

UM-32

POWER TRANSFORMATION TECHNIQUE  
IN BASIC  
FOR FLOOD FREQUENCY ANALYSIS

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## ABSTRACT

Flood frequency analysis is a very useful technique for the estimation of design flood corresponding to a specified recurrence interval from the limited data. Generally, sample data is fit to several frequency distributions and then a suitable distribution is considered for estimating the floods of required recurrence intervals. Instead of fitting a probability distribution to raw data, sometimes the data is transformed, so that it conforms to a particular distribution of known characteristics for the purpose of flood frequency analysis. Power transformation (Box and Cox) is one of the powerful techniques for transforming any data series to near normal series.

The present user's manual describes the power transformation technique in details and the computer programme transforms the given series of annual maximum peak flood to near normal distribution using power transformation. It then performs the flood frequency analysis on this transformed series using the method of moments for estimating 50, 100, 200, 500, 1000 and 10,000 years return period floods using two approaches based on the criteria that (i) coefficient of skewness is nearly zero and (ii) coefficient of skewness is nearly zero and coefficient of Kurtosis nearly equal to 3.0

The programme of this user's manual is usable both on VAX-11/780 computer system as well as on IBM compatible Personal Computer with minor changes, which

has been described in the programme itself. This user's manual also lists the sample input and corresponding generated output of one example.

## 1.0 INTRODUCTION

### 1.1 General

The estimation of design flood of desired frequency from fairly short series of observed data is one of the major problems faced in hydrology. The sample data is used to fit frequency or probability distribution which in turn is used to extrapolate from recorded events to design events either graphically or analytically.

Graphical method has the advantage of simplicity and visual presentation. But the main disadvantage is that different persons will fit different curves. In theoretical analysis, either the data are fitted to the most appropriate frequency distribution or the data are transformed to a particular frequency distribution of known characteristics.

Since the properties of a normal distribution are completely defined, so this distribution is generally used. But the hydrological data in its original form are rarely normally distributed. Many of the hydrological data are positively skewed and so the application of normal distribution to the original data is not appropriate. However, various methods are available to transform the data to normal distribution e.g. log transformation (Chow, 1954), inverse pearson type III transformation (Beard, 1967), Square root transformation, (Richardson, 1978), cube root transformation (Stidd, 1953), and inverse log pearson type III transformation. All

these transformations have been shown to be special cases of power transformation (Box and Cox, 1964).

Goodness of fit of various distribution is examined based on some statistical criteria. Chi-square test, Kolmorov-Smirnov and Crammer-Von Mises test are some of the well known tests for this purpose.

## 1.2 BASIC Language

Although BASIC stands for Beginner's All-purpose Symbolic Instruction Code, it is an extremely powerful and useful language.

Within the last few years, BASIC has become one of the leading programming languages because of widespread popularity and proliferation of microcomputers, nearly all of which now have BASIC interpreters or compilers.

BASIC is easy to learn and use. It is very flexible and is very well suited for use in an interactive environment. It has the facility for manipulation of character strings and carrying out arithmetical operations on matrices.

BASIC is relatively standardized, though there may be minor differences between one version of BASIC and another. Thus the language is largely machine-independent. Consequently, most BASIC programmes can be run on many different computers with little or no modification.

## 1.3 Purpose

The computer programme has been developed in BASIC

on the basis of the logic given by Seth and Perumal (1982). It performs the flood frequency analysis using the power transformation for estimating the floods of 50,100,200, 500,1000, 10,000 years return periods. This analysis is based on the two approaches viz. (i) the coefficient of skewness is nearly zero and (ii) the coefficient of kurtosis is nearly equal to 3.0 as well as coefficient of skewness is nearly zero.

#### 1.4 Scope

The programme can be used to estimate the peak flood of specified return periods. Statistical parameters e.g. mean, standard deviation, coefficient of skewness, coefficient of kurtosis and Chi-Square statistic etc. can also be computed.



## 2.0 FLOOD FREQUENCY ANALYSIS

The basic objective in the use of statistical methods and statistical distribution is the analysis of outcomes of real observations of random phenomena such as floods. For solving the practical statistical problems, generally the following steps are involved:

- i) Application of various statistical distribution.
- ii) Estimation of their parameters
- iii) A check of the goodness of the distribution in fitting the given sample of annual maximum peak series by various statistical tests.
- iv) Selection of most appropriate statistical distribution.
- v) Prediction of future floods using this distribution.

In this user's manual, power transformation has been discussed and used. The parameters of the distribution are estimated by the method of moments.

### 2.1 Power Transformation Technique for flood Frequency Analysis:

The given annual peak flood series can be transformed to the nearly normal distribution by using power transformation (Box & Cox) i.e.

$$Z_i = \frac{X_i^\lambda - 1}{\lambda} \quad \text{for } \lambda \neq 0$$

and  $Z_i = \ln X_i \quad \text{for } \lambda \rightarrow 0 \quad \dots(i)$

in which,

$X_i$  = the variate of given series

$Z_i$  = the transformed variates

$\lambda$  = an exponent which near normalizes the series and its value is found by trial and error.

Eqn.(i) is a more general power transformation and it can be shown that the logarithmic, reciprocal, and square root transformation are special cases of it.

The near normalization is considered to be achieved when the coefficient of skewness (CS) of the transformed series approaches to zero.

The unbiased coefficient of skewness of the sample data is computed as:

$$CS = \frac{N}{(N-1)(N-2)} \left[ \frac{\sum_{i=1}^N (Z_i - \bar{Z}_i)^3}{S^3} \right] \quad \dots(ii)$$

where,

$N$  = the sample size

$Z_i$  = the power transformed variate

$\bar{Z}_i$  = the mean of the power transformed variates

$$= \frac{1}{N} \sum_{i=1}^N Z_i \quad \dots(iii)$$

$S$  = Sample standard deviation

$$= \frac{1}{(N-1)} \left[ \sum_{i=1}^N (Z_i - \bar{Z}_i)^2 \right]^{1/2} \quad \dots(iv)$$

The value of  $\lambda$  which near normalizes the data series is obtained by grid search technique by using the criterion that there is a systematic variation of CS for variation of  $\lambda$ . For near normality the value

of CSL (deviation of coefficient of skewness) is specified depending upon the accuracy required. It is found that 0.001 is a quite reasonable value. So in present programme this value has been inputted.

The unbiased coefficient of kurtosis of the sample data is computed as:

$$CK = \frac{N^2}{(N-1)(N-2)(N-3)} \left[ \frac{\sum_{i=1}^N (Z_i - \bar{Z}_i)^4}{S^4} \right] \dots (v)$$

The transformed series is said to be near normalized if the coefficient of kurtosis (CK) of the transformed series may be near to, if not equal to 3.0, as required for normal distribution.

Estimation of flood peaks:

Neglecting the kurtosis in the transformed series, the flood peak  $X(T)$  of recurrence interval  $T$  can be estimated from the following expression-

$$X_T = (Z_T^{\lambda+1})^{1/\lambda} \dots (vi)$$

where,

$X_T$  = Flood peak magnitude in the original series.

$Z_T$  = Flood peak magnitude in the transformed series.

$$= \bar{Z} + K(T)S \dots (vii)$$

$K(T)$  = Standard deviate corresponding to recurrence interval  $T$

For taking into consideration the effect of kurtosis  $K(T)$  should be adjusted for estimating  $X_T$  by eqn.(vi) so, in spite of standard deviate, it will be a function of Kurtosis  $CK$  to account for non-normality.

Box and Tio (1973) have introduced a factor  $\beta$  as a measure of symmetrical distribution (Table 1 and 2). Thus the transformed series can be adjusted for Kurtosis by using the value of the adjusted standard deviate  $K$  corresponding to the calculated value of  $\beta$ . The programme computes the estimates of different recurrence intervals based on kurtosis correction procedure.

Although, log transformation is a particular case of power transformation, its identification due to the required division of the quantity  $(X^\lambda - 1)$  by  $\lambda$ , which is nearly equal to zero. Therefore, provision is made in the programme to compute, in variably, the log transformation of the series for the purpose of computing flood peak estimates for 50, 100, 200, 500, 1000 and 10,000 year return periods.

The goodness of fit test:

The goodness of fit is evaluated by the most commonly used Chi-Square statistic viz., (i) equal class interval method and (ii) equal probability method. The latter approach has been used in present programme. The observed data are grouped into NCLASS Classes. The number of classes is supplied by the user. The Chi-Square Statistic is computed as:

$$\chi^2 = \sum_{i=1}^{NCLASS} \left[ \frac{(f_{oi} - f_{ei})^2}{f_{ei}} \right] \quad \dots (viii)$$

where

$f_{oi}$  = the observed frequency in the  $i^{th}$  class interval

$f_{ei}$  = the expected frequency in the  $i^{th}$  class interval

TABLE-1

RELATIONSHIP BETWEEN BETA AND CK REQUIRED FOR CURTOSIS CORRECTED  
STANDARD NORMAL DEVIATES

DATA	VALUES									
BETA	-1.00	-0.75	-0.50	-0.25	0.00	0.25	0.50	0.75	1.00	
CK	-1.20	-1.07	-0.81	-0.45	0.00	0.55	1.22	2.03	3.00	

TABLE-2

ADJUSTED STANDARD DEVIATE K FOR SMALLER PROBABILITIES ALPHA FOR VALUES OF BETA

BETA	ALPHA 0.25	ALPHA 0.10	ALPHA 0.05	ALPHA 0.025	ALPHA 0.01	ALPHA 0.005	ALPHA 0.001
-1.00	0.87	1.39	1.56	1.65	1.70	1.71	1.73
-0.75	0.84	1.36	1.57	1.71	1.84	1.91	2.05
-0.50	0.80	1.35	1.61	1.81	2.03	2.16	2.41
-0.25	0.73	1.31	1.63	1.89	2.18	2.37	2.75
0.00	0.67	1.28	1.64	1.96	2.33	2.58	3.09
0.25	0.62	1.25	1.65	2.02	2.46	2.77	3.43
0.50	0.58	1.22	1.65	2.06	2.58	2.94	3.75
0.75	0.53	1.18	1.64	2.09	2.68	3.10	4.08
1.00	0.49	1.14	1.63	2.12	2.77	3.28	4.39

$\alpha$  = the level of significance at which the distribution of fitting the data is being tested.

The programme only computes  $\chi^2$  statistic and it is left to the user for verifying the goodness of fit.

## 2.2 Programme Description

Much of the programme is explained by remark cards. However, subroutines used in the programme are explained in details:

### (a) Subroutine STAPS

This subroutine calculates the statistical parameters e.g. Mean, Unbiased standard deviation, Unbiased coefficient of skewness and unbiased coefficient of kurtosis of the given series.

### (b) Subroutine ASCOR

This subroutine has been used for arranging the given series in ascending order.

### (c) Subroutine INPOL and Subroutine AKIMA

These subroutines are used for interpolation based on smooth curve fitting using procedure given by AKIMA (1970). It interpolates linearly if only two points are available.

### (d) Subroutine CHIST

This subroutine computes the Chi-Square statistic based on equal probability criterion for each class interval

### (e) Subroutine PROND

The purpose of this sub-routine is to calculate standard normal variate and the corresponding ordinate

of the normal distribution for the given probability of non-exceedence.

The listing of computer programme has been given in Appendix I.

### 2.3 Hardware and Software Requirements

The programme has been written in BASIC and has been implemented and tested on VAX-11/780 version 4.2 computer system of National Institute of Hydrology, Roorkee. Same programme has also been tested and implemented on IBM Compatible Personal Computer with minor differences which have been explained in the programme itself by Remark Cards. It requires BASIC compiler and simple BASIC instruction to run the programme on VAX and Microsoft BASIC version.1.12 software on personal computer.

For VAX the CPU time required is 11.53 secs and total elapsed time is 16.57 sec. For P.C. total elapsed time required is 3 mins 4 secs.

### 3.0 DATA REQUIREMENTS

Description of input variables is given below:

Variable	Description
N	Number of annual maximum values to be analysed.
NCLASS	Number of classes used in the Chi-Square test
CSL	Specified accuracy limit for coefficient of skewness
RI	Recurrence interval for which flood estimate are made.
DL	Grid size used in the search method for determining the power transformation exponent which near normalizes the series.
IYEAR	Year corresponding to the annual maximum series
X	the annual maximum series.

### 3.1 Preparation of Input Data

Five input cards which are read in free format are required. The form in which the data to be supplied is as given below:

Card 1

N, NCLASS, CSL

Card 2

RI(1), RI(2), RI(3).....RI(6)

Card 3

DL(1), DL(2), DL(3)

Card 4



IYEAR(1), IYEAR(2),.....IYEAR(N)

Card 5

X(1), X(2), X(3).....X(N)

The declared dimensions of the variables of last four cards which are read by Mat input statement should be exactly the same numbers as used for programme and not more or less.

### 3.2 Output Description

The output tabulates the original, log transformed and power transformed series in chronological order along with years and it arranges these in ascending order of magnitude and corresponding year of occurrence. It assigns the rank to them and computes the probability of non-exceedances using Blom's plotting position. The statistical parameters of the series are written. Chi-Square statistics are also written for log-transformed and for power transformed series. The flood peak estimate of log-transformed and power-transformed corresponding to required recurrence intervals of 50,100,200,500,1000,1000 years are given.

#### 4.0 CASE STUDY

For running the programme and for an example, the data has been taken from Varshney (5).

#### 4.1 Data Used for Case Study

The information required for input data is as follows:-

Card 1

The number of years of annual peak flow series (N) =77

The number of class interval used in Chi-Square test (NCLASS)=8

Limit of accuracy for coefficient of skewness=0.001

So input of Card

77,8,0.001

Card2

The recurrence interval for which the flood magnitudes are to be estimated are

RI(4) = 50, RI(2) =100, RI(3)=200

RI(4) = 500, RI(5)=1000, RI(6) =10000

So input of the card

50,100,200,500,1000,10000

Card 3

The grid size used in grid search technique for estimating the exponent are-

DL(1)=0.1, DL(2)=0.01, DL(3)=0.001

So input of Card

0.1, 0.01, 0.001

Card 4

The year of occurrence of the given magnitude of flood e.g. IYEAR (1), IYEAR(2),.....IYEAR(77)

So input of card

1901, 1902, 1903,.....1977

Card 5

The peak flood series arranged in chronological order e.g. X(1), X(2), X(3),..... X(77).

So input of the card

11400, 9250, 7400,.....5710

The test input and the test output of the programme are given in Appendix II and III respectively.

## 5.0 CONCLUSIONS

Application of the power transformation to flood frequency studies does not require the assumption of the population distribution. It is more efficient than other transformations in normalizing the skewed flood distribution. Power transformation method can also incorporate the effect of the kurtosis in the estimation of flood.

#### REFERENCES

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3. Chander, S.,S.K.Spolia and Arun Kumar (1978), "Flood Frequency Analysis by Power Transformation", Jour. of the Hydraulics Div.ASCE, Vol.104, No.HY11, November, pp.1495-1504.
4. Seth, S.M., and M.Perumal (1982-83), "Flood Frequency Analysis Using Power Transformation", report DP-1, National Institute of Hydrology, Roorkee (U.P.).
5. Varshney, R.S.( 1979 ) , "Engineering Hydrology", Nem Chand and Brothers, Roorkee, U.P., pp 604-605.

APPENDIX - I : LISTING OF PROGRAMME

```

05 REM THIS PROGRAMME PERFORMS THE FLOOD FREQUENCY ANALYSIS &
06 ' OF ANNUAL MAXIMUM SERIES USING LOG TRANSFORMATION AND &
07 ' POWER TRANSFORMATION (BOX-COX TRANSFORMATION), ASSUMING &
08 ' THE TRANSFORMED SERIES FOLLOWS THE NORMAL DISTRIBUTION

10 REM DESCRIPTION OF TERMS
11 REM -----
12 REM X      = ANNUAL MAXIMUM SERIES
15 REM Y      = POWER TRANSFORMED ANNUAL MAXIMUM SERIES
20 REM Z      = LOG TRANSFORMED ANNUAL MAXIMUM SERIES      &
21 '          ARRANGED IN DESCENDING ORDER
25 REM DL     = GRID SIZE USED IN THE SEARCH METHOD FOR      &
26 '          DETERMINING THE EXPONENT ,LAMDA WHICH          &
27 '          NEAR NORMALISES THE SERIES
30 REM SK     = ARRAY FOR STORING KURTOSIS VALUES
35 REM X1     = ARRAY FOR STORING THE ANNUAL MAXIMUM        &
36 '          SERIES IN CHRONOLOGICAL ORDER
40 REM P      = PROBABILITY USING BLOM'S PLOTTING POSITION
45 REM IYEAR  = YEAR CORRESPONDING TO ANNUAL MAX. VALUES
50 REM ALPHA  = TABLE OF STANDARD NORMAL DEVIATES        &
51 '          CORRECTED FOR KURTOSIS
52 REM ALPHAS = TEMPORARY ARRAY FOR STORING ALPHA
53 REM ALINPI = ARRAY OF INTERPOLATED STANDARD NORMAL      &
54 '          DEVIATES CORRESPONDING TO THE DIFFERENT      &
55 '          PROBABILITY OF EXCEEDENCE LEVEL
56 REM IYEAR1 = ARRAY OF YEARS IN CHRONOLOGICAL ORDER
58 REM X2     = TABLE OF DEVIATION OF THE COEFFICIENT OF  &
59 '          KURTOSIS VALUES AWAY FROM 3.00
60 REM Y2     = TABLE OF CORRECTION FACTORS CORRESPONDING TO X2
62 REM Z1     = LOG TRANSFORMED FLOOD FLOW VALUES IN      &
63 '          CHRONOLOGICAL ORDER
64 REM Y1     = POWER TRANSFORMED FLOOD FLOW VALUES IN    &
65 '          CHRONOLOGICAL ORDER
66 REM RI     = RECURRENCE INTERVAL FOR WHICH FLOOD        &
67 '          ESTIMATE ARE MADE
68 REM TD     = STANDARD NORMAL DEVIATE OBTAINED FROM      &
69 '          THE PROBABILITY OF EXCEEDENCE
70 REM ESTP   = ESTIMATED FLOOD PEAK USING POWER TRANSFORMATION
71 REM PEX    = TABLE OF EXCEEDENCE PROBABILITIES FOR      &
72 '          WHICH KURTOSIS CORRECTED STANDARD NORMAL      &
73 '          DEVIATES ARE AVAILABLE
74 REM ALINPI1 = TEMPORARY ARRAY FOR STORING ALINPI
76 REM PEX1   = TEMPORARY ARRAY FOR STORING PEX
78 REM IRI    = TEMPORARY ARRAY FOR STORING RI
80 REM NPTS   = NO. OF CK VALUES AVAILABLE FOR KURTOSIS &
81 '          CORRECTION
82 REM NALPHA = NO. OF EXCEEDENCE PROBABILITIES FOR        &
83 '          WHICH KURTOSIS CORRECTED STANDARD NORMAL      &
84 '          DEVIATES ARE AVAILABLE
85 REM NCLASS = NUMBER OF CLASSES USED IN THE CHI-SQUARE TEST
86 REM N      = NUMBER OF ANNUAL MAXIMUM VALUES
90 REM *****

```

```

100 DIM X(77),Y(100),Z(100),DL(3),SK(100),X1(100),P(100),X2(9)
101 DIM IYEAR(77),ALPHA(9,7),YYY(9),ALPHAS(9),ALINPI(9),Y2(9)
102 DIM IYEAR1(100),Z1(100),Y1(100),RI(6),TD(10),ESTP(10)
103 DIM ALINPI1(9),PEX1(7),IRI(10),T(81),XX(100),XXX(9),PEX(7)

```

```

107 REM *****
108 REM ***** FOR USE ON IBM COMPATIBLE PC'S *****
109 REM *****
110 REM THE FOLLOWING STATEMENTS (115-155) ARE FOR USING &
111 ' PROGRAMME ON IBM COMBATIBLE PERSONAL COMPUTERS &
112 ' (PC'S).FOR USING IT ON MAIN FRAME PUT ' REM ' &
113 ' STATEMENT ON THESE.
120 OPEN "I",#1,"PTP.INP"
125 OPEN "O",#2,"PT.OUT"
126 OPEN "O",#3,"PT1.OUT"
130 REM ***** READ INPUT INFORMATION (FOR PC) *****
135 INPUT#1,N,NCLASS,CKL
140 FOR I = 1 TO 6 : INPUT#1,RI(I) : NEXT I
145 FOR I = 1 TO 3 : INPUT#1,DL(I) : NEXT I
150 FOR I = 1 TO 77 : INPUT#1,IYEAR(I) : NEXT I
155 FOR I = 1 TO 77 : INPUT#1,X(I) : NEXT I
156 REM *****

```

```

164 REM *****
165 REM ***** FOR USE ON VAX-11/780 COMPUTER *****
166 REM *****
170 REM THE FOLLOWING STATEMENTS (180-245) ARE FOR USING &
171 ' PROGRAMME ON VAX-11/780 COMPUTER . FOR USING IT &
172 ' ON IBM COMBATIBLE PERSONAL COMPUTERS (PC'S) PUT &
173 ' REM ' STATEMENT ON THESE.

```

```

180 REM OPEN "PTV.INP" FOR INPUT AS FILE #1
185 REM OPEN "PT.OUT" FOR OUTPUT AS FILE #2,RECORDSIZE 131#
190 REM OPEN "P1.OUT" FOR OUTPUT AS FILE #3,RECORDSIZE 131#

```

```

220 REM **** READ INPUT INFORMATION (FOR VAX COMP.) ****
225 REM INPUT#1,N,NCLASS,CKL
230 REM MAT INPUT#1,RI
235 REM MAT INPUT#1,DL
240 REM MAT INPUT#1,IYEAR
245 REM MAT INPUT#1,X
246 REM *****

```

```

249 REM *****
250 REM *** FROM THIS POINT ONWARDS PROGRAMME CAN BE USED &
251 ' EITHER ON VAX-11/780 COMPUTER OR ON IBM COMBATIBLE &
252 ' PC'S WITH MINOR CHANGES IN STATEMENTS CONTAING &
253 ' PRINT USING STATEMENTS( &
254 ' FORMAT IS GIVEN BELOW: &
255 ' FOR VAX-11/780 ---- PRINT#2 USING A$,B;C &
256 ' FOR PC'S ---- PRINT#2,USING A$,B;C
257 REM *****

```

```

260   FOR I = 1 TO 9
261   READ X2(I)
262   NEXT I
265   FOR J = 1 TO 9
266   READ Y2(J)
267   NEXT J
270   FOR K = 1 TO 7
271   READ PEX(K)
272   NEXT K
275   FOR M = 1 TO 7
276   FOR L = 1 TO 9
277   READ ALPHA(L,M)
278   NEXT L
279   NEXT M

285   DATA -1.20,-1.07,-0.81,-0.45,0.0,0.55,1.22,2.03,3.00
290   DATA -1.00,-0.75,-0.50,-0.25,0.0,0.25,0.50,0.75,1.00
295   DATA 0.25,0.10,0.05,0.025,0.01,0.005,0.001
300   DATA 0.87,0.84,0.80,0.73,0.67,0.62,0.58,0.53,0.49
301   DATA 1.39,1.36,1.35,1.31,1.28,1.25,1.22,1.18,1.14
302   DATA 1.56,1.57,1.61,1.63,1.64,1.65,1.65,1.64,1.63
303   DATA 1.65,1.71,1.81,1.89,1.96,2.02,2.06,2.09,2.12
304   DATA 1.70,1.84,2.03,2.18,2.33,2.46,2.58,2.68,2.77
305   DATA 1.71,1.91,2.16,2.37,2.58,2.77,2.94,3.10,3.28
306   DATA 1.73,2.05,2.41,2.75,3.09,3.43,3.75,4.08,4.39

310   PRINT#2,TAB(13);
315   OS$="THE TOTAL VALUES IN THE ORIGINAL SERIES ARE = ####"
320   PRINT#2,USING OS$;N
325   PRINT#2,CHR$(10);TAB(15);"NOTE: BLOMS PLOTTING POSIT ";
327   PRINT#2,"ION IS USED THROUGHOUT";CHR$(10),CHR$(10)
330   PRINT#2,TAB(22);
331   FOR I= 1 TO 35
332   PRINT#2, CHR$(42);
333   NEXT I
335   PRINT#2,
336   PRINT#2,TAB(22);"* ANALYSIS OF THE ORIGINAL SERIES *"
337   PRINT#2,TAB(22);
338   FOR I= 1 TO 35
339   PRINT#2, CHR$(42);
340   NEXT I
341   PRINT#2,CHR$(10)
342   REM ***   ARRANGING THE DATA IN ASCENDING ORDER   ****
345   FOR I = 1 TO N
350   P(I)=(I-0.375)/(N+0.25)
355   P = P(1)
360   REM CALL PROND(P,T,D,IE)
365   GO SUB 8000
370   IYEAR1(I)=IYEAR(I)
380   X1(I)=X(I)
385   XX(I)=X(I)
390   NEXT I
400   REM CALL ASCOR(N,IYEAR(),X())
405   GO SUB 4000

```



```

420 FOR I=1 TO 76
422 PRINT#2, CHR$(95);
424 NEXT I
426 PRINT#2,
430 DC$="! DATA IN CHRONOLOGICAL !"
432 DA$=" DATA IN ASCENDING !"
433 O$="ORDER"
434 P$="! PROBABILITY !"
435 S$="! SL.NO.!"
436 R$="! RANK ! OF NON- !"
437 EX$="! EXCEEDENCE !"
438 Y$="! YEAR ! DISCHARGE ! YEAR ! DISCHARGE !"
440 PRINT#2, "!" ; TAB(9) ; DC$ ; TAB(36) ; DA$ ; TAB(62) ; "!" ; TAB(76) ; "!"
450 PRINT#2, "!" ; TAB(9) ; "!" ; TAB(19) ; O$ ; TAB(33) ; "!" ;
451 PRINT#2, TAB(42) ; O$ ; TAB(55) ; "!" ; TAB(62) ; P$
460 PRINT#2, S$;
465 FOR I = 1 TO 45
466 PRINT#2, CHR$(45);
467 NEXT I
468 PRINT#2, R$
470 PRINT#2, "!" ; TAB(9) ; Y$ ; TAB(62) ; EX$
480 FOR I=1 TO 76
482 PRINT#2, CHR$(45);
484 NEXT I
486 PRINT#2,
490 FOR I = 1 TO N
500 PRINT#2, "!" ; I ; TAB(9) ; "!" ; IYEAR1(I) ; TAB(18) ; "!" ;
501 PRINT#2, X1(I) ; TAB(33) ; "!" ; IYEAR(I) ; TAB(43) ; "!" ; X(I) ;
502 PRINT#2, TAB(55) ; "!" ; I ; TAB(62) ; "!" ;
505 PRINT#2, USING " #.#####" ; P(I) ;
507 PRINT#2, TAB(76) ; "!"
510 NEXT I
520 FOR I=1 TO 76
521 PRINT#2, CHR$(45);
522 NEXT I
524 PRINT#2, CHR$(10) ,CHR$(10),CHR$(10)
526 A$="STATISTICAL ESTIMSATES OF THE"
528 B$="SERIES ARE AS FOLLOWS : "
529 C$=" ORIGINAL "
530 D$=" LOG TRANSFORMED "
531 E$=" POWER TRANSFORMED "
532 MEAN$="MEAN OF THE SERIES = ###.#####^"
534 SSD$ ="STANDARD DEV OF THE SERIES = ###.#####^"
536 SK$ ="COEFF. OF SKEWNESS OF THE SERIES = ###.#####^"
538 SKU$ ="COEFF. OF KURTOSIS OF THE SERIES = ###.#####^"
539 VL$ ="VALUE OF LAMDA = ###.#####^"
541 PRINT#2, A$;C$;B$
542 REM ** COMPUTE MEAN,STANDARD DEVIATION,COEF. OF SKEWNESS
543 REM AND KURTOSIS OF THE GIVEN ORIGINAL SERIES ***
545 FOR I=1 TO 62
546 PRINT#2, CHR$(45);
547 NEXT I
548 PRINT#2,
550 REM CALL STAPS(X(),N,SMEAN,SSD,SKEW,SKUR)
555 GO SUB 3000

```

```

560 AVEGE=SMEAN
570 PRINT#2, CHR$(10);TAB(4);
580 PRINT#2,USING MEAN$;SMEAN
585 PRINT#2, CHR$(10);TAB(4);
590 PRINT#2,USING SSD$;SSD
595 PRINT#2, CHR$(10);TAB(4);
600 PRINT#2, USING SK$;SKEW
605 PRINT#2, CHR$(10);TAB(4);
610 PRINT#2,USING SKU$;SKUR

615 REM ***** FREQUENCY ANALYSIS USING
616 REM LOG TRANSFORMED SERIES *****
625 PRINT#2,CHR$(10);TAB(17);
626 FOR I= 1 TO 41
627 PRINT#2, CHR$(42);
628 NEXT I
629 PRINT#2,
631 PRINT#2,TAB(17);"* ANALYSIS OF THE LOG";TS$
630 TS$ = " TRANSFORMED SERIES *"
640 PRINT#2, TAB(17);
642 FOR I= 1 TO 41
643 PRINT#2, CHR$(42);
645 NEXT I
650 PRINT#2, CHR$(10)
660 FOR I=1 TO 76
665 PRINT#2, CHR$(95);
670 NEXT I
675 PRINT#2,
680 PRINT#2,"!";TAB(9);DC$;TAB(36);DA$;TAB(62);"!";TAB(76);"! "
690 PRINT#2,"!";TAB(9);"!";TAB(19);O$;TAB(33);"!";TAB(42);
691 PRINT#2, O$;TAB(55);"!";TAB(62);P$
695 PRINT#2, S$;
700 FOR I = 1 TO 45
702 PRINT#2, CHR$(45);
704 NEXT I
710 PRINT#2, R$
720 PRINT#2, "!";TAB(9);Y$;TAB(62);EX$
730 FOR I=1 TO 76
732 PRINT#2, CHR$(45);
734 NEXT I
736 PRINT#2,
740 FOR I = 1 TO N
770 Z(I)=LOG(X(I))/LOG(10)
780 Z1(I)=LOG(X1(I))/LOG(10)
782 XX(I)=Z(I)
790 PRINT#2, "! ";I;TAB(9);"! ";IYEAR1(I);TAB(18);"! ";
791 PRINT#2, Z1(I);TAB(33);"! ";IYEAR(I);TAB(43);"! ";Z(I);
792 PRINT#2, TAB(55);"! ";I;TAB(62);"! ";
800 PRINT#2,USING " #.####";P(I);
802 PRINT#2, TAB(76);"! "
805 NEXT I
810 FOR I=1 TO 76
812 PRINT#2, CHR$(45);
813 NEXT I
816 PRINT#2, CHR$(10) ,CHR$(10),CHR$(10)

```

```

820 PRINT#2, A$;D$;B$
825 FOR I=1 TO 69
830 PRINT#2, CHR$(45);
835 NEXT I
838 PRINT#2,

840 REM *** COMPUTATION OF STATISTICAL PARAMETERS OF &
841 THE LOG TRANSFORMED SERIES ***
850 REM CALL STAPS(Z(),N,SMEAN,SSD,SKEW,SKUR)
852 GO SUB 3000
855 PRINT#2, CHR$(10);TAB(4);
860 PRINT#2,USING MEAN$;SMEAN
865 PRINT#2, CHR$(10);TAB(4);
870 PRINT#2,USING SSD$;SSD
875 PRINT#2, CHR$(10);TAB(4);
880 PRINT#2,USING SK$;SKEW
885 PRINT#2, CHR$(10);TAB(4);
890 PRINT#2,USING SKU$;SKUR
892 PRINT#2,CHR$(10)

915 REM ***** COMPUTATION OF CHI-SQUARE &
916 STATISTIC FOR LOG NORMAL FITTING *****
920 REM CALL CHIST(N,NCLASS,Z(),SMEAN,SSD)
922 GO SUB 7000

925 REM ***** COMPUTATION OF PEAKS FOR
926 REM DIFFERENT RECURRENCE INTERVALS *****
930 FOR I =1 TO 6
940 P = 1-1/RI(I)
950 IRI(I)=RI(I)
960 REM CALL PROND(P1,T,D,IE)
965 GO SUB 8000
970 TD(I)=TT
980 ESTP(I)=SMEAN+SSD*TT
990 ESTP(I)=10^ESTP(I)
1000 NEXT I
1010 FP$="ESTIMATED FLOOD PEAKS"
1012 SL$=": SL.NO. : RECURRENCE : ESTIMATED : "
1014 IN$=": INTERNAL : FLOOD : "
1016 J$ =": # : ##### YEARS : #####. : "
1018 PRINT#2, CHR$(10),CHR$(10)
1020 PRINT#2, TAB(30);FP$
1030 PRINT#2, TAB(18);
1032 FOR I = 1 TO 41
1034 PRINT#2, CHR$(95);
1036 NEXT I
1040 PRINT#2,
1042 PRINT#2, TAB(18);SL$
1045 PRINT#2, TAB(18);": ";TAB(28);IN$
1050 PRINT#2, TAB(18);
1051 FOR I = 1 TO 41
1052 PRINT#2, CHR$(45);
1053 NEXT I
1055 PRINT#2,
1056 FOR I = 1 TO 6

```

```

1057 PRINT#2, TAB(18);
1058 PRINT#2, USING J$; I; IRI(I); ESTP(I)
1060 NEXT I
1062 PRINT#2, TAB(18);
1063 FOR I = 1 TO 41
1064 PRINT#2, CHR$(45);
1065 NEXT I
1066 FOR I = 1 TO 4
1067 PRINT#2, CHR$(10);
1068 NEXT I
1069 REM ** FREQUENCY ANALYSIS USING POWER TRANSFORMED SERIES
1070 REM COMPUTATION OF THE VALUE OF EXPONENT WHICH MAKES &
1071 THE SERIES SYMMETRICALLY DISTRIBUTED ***
1072 PRINT#2,
1073 PRINT#2, TAB(16);
1074 FOR I= 1 TO 44
1075 PRINT#2, CHR$(42);
1076 NEXT I
1077 PRINT#2,
1078 PRINT#2, TAB(16); "* ANALYSIS OF THE POWER"; TS$
1079 PRINT#2, TAB(16);
1080 FOR I= 1 TO 44
1081 PRINT#2, CHR$(42);
1082 NEXT I
1083 PRINT#2, CHR$(10)
1085 FOR I = 1 TO 76
1087 PRINT#2, CHR$(95);
1090 NEXT I
1095 PRINT#2,
1100 PRINT#2, "!" ; TAB(9); DC$; TAB(36); DA$; TAB(62); "!" ; TAB(76); "!"
1105 PRINT#2, "!" ; TAB(9); "!" ; TAB(19); O$; TAB(33); "!" ; TAB(42);
1106 PRINT#2, O$; TAB(55); "!" ; TAB(62); P$
1110 PRINT#2, S$;
1115 FOR I = 1 TO 45
1116 PRINT#2, CHR$(45);
1118 NEXT I
1120 PRINT#2, R$
1125 PRINT#2, "!" ; TAB(9); Y$; TAB(62); EX$
1130 FOR I = 1 TO 76
1131 PRINT#2, CHR$(45);
1132 NEXT I
1133 PRINT#2,
1135 AL=1.5
1136 FOR K = 1 TO 3
1137 J = 0
1140 AL = AL-DL(K)
1145 J = J+1
1150 IF(K=2 AND J=10) GO TO 1207
1155 IF(K=3 AND J=10) GO TO 1207
1160 FOR I = 1 TO N
1161 Y(I)=(X(I)^AL-1.)/AL
1162 NEXT I
1163 FOR I = 1 TO N
1164 XX(I)=Y(I)
1165 NEXT I

```

```

1166 REM CALL STAPS(XX(),N,SMEAN,SSD,SKEW,SKUR)
1167 GO SUB 3000
1170 SK(J)=SKEW
1175 IF(ABS(SK(J))<=CKL) GO TO 1217
1180 IF(J=1) GO TO 1140
1185 IF((SK(J)*SK(J-1))<0.0) GO TO 1200
1190 GO TO 1140
1200 AL=AL+DL(K)
1205 NEXT K
1207 AL=AL+10.*DL(K)
1210 FOR I = 1 TO N
1211 Y(I)=(X(I)^AL-1.)/AL
1212 XX(I)=Y(I)
1213 NEXT I
1214 REM *** COMPUTATION OF STATISTICAL PARAMETERS OF
1215 REM THE POWERTRANSFORMED SERIES ***
1216 REM CALL STAPS(XX(),N,SMEAN,SSD,SKEW,SKUR)
1217 GO SUB 3000
1218 FOR I = 1 TO N
1220 Y1(I)=(X1(I)^AL-1)/AL
1230 PRINT#2, "! ";I;TAB(9);"! ";IYEAR1(I);TAB(18);
1231 PRINT#2, ". ";Y1(I);TAB(33);"! ";IYEAR(I);TAB(43);"!";
1232 PRINT#2, XX(I);TAB(55);"! ";I;TAB(62);"!";
1235 PRINT#2,USING " #.####";P(I);
1236 PRINT#2, TAB(76);"!";
1237 NEXT I
1240 FOR I = 1 TO 76
1241 PRINT#2, CHR$(45);
1242 NEXT I
1245 FOR I = 1 TO 4
1246 PRINT#2, CHR$(10)
1247 NEXT I
1248 PRINT#2, A$;E$;B$
1250 FOR I = 1 TO 69
1251 PRINT#2, CHR$(45);
1252 NEXT I
1253 PRINT#2,
1254 PRINT#2, CHR$(10);TAB(4);
1255 PRINT#2,USING VL$;AL
1256 PRINT#2, CHR$(10);TAB(4);
1257 PRINT#2,USING MEAN$;SMEAN
1258 PRINT#2, CHR$(10);TAB(4);
1260 PRINT#2,USING SSD$;SSD
1262 PRINT#2, CHR$(10);TAB(4);
1264 PRINT#2,USING SK$;SKEW
1266 PRINT#2, CHR$(10);TAB(4);
1268 PRINT#2,USING SKU$;SKUR
1269 PRINT#2, CHR$(10),CHR$(10)
1270 REM *** COMPUTATION OF CHI-SQARE STATISTIC FOR
1271 REM POWER TRANSFORMATION FITTING ***
1280 REM CALL CHIST(N,NCLASS,Y(),SMEAN,SSD)
1285 GO SUB 7000

1290 REM *** COMPUTATION OF PEAKS FOR DIFFERENT RECU-
1291 REM RRENCE INTERVALS (WITHOUT KURTOSIS CORRECTION) *

```

```

1300 FOR I = 1 TO 6
1310 ESTP(I)=SMEAN+SSD*TD(I)
1312 ESTP(I)=(ESTP(I)*AL+1.)^(1./AL)
1315 NEXT I
1317 PRINT#2, CHR$(10),CHR$(10),CHR$(10)
1320 PRINT#2, TAB(29);FP$
1330 PRINT#2, TAB(18);
1331 FOR I = 1 TO 41
1332 PRINT#2, CHR$(95);
1333 NEXT I
1335 PRINT#2,
1340 PRINT#2,TAB(18);SL$
1345 PRINT#2,TAB(18);":";TAB(28);IN$
1350 PRINT#2, TAB(18);
1351 FOR I = 1 TO 41
1352 PRINT#2, CHR$(45);
1354 NEXT I
1355 PRINT#2,
1356 FOR I = 1 TO 6
1357 PRINT#2, TAB(18);
1358 PRINT#2,USING J$;I;IRI(I);ESTP(I)
1360 NEXT I
1380 PRINT#2, TAB(18);
1382 FOR I = 1 TO 41
1384 PRINT#2, CHR$(45);
1386 NEXT I
1390 PRINT#2,
1400 CK = SKUR-3.0
1410 XINP=CK

1420 REM *** COMPUTATION OF THE STANDARD NORMAL DEVIATI
1425 REM CORRECTED FOR KURTOSIS DEVIATION AWAY FROM 3.00
1440 NPTS=9
1450 NALPHA=7
1455 FOR I=1 TO 9
1456 XXX(I)=X2(I)
1457 YYY(I)=Y2(I)
1458 NEXT I
1460 REM CALL INPOL(NPTS,XXX(),YYY(),XINP,YINP)
1465 GO SUB 5000
1467 XINP=YINP
1468 FOR I=1 TO 9
1469 XXX(I)=Y2(I)
1470 NEXT I
1475 FOR J = 1 TO NALPHA
1480 FOR I = 1 TO NPTS
1490 REM ALPHAS(I)=ALPHA(I,J)
1495 YYY(I)=ALPHA(I,J)
1497 NEXT I
1500 REM CALL INPOL(NPTS,Y2(),ALPHAS(),YINP,ALINP)
1505 GO SUB 5000
1510 REM ALINPI(J)=ALINP
1515 ALINPI(J)=YINP
1517 NEXT J
1520 PRINT#2, CHR$(10),CHR$(10)

```

```

1700 PRINT#2, "REQUIRED VALUES FOR KURTOSIS CORRECTION ARE:"
1701 FOR I = 1 TO 44
1702 PRINT#2, CHR$(45);
1703 NEXT I
1704 PRINT#2,
1705 PRINT#2, CHR$(10);TAB(4);
1706 PRINT#2,USING "COEFF. OF KURTOSIS      (CK) = ##.##";CK
1710 PRINT#2, TAB(4);
1715 PRINT#2,USING "CORRESPONDING VALUE OF BETA = ##.##";XINP
1720 PRINT#2, CHR$(10);CHR$(10);"KURTOSIS CORRECTED ";
1725 PRINT#2,"STANDARD DEVIATES CORRESPONDING TO THE ";
1726 PRINT#2,"COMPUTED CK "
1730 FOR I = 1 TO 71
1732 PRINT#2, CHR$(95);
1734 NEXT I
1736 PRINT#2,
1740 PRINT#2, "! BETA !";
1745 FOR I = 1 TO 7
1746 PRINT#2, " ALPHA !";
1747 NEXT I
1748 PRINT#2,
1750 PRINT#2, " !";TAB(8);"! 0.25 ! 0.10 ! ";
1751 PRINT#2, " 0.05 ! 0.025 ! 0.01 ! 0.005 ! 0.001 ! "
1760 FOR I = 1 TO 71
1762 PRINT#2, CHR$(45);
1764 NEXT I
1766 PRINT#2,
1770 PRINT#2,
1771 AL$=" #.### !"
1772 PRINT#2,USING " ##.## !";XINP;
1774 FOR I = 1 TO 6
1775 PRINT#2,USING AL$;ALINPI(I);
1776 NEXT I
1778 PRINT#2,USING AL$;ALINPI(7)
1780 FOR I = 1 TO 71
1782 PRINT#2, CHR$(45);
1784 NEXT I
1790 PRINT#2,
1800 REM ***      COMPUTATION OF PEAKS FOR DIFFERENT      &
1805      RECURRENCE INTERVALS (WITH KURTOSIS CORRECTION) **

1810 FOR I = 1 TO NALPHA
1820 PEX1(I)=PEX(I)
1830 ALINPI1(I)=ALINPI(I)
1840 NEXT I
1850 FOR I = 1 TO NALPHA
1860 K = NALPHA-I+1
1870 PEX(I)=PEX1(K)
1880 ALINPI(I)=ALINPI1(K)
1885 NEXT I
1890 FOR I = 1 TO 6
1900 XINP=1./RI(I)
1905 REM CALL INPOL(NALPHA,PEX(),ALINPI(),P1,T1)
1906 FOR J=1 TO 7
1907 XXX(J)=PEX(J)

```

```

1908 NEXT J
1909 FOR J=1 TO 9
1910 YYY(J)=ALINPI(J)
1911 NEXT J
1913 GO SUB 5000
1914 T1=YINP
1915 ESTP(I)=SMEAN+SSD*T1
1920 ESTP(I)=(ESTP(I)*AL+1.)^(1./AL)
1922 NEXT I
1925 PRINT#2, CHR$(10);CHR$(10);TAB(30);FP$
1930 PRINT#2, TAB(21);
1931 FOR I = 1 TO 41
1932 PRINT#2, CHR$(95);
1933 NEXT I
1935 PRINT#2,
1940 PRINT#2, TAB(21);SL$
1945 PRINT#2, TAB(21);":";TAB(31);IN$
1950 PRINT#2, TAB(21);
1951 FOR I = 1 TO 41
1952 PRINT#2, CHR$(45);
1953 NEXT I
1954 PRINT#2,
1956 FOR I = 1 TO 6
1957 PRINT#2, TAB(21);
1958 PRINT#2,USING J$;I;IRI(I);ESTP(I)
1960 NEXT I
1965 PRINT#2, TAB(21);
1970 FOR I = 1 TO 41
1975 PRINT#2, CHR$(45);
1980 NEXT I
2000 GOTO 9000

```

```

3000 REM SUB STAPS(XX(),N,SMEAN,SSD,SKEW,SKUR)
3100 REM -----
3110 REM FOR COMPUTING THE STATISTICAL PARAMETERS OF THE DATA
3120 REM COMPUTES MEAN, STANDARD DEVIATION, COEF. OF
3125 REM SKEWNESS AND COEF. OF KURTOSIS
3140 REM INPUT DATA ARE AS FOLLOWS:
3145 REM =====
3150 REM XX = GIVEN SERIES FOR WHICH STATISTICAL PARAMETERS
3155 REM ARE REQUIRED
3160 REM N = NUMBER OF X VALUES
3170 REM OUTPUT DETAILS ARE AS FOLLOWS:
3175 REM =====
3180 REM SMEAN = MEAN OF THE SERIES
3190 REM SSD = UNBIASED STANDARD DEVIATION OF THE SERIES
3200 REM SKEW = COEFFICIENT OF SKEWNESS OF THE SERIES
3210 REM SKUR = COEFFICIENT OF KURTOSIS OF THE SERIES
3220 REM *****
3310 SUMG=0.0
3320 FOR I= 1 TO N
3322 SUMG=SUMG+XX(I)

```



```

3325 NEXT I
3330 SMEAN=SUMG/N
3335 SUM=0.0
3336 ASUM=0.0
3337 BSUM=0.0
3340 FOR M = 1 TO N
3350 SUM=SUM+(XX(M)-SMEAN)^2
3360 ASUM=ASUM+(XX(M)-SMEAN)^3
3370 BSUM=BSUM+(XX(M)-SMEAN)^4
3380 NEXT M
3390 SSD=SQR(SUM/(N-1))
3400 B=(N*N)/((N-1)*(N-2))
3410 C=(B*N)/(N-3)
3420 SKEW=(ASUM/(SSD^3))*(1/N)
3430 SKEW=SKEW*B
3440 SKUR=(BSUM/(SSD^4))*(1/N)
3450 SKUR=SKUR*C
3460 RETURN

```

```

4000 REM SUB ASCOR(N,IYEAR(),X())
4100 REM -----
4110 REM FOR ARRANGING THE SERIES IN ASCENDING ORDER
4120 REM INPUT DATA ARE AS FOLLOWS:
4125 REM =====
4130 REM N = NUMBER OF VALUES TO BE ARRANGED
4140 REM X = DATA SERIES IN CHRONOLOGICAL ORDER
4150 REM IYEAR = YEAR IN CHRONOLOGICAL ORDER
4160 REM OUTPUT RESULTS ARE AS FOLLOWS:
4165 REM =====
4170 REM X = DATA SERIES IN ASCENDING ORDER
4180 REM IYEAR = YEAR CORRESPONDING TO X
4190 REM *****
4300 J=0
4350 J=J+1
4400 FOR I = J TO N
4450 IF X(I)>X(J) THEN 4800
4500 XT=X(J)
4550 XTY=IYEAR(J)
4600 X(J)=X(I)
4650 IYEAR(J)=IYEAR(I)
4700 X(I)=XT
4750 IYEAR(I)=XTY
4800 NEXT I
4850 IF J<=(N-1) THEN 4350
4900 RETURN

```

```

5000 REM SUB INPOL(NPTS,XXX(),YYY(),XINP,YINP)
5100 REM -----
5110 REM PROGRAMME FOR SPLINE INTERPOLATION
5120 REM NPTS - NO. OF POINTS
5130 REM DIMENSIONS SET FOR DAMAGE CLACULATION IN HEC-1 .
5140 REM ARRAY NAME DIMENSION
5150 REM -----
5160 REM EM , T KPTS=(10*(KRTIO-1)+1)
5170 REM *** COMPUTES SPLINE COEFFICIENTS BY AKIMA METHOD
5172 REM --- A NEW METHOD OF INTERPOLATION AND SMOOTH &
5174 REM CURVE FITTING BASED ON LOCAL PROCEDURE
5176 REM H. AKIMA, J.A.C.M., 17, 589-602, 1970. ***
5180 REM PROGRAM BY H.KUBIK, HYDROLOGIC ENGINEERING CENTER
5185 REM -- AUGUST 1976
5200 REM XXX = X ARRAY, VALUES MUST BE UNIQUE AND INCREASE.
5210 REM YYY = Y ARRAY.
5215 REM NP = NUMBER OF POINTS IN ARRAY.
5220 REM T = COEFFICIENT ARRAY
5230 REM ** IF ONLY TWO POINTS, USE LINEAR INTERPOLATION **
5240 REM *****
5300 KPTS=81
5340 NP=NPTS
5350 IF NP<=2 THEN 5720
5360 IF NP>KPTS THEN 5730
5370 FOR MI = 2 TO NP
5380 MJ=MI
5390 TMP=XXX(MI)-XXX(MI-1)
5400 IF TMP<=0 THEN 5750
5410 EM(MI-1)=(YYY(MI)-YYY(MI-1))/TMP
5420 NEXT MI
5430 FOR MI = 1 TO NP
5440 IF MI=1 THEN 5520
5445 IF MI= 2 THEN 5570
5450 IF MI=(N-1) THEN 5588
5460 IF MI=N THEN 5620
5470 TEMP1= ABS(EM(MI+1)-EM(MI))
5480 TEMP2= ABS(EM(MI-1)-EM(MI-2))
5490 TEMP3= EM(MI-1)
5500 TEMP4= EM(MI)
5510 GO TO 5660
5520 TEMP1= ABS(EM(2)-EM(1))
5530 TEMP2= TEMP1
5540 TEMP3= 2.*EM(1)-EM(2)
5550 TEMP4= EM(1)
5560 GO TO 5660
5570 TEMP1= ABS(EM(3)-EM(2))
5580 TEMP2= ABS(EM(2)-EM(1))
5582 TEMP3= EM(1)
5584 TEMP4= EM(2)
5586 GO TO 5660
5588 TEMP1= ABS(EM(N-1)-EM(N-2))
5590 TEMP2= ABS(EM(N-2)-EM(N-3))
5595 TEMP3= EM(N-2)
5600 TEMP4=EM(N-1)
5610 GO TO 5660

```

```

5620 TEMP1= ABS(EM(N-1)-EM(N-2))
5630 TEMP2= TEMP1
5640 TEMP3= EM(N-1)
5650 TEMP4= 2.*EM(N-1)-EM(N-2)
5660 IF TEMP1 <=0 THEN 5665
5665 IF TEMP2 <=0 THEN 5690
5670 T(MI)=(TEMP3*TEMP1+TEMP4*TEMP2)/(TEMP1+TEMP2)
5680 GO TO 5700
5690 T(MI)=(TEMP4+TEMP3)/2.
5700 NEXT MI
5709 REM CALL AKIM(NPTS,X(),Y(),XINP,YINP,T())
5710 GO SUB 6000
5719 REM CALL AKIM(NPTS,X(),Y(),XINP,YINP,T())
5720 GO SUB 6000
5730 PRINT#3,CHR$(10)
5740 ER1$="** ERROR ** ARRAY SIZE EXCEEDED IN AKIMA,"
5742 ER2$="DIM=,####, BUT NPTS' =,####"
5745 PRINT#3,ER1$;
5747 PRINT#3,USING ER2$;KPTS;N
5750 HE1$="*** ERROR *** X VALUES ARE NOT "
5751 HE2$="UNIQUE, AND/OR INCREASING FOR CUBIC SPLINE"
5752 CU$=" INTERPOLATION MJ="
5754 CU1$="###,XXX(MJ-1)=,#####.##, XXX(MJ)=,#####.##"
5760 PRINT#3,CHR$(10),HE$;CU$;
5765 PRINT#3,USING CU1$;MJ;XXX(MJ-1);XXX(MJ)
5770 RETURN

```

```

6000 REM SUB AKIM(NPTS,XXX(),YYY(),XINP,FUNCT,T())
6100 REM -----
6110 REM *** INTERPOLATION BY AKIMA METHOD.
6115 REM SEE SUBROUTINE AKIMA FOR REF. PROGRAM BY
6120 REM H.KUBIK,HYDROLOGIC ENGG. CENTER - AUG 1976
6220 REM *****
6300 NP=NPTS
6320 XIN=XINP
6340 IF NP<2 THEN 6620
6360 IF NP>2 THEN 6440.
6380 REM USE LINEAR INTERPOLATION IF ONLY TWO POINTS
6400 YINP=YYY(1)+(XIN-XXX(1))/(XXX(2)-XXX(1))*(YYY(2)-YYY(1))
6420 GO TO 6600
6440 FOR II = 2 TO NP
6460 LI=II-1
6480 IF XIN<XXX(II) THEN 6520
6500 NEXT II
6520 TP1=XIN-XXX(LI)
6540 TP2=YYY(LI+1)-YYY(LI)
6560 TP3=XXX(LI+1)-XXX(LI)
6565 FUN1=((3.*TP2)/TP3-2.*T(LI)-T(LI+1))
6570 FUN2=(T(LI)+T(LI+1)-2.*TP2/TP3)
6580 YINP=YYY(LI)+T(LI)*TP1+FUN1/TP3*TP1^2+FUN2*TP1^3/TP3^2
6600 GO TO 6640
6620 PRINT#3,"** ERROR ** ONLY 1 DATA POINT FOR INTERPO."
6640 RETURN

```

```

7000 REM SUB CHIST(N,NCLASS,XX(),SMEAN,SSD)
7100 REM -----
7110 REM SUBROUTINE CHIST FINDS CHI-SQUARE STATISTIC &
7120 ' USING EQUAL PROBABILITY METHOD
7130 REM INPUT INFORMATION ARE AS FOLLOWS:
7135 REM =====
7140 REM XX = THE PEAK FLOOD SERIES
7150 REM N = NUMBER OF XX
7160 REM NCLASS = NO. OF CLASSES USED IN COMPUTING THE
7165 REM CHI-SQUARE STATISTIC
7170 REM SMEAN = MEAN OF THE XX SERIES
7180 REM SSD = STANDARD DEVIATION OF THE XX SERIES
7190 REM NDF = NO. OF DEGREES OF FREEDOM (NCLASS-NO.
7195 REM OF PARAMETERS -1)
7200 REM *****
7360 FOR I=1 TO NCLASS
7380 FL(I)=1/NCLASS ,
7400 EXPF(I)=FL(I)*N
7420 NEXT I
7440 NCLAS=NCLASS-1
7460 FOR I= 1 TO NCLAS
7480 K=I
7500 THFL(I)=K*FL(I)
7520 P=THFL(I)
7540 REM CALL PROND(P,Y,D,IE)
7545 GO SUB 8000
7560 SND(I)=TT
7580 MINP(I)=SMEAN+SSD*SND(I)
7600 OBSF(I)=0.0
7620 NEXT I
7630 TNUM=0.0
7640 J=1
7650 OBSF=0.0
7660 FOR I= 1 TO N
7680 IF (XX(I)-MINP(J))>0 THEN 7760
7700 OBSF(J)=OBSF(J)+1.
7720 TNUM=TNUM+1.
7740 GO TO 7840
7760 IF J<NCLAS THEN 7800
7780 GO TO 7860
7800 J=J+1
7820 GO TO 7680
7840 NEXT I
7860 OBSF(NCLASS)=N-TNUM
7880 REM CALCULATION OF CHI-SQUARE STATISTIC
7885 CHISQ=0.0
7900 FOR I = 1 TO NCLASS
7910 CHIS=(OBSF(I)-EXPF(I))^2/EXPF(I)
7920 CHISQ=CHISQ+CHIS
7935 NEXT I
7940 NDF=NCLASS-3
7950 PRINT#2, CHR$(10);TAB(10);
7955 NCL$="NO. OF CLASS USED (NCLASS) = ####"
7956 NOD$="NO. OF DEGREE OF FREEDOM (NDF)= ####"
7957 CSS$="CHI-SQUARE STATISTIC (CHISQ) = ##.###"

```

```

7960 PRINT#2,USING NCL$;NCLASS
7965 PRINT#2, CHR$(10);TAB(10);
7970 PRINT#2,USING NOD$;NDF
7975 PRINT#2, CHR$(10);TAB(10);
7980 PRINT#2,USING CSS$;CHISQ
7990 RETURN

```

```

8000 REM SUB PROND(P,TT,D,IE)
8100 REM -----
8120 REM COMPUTES  $X=P^{(-y)}$ , THE ARGUMENT X SUCH THAT
8130 REM  $Y = P(X) =$  THE PROBABILITY THAT THE RANDOM
8135 REM VARIABLE U, DISTRIBUTED NORMALLY(0,1), IS  $\leq$ 
8140 REM X. F(X), THE ORDINATE OF THE NORMAL DENSITY,
8150 REM AT X, IS ALSO COMPUTED
8190 REM DESCRIPTION OF PARAMETERS :
8195 REM =====
8200 REM P = INPUT PROBABILITY
8210 REM TT = OUTPUT ARGUMENT SUCH THAT  $P = Y =$  THE
8220 REM PROBABILITY THAT THE RANDOM VARIABLE
8225 REM IS LESS THAN OR EQUAL TO TT
8230 REM C = OUTPUT DENSITY,F(X)
8240 REM IE = OUTPUT ERROR CODE
8250 REM = -1 IF P IS NOT IN THE INTERVAL
8255 REM (0,1), INCLUSIVE
8260 REM TT = C = .99999E+37 IN THIS CASE
8270 REM = C IF THERE IS NO ERROR
8280 REM ***** SEE REMARKS BELOW *****
8290 REM REMARKS - MAXIMUM ERROR IS 0.00045
8310 REM IF P=0,TT IS SET TO  $-(10)**74$ . D IS SET TO C
8320 REM IF P=1,TT IS SET TO  $(10)**74$ . D IS SET TO C
8330 REM SUBROUTINES AND SUBPROGRAMS REQUIRED - NONE
8360 REM METHOD BASED ON APPROXIMATIONS IN C.HASTINGS,
8365 REM "APPROXIMATIONS FOR DIGITAL COMPUTERS",PRINCETON
8370 REM UNIV.PRESS,PRINCETON,N.J.,1955. SEE EQUATION 26.2.23
8375 REM HAND BOOK OF MATHEMATICAL FUNCTIONS,ABRAMOWITZ AND
8380 REM STEGUN, DOVER PUBLICATIONS, INC., NEW YORK.
8410 REM *****
8510 IE=C
8520 TT=0.99999E+37
8530 D=TT
8540 IF P=0 THEN 8590
8545 IF P>0 THEN 8570
8550 IE=-1
8560 GOTO 8720
8570 IF P<1.0 THEN 8620
8580 IF P=1 THEN 8600
8585 IF P>1 THEN 8550
8590 TT=-0.999999E+37
8600 D=0.0
8610 GOTO 8720
8620 D=P
8630 IF D<=0.5 THEN 8660

```

```
8650 D=1.0-D
8660 T2=LOG(1.0/(D*D))
8670 T=SQR(T2)
8680 TT1 = (2.515517+0.802853*T+0.010328*T2)
8682 TT2 = (1.0+1.432788*T+0.189269*T2+0.001308*T*T2)
8685 TT = T-TT1/TT2
8690 IF P>0.5 THEN 8710
8700 TT=-TT
8710 D=0.3989423*EXP(-TT*TT/2.0)
8720 RETURN
9000 END
```

APPENDIX - II

TEST INPUT FOR P.C.

77,8,0.001

50, 100, 200, 500, 1000,10000

0.1,0.01,0.001

1901,1902,1903,1904,1905,1906,1907,1908,1909,1910,1911

1912,1913,1914,1915,1916,1917,1918,1919,1920,1921,1922

1923,1924,1925,1926,1927,1928,1929,1930,1931,1932,1933

1934,1935,1936,1937,1938,1939,1940,1941,1942,1943,1944

1945,1946,1947,1948,1949,1950,1951,1952,1953,1954,1955

1956,1957,1958,1959,1960,1961,1962,1963,1964,1965,1966

1967,1968,1969,1970,1971,1972,1973,1974,1975,1976,1977

11400,9250,7400,8550,9070,7070,7530,11500,8320,11880,6940

8320,3510,9230,7400,4700,8410,4640,6280,8150,9070,7400

5480,19130,9650,3680,7240,3680,4540,6160,3460,6150,5270

9000,5280,3310,3220,3520,2340,2430,3130,6620,4400,4220

5100,4620,4340,4880,3610,6190,4760,3810,5470,6375,4610

6365,4520,4050,5020,3880,4850,5750,6350,4010,2430,4750

5920,3320,5360,6310,5700,4920,7400,5160,3810,6790,5710

TEST INPUT FOR VAX - 11 / 780 COMPUTER

77,8,0.001

50, 100, 200, 500, 1000,10000

0.1,0.01,0.001

1901,1902,1903,1904,1905,1906,1907,1908,1909,1910,1911 &  
1912,1913,1914,1915,1916,1917,1918,1919,1920,1921,1922 &  
1923,1924,1925,1926,1927,1928,1929,1930,1931,1932,1933 &  
1934,1935,1936,1937,1938,1939,1940,1941,1942,1943,1944 &  
1945,1946,1947,1948,1949,1950,1951,1952,1953,1954,1955 &  
1956,1957,1958,1959,1960,1961,1962,1963,1964,1965,1966 &  
1967,1968,1969,1970,1971,1972,1973,1974,1975,1976,1977  
11400,9250,7400,8550,9070,7070,7530,11500,8320,11880,6940 &  
8320,3510,9230,7400,4700,8410,4640,6280,8150,9070,7400 &  
5480,19130,9650,3680,7240,3680,4540,6160,3460,6150,5270 &  
9000,5280,3310,3220,3520,2340,2430,3130,6620,4400,4220 &  
5100,4620,4340,4880,3610,6190,4760,3810,5470,6375,4610 &  
6365,4520,4050,5020,3880,4850,5750,6350,4010,2430,4750 &  
5920,3320,5360,6310,5700,4920,7400,5160,3810,6790,5710



APPENDIX - III : TEST OUTPUT

THE TOTAL NO. VALUES IN THE ORIGINAL SERIES ARE =

NOTE: BLOMS PLOTTING POSITION IS USED THROUGHOUT

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 \* ANALYSIS OF THE ORIGINAL SERIES \*  
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SL.NO.	DATA IN CHRONOLOGICAL ORDER		DATA IN ASCENDING ORDER		RANK	PROBABILITY OF NON-EXCEEDENCE
	YEAR	DISCHARGE	YEAR	DISCHARGE		
1	1901	11400	1939	2340	1	0.0081
2	1902	9250	1965	2430	2	0.0210
3	1903	7400	1940	2430	3	0.0340
4	1904	8550	1941	3130	4	0.0469
5	1905	9070	1937	3220	5	0.0599
6	1906	7070	1936	3310	6	0.0728
7	1907	7530	1968	3320	7	0.0858
8	1908	11500	1931	3460	8	0.0987
9	1909	8320	1913	3510	9	0.1117
10	1910	11880	1938	3520	10	0.1246
11	1911	6940	1949	3610	11	0.1375
12	1912	8320	1928	3680	12	0.1505
13	1913	3510	1926	3680	13	0.1634
14	1914	9230	1975	3810	14	0.1764
15	1915	7400	1952	3810	15	0.1893
16	1916	4700	1960	3880	16	0.2023
17	1917	8410	1964	4010	17	0.2152
18	1918	4640	1958	4050	18	0.2282
19	1919	6280	1944	4220	19	0.2411
20	1920	8150	1947	4340	20	0.2540
21	1921	9070	1943	4400	21	0.2670
22	1922	7400	1957	4520	22	0.2799
23	1923	5480	1929	4540	23	0.2929
24	1924	19130	1955	4610	24	0.3058
25	1925	9650	1946	4620	25	0.3188
26	1926	3680	1918	4640	26	0.3317
27	1927	7240	1916	4700	27	0.3447
28	1928	3680	1966	4750	28	0.3576
29	1929	4540	1951	4760	29	0.3706
30	1930	6160	1961	4850	30	0.3835
31	1931	3460	1948	4880	31	0.3964
32	1932	6150	1972	4920	32	0.4094
33	1933	5270	1959	5020	33	0.4223
34	1934	9000	1945	5100	34	0.4353
35	1935	5280	1974	5160	35	0.4482
36	1936	3310	1933	5270	36	0.4612
37	1937	3220	1935	5280	37	0.4741
38	1938	3520	1969	5360	38	0.4871

39	1939	2340	1953	5470	39	0.5000
40	1940	2430	1923	5480	40	0.5129
41	1941	3130	1971	5700	41	0.5259
42	1942	6620	1977	5710	42	0.5388
43	1943	4400	1962	5750	43	0.5518
44	1944	4220	1967	5920	44	0.5647
45	1945	5100	1932	6150	45	0.5777
46	1946	4620	1930	6160	46	0.5906
47	1947	4340	1950	6190	47	0.6036
48	1948	4880	1919	6280	48	0.6165
49	1949	3610	1970	6310	49	0.6294
50	1950	6190	1963	6350	50	0.6424
51	1951	4760	1956	6365	51	0.6553
52	1952	3810	1954	6375	52	0.6683
53	1953	5470	1942	6620	53	0.6812
54	1954	6375	1976	6790	54	0.6942
55	1955	4610	1911	6940	55	0.7071
56	1956	6365	1906	7070	56	0.7201
57	1957	4520	1927	7240	57	0.7330
58	1958	4050	1973	7400	58	0.7460
59	1959	5020	1922	7400	59	0.7589
60	1960	3880	1915	7400	60	0.7718
61	1961	4850	1903	7400	61	0.7848
62	1962	5750	1907	7530	62	0.7977
63	1963	6350	1920	8150	63	0.8107
64	1964	4010	1912	8320	64	0.8236
65	1965	2430	1909	8320	65	0.8366
66	1966	4750	1917	8410	66	0.8495
67	1967	5920	1904	8550	67	0.8625
68	1968	3320	1934	9000	68	0.8754
69	1969	5360	1921	9070	69	0.8883
70	1970	6310	1905	9070	70	0.9013
71	1971	5700	1914	9230	71	0.9142
72	1972	4920	1902	9250	72	0.9272
73	1973	7400	1925	9650	73	0.9401
74	1974	5160	1901	11400	74	0.9531
75	1975	3810	1908	11500	75	0.9660
76	1976	6790	1910	11880	76	0.9790
77	1977	5710	1924	19130	77	0.9919

STATISTICAL ESTIMATES OF THE ORIGINAL SERIES ARE AS FOLLOWS :

MEAN OF THE SERIES = 60.26884E+02

STANDARD DEV OF THE SERIES = 26.40165E+02

COEFF. OF SKEWNESS OF THE SERIES = 19.35438E-01

COEFF. OF KURTOSIS OF THE SERIES = 99.32779E-01

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 \* ANALYSIS OF THE LOG TRANSFORMED SERIES \*  
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SL.NO.	DATA IN CHRONOLOGICAL ORDER		DATA IN ASCENDING ORDER		RANK	PROBABILITY OF NON-EXCEEDENCE
	YEAR	DISCHARGE	YEAR	DISCHARGE		
1	1901	4.056904	1939	3.369216	1	0.0081
2	1902	3.966142	1965	3.385606	2	0.0210
3	1903	3.869232	1940	3.385606	3	0.0340
4	1904	3.931966	1941	3.495544	4	0.0469
5	1905	3.957607	1937	3.507856	5	0.0599
6	1906	3.849419	1936	3.519828	6	0.0728
7	1907	3.876795	1968	3.521138	7	0.0858
8	1908	4.060698	1931	3.539076	8	0.0987
9	1909	3.920123	1913	3.545307	9	0.1117
10	1910	4.074816	1938	3.546543	10	0.1246
11	1911	3.841359	1949	3.557507	11	0.1375
12	1912	3.920123	1928	3.565848	12	0.1505
13	1913	3.545307	1926	3.565848	13	0.1634
14	1914	3.965202	1975	3.580925	14	0.1764
15	1915	3.869232	1952	3.580925	15	0.1893
16	1916	3.672098	1960	3.588832	16	0.2023
17	1917	3.924796	1964	3.603144	17	0.2152
18	1918	3.666518	1958	3.607455	18	0.2282
19	1919	3.797959	1944	3.625312	19	0.2411
20	1920	3.911158	1947	3.63749	20	0.2540
21	1921	3.957607	1943	3.643453	21	0.2670
22	1922	3.869232	1957	3.655139	22	0.2799
23	1923	3.73878	1929	3.657056	23	0.2929
24	1924	4.281715	1955	3.663701	24	0.3058
25	1925	3.984527	1946	3.664642	25	0.3188
26	1926	3.565848	1918	3.666518	26	0.3317
27	1927	3.859738	1916	3.672098	27	0.3447
28	1928	3.565848	1966	3.676694	28	0.3576
29	1929	3.657056	1951	3.677607	29	0.3706
30	1930	3.789581	1961	3.685742	30	0.3835
31	1931	3.539076	1948	3.68842	31	0.3964
32	1932	3.788875	1972	3.691965	32	0.4094
33	1933	3.721811	1959	3.700704	33	0.4223
34	1934	3.954243	1945	3.70757	34	0.4353
35	1935	3.722634	1974	3.71265	35	0.4482
36	1936	3.519828	1933	3.721811	36	0.4612
37	1937	3.507856	1935	3.722634	37	0.4741
38	1938	3.546543	1969	3.729165	38	0.4871
39	1939	3.369216	1953	3.737987	39	0.5000
40	1940	3.385606	1923	3.73878	40	0.5129
41	1941	3.495544	1971	3.755875	41	0.5259
42	1942	3.820858	1977	3.756636	42	0.5388
43	1943	3.643453	1962	3.759668	43	0.5518
44	1944	3.625312	1967	3.772322	44	0.5647
45	1945	3.70757	1932	3.788875	45	0.5777

46	1946	3.664642	1930	3.789581	46	0.5906
47	1947	3.63749	1950	3.791691	47	0.6036
48	1948	3.68842	1919	3.797959	48	0.6165
49	1949	3.557507	1970	3.80003	49	0.6294
50	1950	3.791691	1963	3.802774	50	0.6424
51	1951	3.677607	1956	3.803798	51	0.6553
52	1952	3.580925	1954	3.80448	52	0.6683
53	1953	3.737987	1942	3.820858	53	0.6812
54	1954	3.80448	1976	3.83187	54	0.6942
55	1955	3.663701	1911	3.841359	55	0.7071
56	1956	3.803798	1906	3.849419	56	0.7201
57	1957	3.655139	1927	3.859738	57	0.7330
58	1958	3.607455	1973	3.869232	58	0.7460
59	1959	3.700704	1922	3.869232	59	0.7589
60	1960	3.588832	1915	3.869232	60	0.7718
61	1961	3.685742	1903	3.869232	61	0.7848
62	1962	3.759668	1907	3.876795	62	0.7977
63	1963	3.802774	1920	3.911158	63	0.8107
64	1964	3.603144	1912	3.920123	64	0.8236
65	1965	3.385606	1909	3.920123	65	0.8366
66	1966	3.676694	1917	3.924796	66	0.8495
67	1967	3.772322	1904	3.931966	67	0.8625
68	1968	3.521138	1934	3.954243	68	0.8754
69	1969	3.729165	1921	3.957607	69	0.8883
70	1970	3.80003	1905	3.957607	70	0.9013
71	1971	3.755875	1914	3.965202	71	0.9142
72	1972	3.691965	1902	3.966142	72	0.9272
73	1973	3.869232	1925	3.984527	73	0.9401
74	1974	3.71265	1901	4.056904	74	0.9531
75	1975	3.580925	1908	4.060698	75	0.9660
76	1976	3.83187	1910	4.074816	76	0.9790
77	1977	3.756636	1924	4.281715	77	0.9919

STATISTICAL ESTIMATES OF THE LOG TRANSFORMED SERIES ARE AS FOLLOWS :

MEAN OF THE SERIES = 37.45347E-01  
STANDARD DEV OF THE SERIES = 17.19228E-02  
COEFF. OF SKEWNESS OF THE SERIES = 23.99446E-02  
COEFF. OF KURTOSIS OF THE SERIES = 34.12415E-01

NO. OF CLASS USED (NCLASS) = 8  
NO. OF DEGREE OF FREEDOM (NDF) = 5  
CHI-SQUARE STATISTIC (CHISQ) = 1.026

ESTIMATED FLOOD PEAKS

SL.NO.	RECURRENT INTERNAL	ESTIMATED FLOOD
1	50 YEARS	12546.
2	100 YEARS	13976.
3	200 YEARS	15426.
4	500 YEARS	17387.
5	1000 YEARS	18909.
6	10000 YEARS	24252.

\*\*\*\*\*  
 \* ANALYSIS OF THE POWER TRANSFORMED SERIES \*  
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SL.NO.	DATA IN CHRONOLOGICAL ORDER		DATA IN ASCENDING ORDER		RANK	PROBABILITY OF NON-EXCEEDENCE
	YEAR	DISCHARGE	YEAR	DISCHARGE		
1	1901	4.385721	1939	4.069888	1	0.0081
2	1902	4.349248	1965	4.078567	2	0.0210
3	1903	4.308681	1940	4.078567	3	0.0340
4	1904	4.335137	1941	4.135209	4	0.0469
5	1905	4.345744	1937	4.141385	5	0.0599
6	1906	4.300175	1936	4.147359	6	0.0728
7	1907	4.311909	1968	4.14801	7	0.0858
8	1908	4.387214	1931	4.156899	8	0.0987
9	1909	4.330198	1913	4.159969	9	0.1117
10	1910	4.392751	1938	4.160578	10	0.1246
11	1911	4.296694	1949	4.165959	11	0.1375
12	1912	4.330198	1928	4.170035	12	0.1505
13	1913	4.159969	1926	4.170035	13	0.1634
14	1914	4.348862	1975	4.177366	14	0.1764
15	1915	4.308681	1952	4.177366	15	0.1893
16	1916	4.220687	1960	4.181192	16	0.2023
17	1917	4.33215	1964	4.188082	17	0.2152
18	1918	4.218085	1958	4.190149	18	0.2282
19	1919	4.277735	1944	4.198672	19	0.2411
20	1920	4.326442	1947	4.204445	20	0.2540
21	1921	4.345744	1943	4.207261	21	0.2670
22	1922	4.308681	1957	4.212759	22	0.2799
23	1923	4.251301	1929	4.213658	23	0.2929
24	1924	4.470094	1955	4.216769	24	0.3058
25	1925	4.356753	1946	4.217209	25	0.3188
26	1926	4.170035	1918	4.218085	26	0.3317
27	1927	4.304615	1916	4.220687	27	0.3447
28	1928	4.170035	1966	4.222825	28	0.3576
29	1929	4.213658	1951	4.22325	29	0.3706

30	1930	4.274034	1961	4.227023	30	0.3835
31	1931	4.156899	1948	4.228263	31	0.3964
32	1932	4.273721	1972	4.229901	32	0.4094
33	1933	4.243594	1959	4.233928	33	0.4223
34	1934	4.344359	1945	4.237083	34	0.4353
35	1935	4.243969	1974	4.23941	35	0.4482
36	1936	4.147359	1933	4.243594	36	0.4612
37	1937	4.141385	1935	4.243969	37	0.4741
38	1938	4.160578	1969	4.246941	38	0.4871
39	1939	4.069888	1953	4.250942	39	0.5000
40	1940	4.078567	1923	4.251301	40	0.5129
41	1941	4.135209	1971	4.259007	41	0.5259
42	1942	4.287783	1977	4.259349	42	0.5388
43	1943	4.207261	1962	4.260709	43	0.5518
44	1944	4.198672	1967	4.266367	44	0.5647
45	1945	4.237083	1932	4.273721	45	0.5777
46	1946	4.217209	1930	4.274034	46	0.5906
47	1947	4.204445	1950	4.274967	47	0.6036
48	1948	4.228263	1919	4.277735	48	0.6165
49	1949	4.165959	1970	4.278648	49	0.6294
50	1950	4.274967	1963	4.279856	50	0.6424
51	1951	4.22325	1956	4.280307	51	0.6553
52	1952	4.177366	1954	4.280607	52	0.6683
53	1953	4.250942	1942	4.287783	53	0.6812
54	1954	4.280607	1976	4.292578	54	0.6942
55	1955	4.216769	1911	4.296694	55	0.7071
56	1956	4.280307	1906	4.300175	56	0.7201
57	1957	4.212759	1927	4.304615	57	0.7330
58	1958	4.190149	1973	4.308681	58	0.7460
59	1959	4.233928	1922	4.308681	59	0.7589
60	1960	4.181192	1915	4.308681	60	0.7718
61	1961	4.227023	1903	4.308681	61	0.7848
62	1962	4.260709	1907	4.311909	62	0.7977
63	1963	4.279856	1920	4.326442	63	0.8107
64	1964	4.188082	1912	4.330198	64	0.8236
65	1965	4.078567	1909	4.330198	65	0.8366
66	1966	4.222825	1917	4.33215	66	0.8495
67	1967	4.266367	1904	4.335137	67	0.8625
68	1968	4.14801	1934	4.344359	68	0.8754
69	1969	4.246941	1921	4.345744	69	0.8883
70	1970	4.278648	1905	4.345744	70	0.9013
71	1971	4.259007	1914	4.348862	71	0.9142
72	1972	4.229901	1902	4.349248	72	0.9272
73	1973	4.308681	1925	4.356753	73	0.9401
74	1974	4.23941	1901	4.385721	74	0.9531
75	1975	4.177366	1908	4.387214	75	0.9660
76	1976	4.292578	1910	4.392751	76	0.9790
77	1977	4.259349	1924	4.470094	77	0.9919

STATISTICAL ESTIMATES OF THE POWER TRANSFORMED SERIES ARE AS FOLLOWS :

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VALUE OF LAMDA = -18.90002E-02  
 MEAN OF THE SERIES = 42.51416E-01  
 STANDARD DEV OF THE SERIES = 77.22943E-03  
 COEFF. OF SKEWNESS OF THE SERIES = -81.22850E-06  
 COEFF. OF KURTOSIS OF THE SERIES = 32.02708E-01

NO. OF CLASS USED (NCLASS) = 8  
 NO. OF DEGREE OF FREEDOM (NDF) = 5  
 CHI-SQUARE STATISTIC (CHISQ) = 1.234

ESTIMATED FLOOD PEAKS

SL.NO.	RECURRENCE	ESTIMATED
:	INTERNAL	FLOOD
1	50 YEARS	13168.
2	100 YEARS	14966.
3	200 YEARS	16872.
4	500 YEARS	19583.
5	1000 YEARS	21797.
6	10000 YEARS	30344.

REQUIRED VALUES FOR KURTOSIS CORRECTION ARE:

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COEFF. OF KURTOSIS (CK) = 0.20  
 CORRESPONDING VALUE OF BETA = 0.10

KURTOSIS CORRECTED STANDARD DEVIATES CORRESPONDING TO THE COMPUTED CK

BETA	ALPHA	ALPHA	ALPHA	ALPHA	ALPHA	ALPHA	ALPHA
:	0.25	0.10	0.05	0.025	0.01	0.005	0.001
0.10	0.649	1.268	1.644	1.985	2.384	2.658	3.223

ESTIMATED FLOOD PEAKS

SL.NO.	RECURRENCE	ESTIMATED
	INTERNAL	FLOOD
1	50 YEARS	13392.
2	100 YEARS	15380.
3	200 YEARS	17561.
4	500 YEARS	21298.
5	1000 YEARS	23326.
6	10000 YEARS	25475.