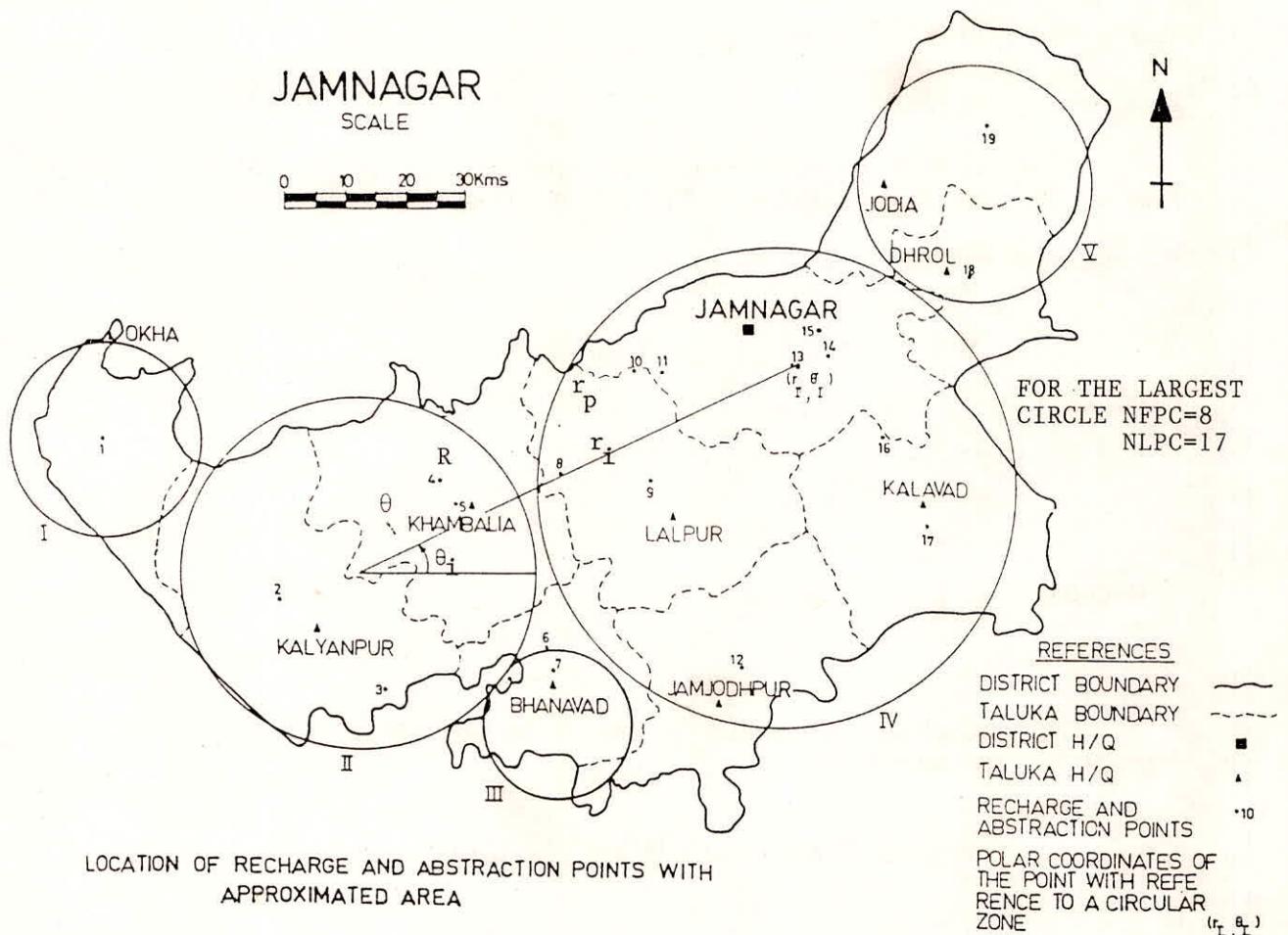


FIG.1: INFLOW TO AND OUTFLOW FROM A CIRCULAR ZONE OF AN INFINITE AQUIFER DUE TO VARIOUS RECHARGE AND ABSTRACTION

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C SOURCE PROGRAM: G11.FOR
C GROUND WATER AVAILABILITY STUDY
C ANNUAL GROUND WATER BALANCE
C 15 SPACE SHOULD BE ASSIGNED FOR EACH BLOCKNAME IN DATA
C FILE
C 6 SPACE SHOULD BE ASSIGNED FOR EACHMONTH NAME IN DATA
C FILE
C 10 SPACE FOR NAME OF INPUTFILE AND OUTPUT FILE
C
C CHARACTER*15 BLNAME
C CHARACTER*6 MONTH
C CHARACTER*10 INPUT,OUTPUT
C
C DIMENSION RABST(50),THABST(50),RRECH(50),THRECH(50),
1 QP(50,20),QR(50,20),SUMQP(20),SUMQR(20),SUMQPI(20)
2 ,SUMQRO(20),GAVAIL(20),DELP(50,20),DELPF(50,20)
3 ,DELR(50,20),DELRF(50,20),MONTH(20),BLNAME(20),BLAREA(20)
4 ,BLWATER(20)
C
C WRITE (5,30)
C30 FORMAT(4X,' INPUT FILE NAME: '$)
C READ(5,29)INPUT
C WRITE(5,31)
C31 FORMAT(4X,'OUTPUT FILE NAME: '$)
C READ(5,29)OUTPUT
C29 FORMAT(A)
C
C OPEN(UNIT=1,FILE=INPUT,STATUS='OLD')
C OPEN(UNIT=2,FILE=OUTPUT,STATUS='NEW')
C OPEN(UNIT=1,FILE='G11.DAT')
C OPEN(UNIT=2,FILE='G11.OUT')
C READ(1,*)NABSTP,NRECHP,NTIME,NFPC,NLPC
C READ(1,*)R,T,PHI,NBL,AVFL
C
C R=RADIUS OF THE CIRCULAR ZONE
C T= AQUIFER TRANSMISSIVITY IN SQUARE METER PER MONTH
C PHI=STORAGE COEFFICIENT
C NBL=NUMBER OF BLOCKS INSIDE THE CIRCLE
C AVFL=AVERAGE WATER LEVEL HEIGHT ABOVE THE DATUM IN
C METER
C AVFL REPRESENTS THE INITIAL STORAGE PRIOR TO ONSET OF
C MONSOON
C
C PAI=4.*ATAN(1.)
C AREA=PAI*R*R/1000000.
C AREA IS IN SQ KM
C DYASTI=PAI*R*R*PHI
C READ(1,46)(MONTH(N),N=1,NTIME)

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DO K=1,NBL
READ(1,42)BLNAME(K),BLAREA(K)
C BLAREA SHOULD BE READ IN SQ KM
ENDDO
READ(1,*)(RABST(I),I=1,NABSTP)
READ(1,*)(THABST(I),I=1,NABSTP)
C RABST(I)= RADIUS OF THE ITH ABSTRACTION POINT
C THABST(I)=THETA OF THE ITH ABSTRACTION POINT
DO 1 I=NABSTP
THABST(I)=THABST(I)*PAI/180.
1 CONTINUE
READ(1,*)(RRECH(I),I=1,NRECHP)
READ(1,*)(THRECH(I),I=1,NRECHP)
C RABST(I)= RADIUS OF THE ITH RECHARGE POINT
C THABST(I)=THETA OF THE ITH RECHARGE POINT
DO 2 I=1,NRECHP
THRECH(I)=THRECH(I)*PAI/180.
2 CONTINUE
DO I=1,NABSTP
READ(1,*)(QP(I,J),J=1,NTIME)
C
C QP(I,J)= PUMPING RATE AT ITH WELL DURING JTH MONTH
C IN CUBIC METER PER MONTH
C
ENDDO
SUM1=0.
SUM2=0.
C NFPC=FIRST(LOWEST) NUMBER ASSIGNED TO WELL (RECHARGE OR
C DISCHARGE)
C NLPC=LAST(HIGHEST) NUMBER ASSIGNED TO WELL (RECHARGE OR
C DISCHARGE)
DO 50 I=NFPC,NLPC
DO 51 J=1,4
SUM1=SUM1+QP(I,J)
51 CONTINUE
DO 52 J=5,12
SUM2=SUM2+QP(I,J)
52 CONTINUE
50 CONTINUE
QMP=SUM1
QNMP=SUM2
C
DO I=1,NRECHP
READ(1,*)(QR(I,J),J=1,NTIME)
C QR(I,J)= RECHARGE RATE AT ITH WELL DURING JTH MONTH
C IN CUBIC METER PER MONTH
ENDDO

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SUM1=0.
SUM2=0.
DO 53 I=NFPC,NLPC
DO 54 J=1,4
SUM1=SUM1+QR(I,J)
54 CONTINUE
DO 55 J=5,12
SUM2=SUM2+QR(I,J)
55 CONTINUE
53 CONTINUE
QMR=SUM1
QNMR=SUM2
WRITE(2,32)AVFL
WRITE(2,49)DYASTI
WRITE(2,33)AREA
WRITE(2,34)PHI
WRITE(2,35)T
WRITE(2,36)QMR
WRITE(2,37)QNMR
WRITE(2,38)QMP
WRITE(2,39)QNMP
WRITE(2,40)
WRITE(2,41)
WRITE(2,28)
WRITE(2,26)
DO 6 I=1,NABSTP
THETA=THABST(I)
AAR=RABST(I)
DO 7 J=1,NTIME
AJ=J
CALL DEL(THETA,AAR,AJ,R,T,PHI,RES)
DELP(I,J)=RES
7 CONTINUE
6 CONTINUE
DO 8 I=1,NABSTP
DELPF(I,1)=DELP(I,1)
DO 9 J=2,NTIME
DELPF(I,J)=DELP(I,J)-DELP(I,J-1)
9 CONTINUE
8 CONTINUE
DO 10 I=1,NRECHP
THETA=THRECH(I)
AAR=RRECH(I)
DO 11 J=1,NTIME
AJ=J
CALL DEL(THETA,AAR,AJ,R,T,PHI,RES)
DELR(I,J)=RES
11 CONTINUE
10 CONTINUE

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DO 12 I=1,NRECHP
DELRF(I,1)=DELR(I,1)
DO 13 J=2,NTIME
DELRF(I,J)=DELR(I,J)-DELR(I,J-1)
13 CONTINUE
12 CONTINUE
DO 14 N=1,NTIME
SUM=0.
DO 15 I=1,NABSTP
DO 16 NGAMA=1,N
16 SUM=SUM+QP(I,NGAMA)*DELPF(I,N-NGAMA+1)
IF(SUM.LT.0.0)SUM=0.0
15 CONTINUE
SUMQPI(N)=SUM
14 CONTINUE
DO 27 N=1,NTIME
SUM=0.
DO 17 I=1,NRECHP
DO 18 NGAMA=1,N
18 SUM=SUM+QR(I,NGAMA)*DELRF(I,N-NGAMA+1)
IF(SUM.LT.0.0)SUM=0.0
17 CONTINUE
SUMQRO(N)=SUM
27 CONTINUE
DO 19 N=1,NTIME
19 GAVAIL(N)=0.
DO 20 N=1,NTIME
SUMQP(N)=0.
SUMQR(N)=0.
DO 21 I=NFPC,NLPC
21 SUMQP(N)=SUMQP(N)+QP(I,N)
DO 22 I=NFPC,NLPC
22 SUMQR(N)=SUMQR(N)+QR(I,N)
20 CONTINUE
DO 23 N=1,NTIME
SUM=0.
DO 24 NGAMA=1,N
SUM=SUM+SUMQPI(NGAMA)-SUMQRO(NGAMA)-
1 SUMQP(NGAMA)+SUMQR(NGAMA)
24 CONTINUE
GAVAIL(N)=SUM+DYASTI
WRITE(2,25)N,MONTH(N),GAVAIL(N),SUMQR(N),SUMQP(N),SUMQRO(N),
1 SUMQPI(N)
23 CONTINUE
WRITE(2,47)
DO 99 K=1,NBL
WRITE(2,43)BLNAME(K)
WRITE(2,48)
WRITE(2,45)

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C
DO 98 N=1,NTIME
BLWATER(N)=GAVAIL(N)
BLWATER(N)=BLWATER(N)*BLAREA(K)/AREA
WRITE(2,44)MONTH(N),BLWATER(N)
98 CONTINUE
WRITE(2,47)
99 CONTINUE

C DO I = 1, 6
C WRITE(2,*) (DELPF(I,J),J=1,12)
C ENDDO
C DO I = 1,4
C WRITE(2,*) (DELRF(I,J),J=1,12)
C ENDDC

25 FORMAT(1X,I2,1X,A7,2X,E10.2,4(2X,E12.4))
26 FORMAT(17x,'(cum)',8x,'(cum)',9x,'(cum)',9x,'(cum)'
1 ,9x,'(cum)'/)
28 FORMAT(1X,'N',2X,'MONTH',2X,'WATERBALANCE',3X,'RECHARGE',
1 5X,'WITHDRAWAL',7X,'OUTFLOW',7X,'INFLOW')
32 FORMAT(10X,'Average water level height above datum =',1X,F5.2,
1 1X,'m',/)
33 FORMAT(10X,'Area of the circular zone ='1X,F7.2,1X,'sq.km.',/)
34 FORMAT(10X,'Storage coefficient ='1X,F7.2,/)
35 FORMAT(10x,'Transmissivity ='1X,E7.2,1X,'sqm/month',/)
36 FORMAT(10X,'Monsoon recharge ='1X,E10.2,1X,'cum',/)
37 FORMAT(10X,'Nonmonsoon recharge ='1X,E10.2,1X,'cum',/)
38 FORMAT(10X,'Monsoon draft ='1X,E10.2,1X,'cum',/)
39 FORMAT(10X,'Nonmonsoon draft ='1X,E10.2,1X,'cum',/)
40 FORMAT(10X,'TEMPORAL GROUNDWATER AVAILABILITY:')
41 FORMAT(10X,34('*'),/)
42 FORMAT(A10,F8.2)
43 FORMAT(26X,'BLOCK:',1X,A10)
44 FORMAT(24X,A7,4X,E10.3)
45 FORMAT(24X,'Month',5X,'WATER BALANCE(in cum)',/)
46 FORMAT(12A6)
47 FORMAT(/)
48 FORMAT(25X,18('*'))
49 FORMAT(10X,'INITIAL DYNAMIC STORAGE ='2X,E12.4, 2X,'cum',/)
STOP
END
C

```

C  
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C  
C

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Numerical Integration

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```
SUBROUTINE DEL(THETA,AAR,AJ,R,T,PHI,RES)
PAI=4.*ATAN(1.)
N=100
A=0.
B=2.*PAI
H=B/FLOAT(N)
CALL EVAL(A,THETA,AAR,AJ,R,T,PHI,FINAL)
FA=FINAL
CALL EVAL(B,THETA,AAR,AJ,R,T,PHI,FINAL)
FB=FINAL
SUM=FA+FB
NN=N-1
DO 10 K=1,NN
X=A+FLOAT(K)*H
CALL EVAL(X,THETA,AAR,AJ,R,T,PHI,FINAL)
SUM=SUM+2.*FINAL
10 CONTINUE
RES=H*SUM/2.
RETURN
END
```

10

C  
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C  
C  
C

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Computation of the Integrand

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```
SUBROUTINE EVAL(TH,THETA,AAR,AJ,R,T,PHI,FINAL)
PAI=4.*ATAN(1.)
F1=AAR*COS(THETA-TH)
F2=R*R+AAR*AAR
F3=R-F1
F4=F2-2.*R*F1
BETA=4.*T/PHI
F5=F4/(BETA*AJ)
CALL EXI(F5,EXFN)
F6=AJ*EXP(-F5)-EXFN*F5*AJ
F7=R*F3/(2.*PAI*F4)
FINAL=F7*F6
RETURN
END
```

C

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C *****
C           Computation of Exponential Integral
C *****
C
SUBROUTINE EXI(X,EXFN)
  IF(X-1.0)1,1,22
1  EXFN=-ALOG(X)-0.57721566+0.99999193*X-0.24991055*X**2
  1  +0.05519968*X**3-0.00976004*X**4+0.00107857*X**5
  GO TO 3
22  CONTINUE
  IF(X-80.)5,4,4
5  CONTINUE
  EXFN=((X**4+8.5733287*X**3+18.059017*X**2+8.6347608*X
1  +0.26777373)/(X**4+9.5733223*X**3+25.632956*X**2
2  +21.099653*X+3.9584969))/(X*EXP(X))
  GO TO 3
4  EXFN=0.
3  CONTINUE
  RETURN
  END

```

INPUT FILE: G11.DAT

6 4 12 1 5  
3000. 9000. 0.01 2 2.  
JUL. AUG. SEP. OCT. NOV. DEC. JAN. FEB. MAR. APR. MAY JUN.  
WASIS 7.0  
SPRING 3.0  
1000. 2000. 1500. 4000. 5000. 3500.  
15. 30. 45. 90. 60. 65.  
700. 2500. 5000. 6000.  
5. 20. 35. 70.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 1000. 4500. 1000. 1000. 1000.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 2000. 2500. 1000. 1000. 1000.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 3000. 1500. 1000. 1000. 1000.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 4000. 2000. 1000. 1000. 1000.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 5000. 3500. 1000. 1000. 1000.  
0.0 0.0 0.0 0.0 1000. 2000. 750. 6000. 4000. 1000. 1000. 1000.  
  
1000. 1500. 1400. 4300. 0. 0. 100. 200. 300. 300.  
100. 100.  
2000. 2500. 2400. 3300. 0. 0. 100. 200. 300. 300.  
100. 120.  
3000. 3500. 3400. 2300. 0. 0. 100. 200. 300. 300.  
100. 130.  
4000. 4500. 4400. 1300. 0. 0. 100. 200. 300. 300.  
100. 140.

OUTPUT FILE: G11.OUT

Average water level height above datum = 2.00 m

INITIAL DYNAMIC STORAGE = .2827E+06 cum

Area of the circular zone = 28.27 sq.km.

Storage coefficient = .01

Transmissivity = .90E+04 sqm/month

Monsoon recharge = .45E+05 cum

Nonmonsoon recharge = .45E+04 cum

Monsoon draft = .00E+00 cum

Nonmonsoon draft = .63E+05 cum

TEMPORAL GROUNDWATER AVAILABILITY:

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N	MONTH	WATER BALANCE (cum)	RECHARGE (cum)	WITHDRAWAL (cum)	OUTFLOW (cum)	INFLOW (cum)
1	JUL.	.29E+06	.1000E+05	.0000E+00	.6228E+03	.0000E+00
2	AUG.	.30E+06	.1200E+05	.0000E+00	.1707E+04	.0000E+00
3	SEP.	.31E+06	.1160E+05	.0000E+00	.3022E+04	.0000E+00
4	OCT.	.32E+06	.1120E+05	.0000E+00	.4915E+04	.0000E+00
5	NOV.	.31E+06	.0000E+00	.5000E+04	.6608E+04	.0000E+00
6	DEC.	.29E+06	.0000E+00	.1000E+05	.7885E+04	.3588E+03
7	JAN.	.28E+06	.4000E+03	.3750E+04	.8902E+04	.1569E+04
8	FEB.	.26E+06	.8000E+03	.1500E+05	.9786E+04	.1783E+04
9	MAR.	.23E+06	.1200E+04	.1400E+05	.1062E+05	.2763E+04
10	APR.	.22E+06	.1200E+04	.5000E+04	.1141E+05	.5321E+04
11	MAY	.22E+06	.4000E+03	.5000E+04	.1210E+05	.8051E+04
12	JUN.	.21E+06	.4900E+03	.5000E+04	.1272E+05	.1070E+05

BLOCK: WASIS

\*\*\*\*\*

Month WATER BALANCE(in cum)

JUL.	.723E+05
AUG.	.749E+05
SEP.	.770E+05
OCT.	.785E+05
NOV.	.757E+05
DEC.	.713E+05
JAN.	.687E+05
FEB.	.632E+05
MAR.	.581E+05
APR.	.556E+05
MAY	.535E+05
JUN.	.519E+05

BLOCK: SPRING

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Month WATER BALANCE(in cum)

JUL.	.310E+05
AUG.	.321E+05
SEP.	.330E+05
OCT.	.337E+05
NOV.	.324E+05
DEC.	.306E+05
JAN.	.294E+05
FEB.	.271E+05
MAR.	.249E+05
APR.	.238E+05
MAY	.229E+05
JUN.	.222E+05