

CS(AR)-16/98-99

**DAILY RAINFALL-RUNOFF MODELLING USING  
A SIMPLE CONCEPUTAL MODEL FOR  
GUNDLAKAMMA RIVER IN A.P.**



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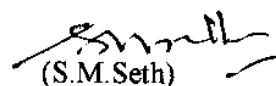
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1998-99**

## PREFACE

Modelling of catchment response using monthly data does not serve the needs of most applications. To use sufficiently, fine data interval to catch the complete temporal variations of observed flows is impossible and impractical. For most of the catchments, daily data are available for both rainfall and flow. Though daily flow data blur many hydrograph features on small and flashy catchments, don't totally hide them.

Conceptual modelling is one way of undertaking hydrological modelling wherein mathematical representation of physical processes is employed with specific inputs to derive the output. Also, it is important to see that the number of parameters of the model is not high to make the modelling process cumbersome. To make the modelling quick and effective, conceptual models with a few parameters are being preferred. Fewer parameters means quicker optimization and simpler application to any basin.

In this study, a simple 5-parameter model based on the concept of probability distributed method as proposed by Moore (1985) is applied to undertake modelling of the daily runoff over a 9 year period of 1989 to 1997 at Tammavaram in Prakasam district of Andhra Pradesh on the Gundlakamma river. A program in Fortran 77 is developed to undertake automatic optimization of the model to simulate the observed flows using appropriate objective function. This study was undertaken by Mr. S.V.Vijaya Kumar, Scientist 'C' and Mr. U.V.N.Rao, S.R.A., as part of technical work plan of Deltaic Regional Centre, Kakinada. Dr. S K Mishra, Scientist 'E' reviewed this report.



(S.M. Seth)

Director

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## **Abstract**

Since 1990's, some new techniques are being applied more widely in solving analytical problems of rainfall-runoff modelling on the readily accessible personal computers. Utilizing the concepts of physics to describe the land phase of hydrological cycle in space and time and computing facilities available hydrological modelling is being made easy and simple. It is important to see that the number of parameters of the model is not so large that modelling the process becomes cumbersome. To make the modelling quick and effective, conceptual models with a few parameters are being preferred.

In this study, a simple 5-parameter model; based on the conceptual of probabilitydistributed method as proposed by Moore (1985) is applied to simulate the daily runoff over a 9-year period of 1989 to 1997 at Tamavaram in Prakasam district of Andhra Pradesh on the Gundlakamma river. A program in Fortran 77 is developed to undertake automatic optimization of the model to simulate the observed flows using a proper objective function. From the calibration and validation of the modelling study, it is found that the model, though a five-parameter one, could respond properly to the rainfall and resulted in a reasonable by efficiency of 72.14% in calibration and 68.25% in validation

## **INTRODUCTION**

Hydrologists are concerned with developing a proper relationship between the rainfall over a catchment and the resulting runoff at the catchment outlet. The link between rainfall and runoff has inspired many research workers and the evaluation of river flow from rainfall has stimulated the imagination and ingenuity of engineers. The availability of high-speed digital computers with large storage for data is now an added advantage. Since 1990's, some new techniques are being applied more widely in solving analytical and numerical engineering problems on the readily accessible personal computers. Utilizing the concepts of physics to describe the land phase of hydrological cycle in space and time and the computing facilities available, hydrological modelling is made easy and simple. Conceptual modelling is one way of undertaking hydrological modelling wherein mathematical representation of physical process is employed with specific inputs to derive the output. Also, it is important to see that the number of parameters of the model is not so large that modelling the process becomes cumbersome. To make the modelling quick and effective, conceptual models with a few parameters are being preferred. "Fewer parameters" means quicker optimization and simpler application to any basin.

### **1.1 Hydrological Modelling**

Hydrological models can be classified in many ways. Depending upon the phenomenon of importance, they are classified as event-based models i.e., to simulate a flood peak resulting due to a single or multiple storm events or continuous models i.e., to simulate the flow processes over a season or over a number of years preferably to develop rainfall-runoff relationships on daily basis. The other classification is based on the mathematical theory being applied and are classified as 'deterministic' models which seek to simulate the physical processes in the catchment wherein rainfall gets transformed into runoff or 'stochastic' models wherein the hydrological time series of single or several variables such as rainfall, evaporation, stream flow etc., involving distribution in probability are applied. Also, a combined or hybrid models wherein both deterministic and stochastic approaches are selectively being employed are proving to be more successful.

## **1.2 Conceptual models :**

It is well known that the movement of water in the land phase of hydrologic cycle is a complex process involving the sub-processes of interception, infiltration, percolation, surface runoff, sub-surface runoff, interflow, baseflow etc., To put it simply the hydrology of a drainage basin, from precipitation through to the stream discharge at the point of interest can be conceived as a series of inter-linked processes of inflows, storages and outflows. In conceptual modelling the catchment processes are described mathematically, and storages are considered as reservoirs for which water budgets are kept. Many conceptual catchment models have been developed over the past. Dawdy and O'Donnell (1965) described the structure and operation of a conceptual model. Nash and Sutcliffe (1970) discussed the principle of river flow forecasting through conceptual models. Blackie and Eeles (1985) discussed in detail about lumped catchment models and parameter optimization for hydrological forecasting.

## **1.3 Simple conceptual models :**

To model catchment response using monthly data would not serve the needs of most of the applications. To use sufficiently fine data interval to catch all the variations of observed flows would be impossible and impractical. For most of the catchments daily data are available for both rainfall and flow. Though daily flow data blur the many hydrograph features on small and flashy catchments, the data don't totally hide them. Daily rainfall and runoff models are fairly commonly used either for generating the flows or for operational purposes, as required. These models try to reproduce the catchment response, as closely as possible, so that they can be used to generate long sequences of flows from rainfall data or show how changes in the catchment may affect runoff. For a good simulation a model and its parameters provide a description of how the catchment responds. A near perfect simulation requires a large number of model parameters. To simulate the model adjusting these parameters either by trial and error may be impossible or by automatic optimization may be computationally difficult. So, a near perfect simulation of observed flows may not be as important as obtaining a response hydrograph that has general features as the observed flows. Relaxing the goodness of fit criteria may enable much more simple models to be used (Bonvoisin & Boorman, 1992). A reasonable number of model parameters are probably around 3 to 5 which should allow adequate simulation, enable fairly confident parameter estimates to be made, ensure no parameters

are redundant, provide parameters that have readily understandable functions and hence parameter values that describe major catchment effects.

In this study, a simple 5-parameter model, based on the concept of probability distributed method as proposed by Moore (1985) is applied to simulate the daily runoff over a 9 year period of 1989 to 1997 at Tammavaram in Prakasam district of Andhra Pradesh on the Gundlakamma river. The better performance of the model in the daily rainfall-runoff modelling studies on the Nagavali and the Sarada rivers conducted by Vijayakumar (1995) earlier has encouraged in applying it to this basin too.

## 2.0 MODEL DESCRIPTION

As mentioned earlier, simple conceptual models are being adopted to simulate daily rainfall runoff now a days. The models consist of a number of stores with model parameter controlling the store sizes and rate of outflows. They use the conceptualization of flow processes with inputs of daily rainfall and pan evaporation to generate runoff. The main components of a model in general are

\_\_\_\_\_ a procedure to determine actual evaporation from potential evaporation, derived from pan evaporation or any other methods. The ratio of actual evaporation to potential evaporation is generally taken to be a function of the water content of one of the soil moisture stores. Some models use a linear function i.e., a linear decline in evaporation as soil moisture content falls below some maximum, whilst others use a negative exponential function i.e., the ratio of AE to PE falls slowly at first, but more rapidly as the store empties.

\_\_\_\_\_ a storage accounting procedure to determine the water content of each soil moisture store. Store content at the end of a time step is based on the content at the beginning of the step and on inflow and outflow during the step. The outflow from one store is generally the inflow to another store. Different models have different procedures for determining outflows, usually within prescribed limits e.g. some stores can overflow while others can only drain downwards. Models have different number of stores, which may be combined in different ways.

\_\_\_\_\_ a runoff generation procedure. This is either as direct surface flow or a baseflow. The former is usually through a saturation excess or infiltration excess model, and the latter as a function of the soil moisture store content.

\_\_\_\_\_ a procedure to route the outflow from appropriate soil moisture stores into flow in the river. This is usually, based on a system of linear reservoirs, one from each store.

The 5-parameter model used in this study employing the above procedure is described in detail here. The schematic diagram of the model is shown in Fig.1. The model is based on Moore's probability distributed technique (Moore, 1985) and has a soil moisture store with a capacity varying across the basin and a groundwater store. Vijayakumar (1995) applied 5 such simple daily rainfall-runoff models for the Nagavali and for the Sarada catchments along the east coast of India and observed the performance of the 5 parameter model as very efficient. The model is being widely used in flood forecasting (Moore et. al 1990, Moore & Jones, 1991 and Moore 1993). In the model distribution of the soil capacity, C, is represented by the reflected power (or pareto) distribution.

$$F(c) = 1 - 1(1-C/C_{max})^b \text{ for } 0 \leq C \leq C_{max}. \quad \dots \quad 2.1$$

Where 'Cmax' is the maximum storage capacity at any point within the basin and 'b' is a dimensionless parameter, which defines the degree of spatial heterogeneity. The maximum amount of water that can be held in storage in the basin, 'Smax', for the reflected power distribution is

$$\begin{aligned} S_{max} &= \int_0^{C_{max}} (1-F(c)).dc \quad \dots \quad 2.2 \\ &= C_{max}/(b+1) \quad \dots \quad 2.3 \end{aligned}$$

In the model, precipitation is added to the soil moisture and excess precipitation becomes direct runoff which is routed through two cascading linear reservoirs as direct runoff. Evapotranspiration from the soil moisture store occurs at a rate proportional to store contents, as does drainage from the soil moisture store. Baseflow occurs from the groundwater store and is added to the direct runoff to becomes the catchment outflow.

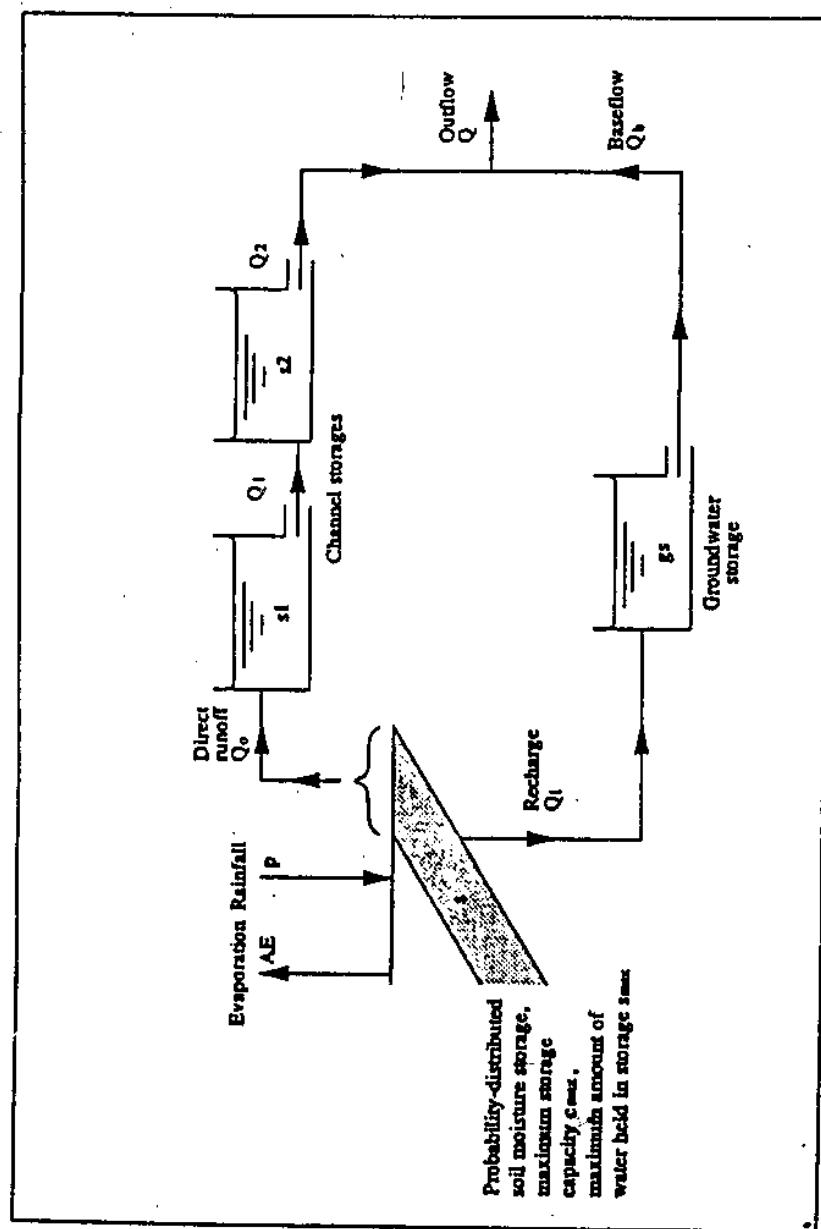


Fig.01 Schematic diagram of the 5 parameter model

The model has five parameters. The maximum storage capacity at any point within the basin ‘Cmax’; the average maximum amount of water that could be held in storage over the whole basin ‘Smax’, a soil drainage coefficient ‘Kb’, a groundwater discharge coefficient ‘Ground’ and a channel routing coefficient ‘Srout’. The model formulation and the accounting procedure is discussed in detail by Houghton-carr and Arnell (1994) and is briefly presented here:

Actual evapotranspiration (AE) is derived from potential evapotranspiration (PE) as

$$AE_t = PE_t \{ 1 - e^{(-6.68 S_{t-1}/Smax)} \} \quad \dots \quad 2.4$$

Drainage to the Groundwater store is

$$Qi = Kb(S_{t-1}/Smax) \quad \dots \quad 2.5$$

If rainfall P is less than AE and Qit there is no direct runoff. Otherwise direct runoff does occur. The critical capacity at the end of previous time step ‘Cc’ below which all the soil moisture goes to storage is calculated from the reflected power (pareto) distribution as

$$Cc_{t-1} = Cmax \{ 1 - (1 - S_t/Smax)^{1/(b+1)} \} \quad \dots \quad 2.6$$

Hence critical capacity at the end of the present time step is

$$Cc_t = Cc_{t-1} + (P_t - AE_t - Qi_t) \quad \dots \quad 2.7$$

If Cct is less than Cmax, direct runoff is

$$Qo_t = (P_t - AE_t - Qi_t) - Smax \{ 1 - Cc_{t-1}/Cmax \}^{b+1} - (1 - Cc_t/Cmax)^{b+1} \quad \dots \quad 2.8$$

If Cct is greater than Cmax, direct runoff is

$$Qo_t = (P_t - AE_t - Qi_t) - (Smax - S_{t-1}) \quad \dots \quad 2.9$$

and the soil moisture store is full to Smax.

Baseflow (Qb) from groundwater storage gs is

$$Qb_t = Grout (S_{t-1}/100) \quad \dots \quad 2.10$$

Direct runoff through two cascading reservoir of storage Ss made routed as

$$Q = Srout (S_s) \quad \dots \quad 2.11$$

Adding the baseflow ‘Qb’ and direct runoff ‘Q’ results in the modelled catchment runoff, which can be compared with the observed runoff at the point of interest.

## 2.1 Optimization

With a model, for any given of parameter set values, one can estimate modelled flows using input data like, rainfall, evaporation etc., The job of the modelling is to recommended best set of parameters which will closely simulate the observed flows at the particular point of interest on the stream. It can be accompanied either by trial and error or by automatic optimization of the parameter set. There are many criteria to undertake modelling. One technique is by plotting both observed and modeled and selecting the parameters, which give visually better fit. Another one is a numerical technique, in which the parameters are subjected to automatic optimization to achieve a mathematically best fit, indicated by an objective function. Hence the objective function is regarded as a tool to aid fitting and assess the model. If proper limits for parameter set are chosen, this criteria generally results in visually better fit too. In daily rainfall – runoff modelling the following two functions are used as fitting criteria as error functions.

The first objective function is to maximize the sum of the squares of difference of the observed and simulated daily flow during the entire period of simulation i.e.

$$\text{Minimize } \text{Obj1} = \sum (Q_{\text{obs}} - Q_{\text{sim}})^2 \quad \dots \quad 2.1.1$$

Which may give a good fit for long periods of low flows.

The second objective function is to minimize the sum of squares of difference of the logarithm of the observed and simulated daily flows i.e.

$$\text{Minimize } \text{Obj2} = \sum (\log Q_{\text{obs}} - \log Q_{\text{sim}})^2 \quad \dots \quad 2.1.2$$

This objective function prevents the optimization becoming bassed towards larger flows. This function may not be useful when there are no flows during most part of the year.

To undertake automatic optimization Rosenbrock (1960) optimization procedure was invoked to minimize the objective function. The objective function may be used to compare the results from calibration and validation data sets.

## 2.2 Normalization

Objective function values as explained above are not comparable across different catchments, since they are not normalized. Hence, a suitable technique like NashSutcliffe (1970) efficiency criteria may be used to undertake normalization. The normalization function as per above criteria is

$$\text{Obj3} = \text{Efficiency} = 1.0 - \text{Obj1} / \sum (Q_{\text{obs}} - Q_{\bar{\text{bar}}})^2 \quad \text{-----2.2.1}$$

Where Obj1 is objective function one as defined above. The denominator is the sum of the square of differences of the daily observed and observed mean daily flow over the period of modelling. Since the objective function one is minimized in the optimization criteria the equation 2.2.1 gives maximum efficiency. The efficiency criterion is biased towards larger discharges, but is widely used and gives an objective indication of model performance. A perfect agreement between the observed and simulated flows yields an efficiency of 1.0, whilst a negative efficiency represents a lack of agreement, worse than if the simulated flows were replaced with the observed mean daily flows.

### **3.0 STUDY AREA :**

The Gundlakamma river basin is a medium river of about 264 kms length taking its origin from the Nallamalai hills in Mallamalai forest near Gundla brahmeswaram village, Longitude 76046'E and Latitude 15040'N in Nandyal taluka of Kurnool district at altitude of 680 metres. It flows through deep ravines and thickly grown natural forests and hilly tracts upto Cumbum tank situated in Cumbum village in Prakasam district. The river flows generally in northeast direction upto the confluence of Konduleru river, then takes a turn towards east upto the confluence of Konkeru at Pittambanda village. It turns southeast and flows at a uniform slope till it joins Bay of Bengal near Pallipalem village. The river's total catchment area is 8195 km<sup>2</sup>, including the area drained by its tributaries. Jamaleru, Venumuleru, Mekaleru, Teegaleru, Duvvaleru, Rallavagu, Konduleru, Pasupaluru, Konkeru, Chilakaleru, Voleru etc., The Gundlakamma basin is bounded by Vogeru vagu, Romperu on East side, by Nallamalai hill range on the western side, Krishna basin on the northern side and Musi river basin on the southern side and flowing eastwards into Bay of Bengal.

About 50 km from its source, the Gundlakamma receives the waters of the tributary Jampaleru from the eastern side of the Eastern ghats and joins on left side of Gundlakamma. About 52 km from this point Gundlakamma receives waters from Teegaleru from western side. After another 6.4 km it meets Rallavagu from westwards. After 17.6 km from this point it receives Konduleru from the north. After 25.6 km from

Teegaleru from western side. After another 6.4 km it meets Rallavagu from westwards. After 17.6 km from this point it receives Konduleru from the north. After 25.6 km from this confluence it receives waters from Konkeru river from North. About 49 km from the mouth, it is joined by Chilakaleru. Mixed red and black soils on upper reaches, red sandy soils in the middle part and a mixture of coastal alluvium and coastal sandy soils in the lower reaches.

### **3.1 Drainage**

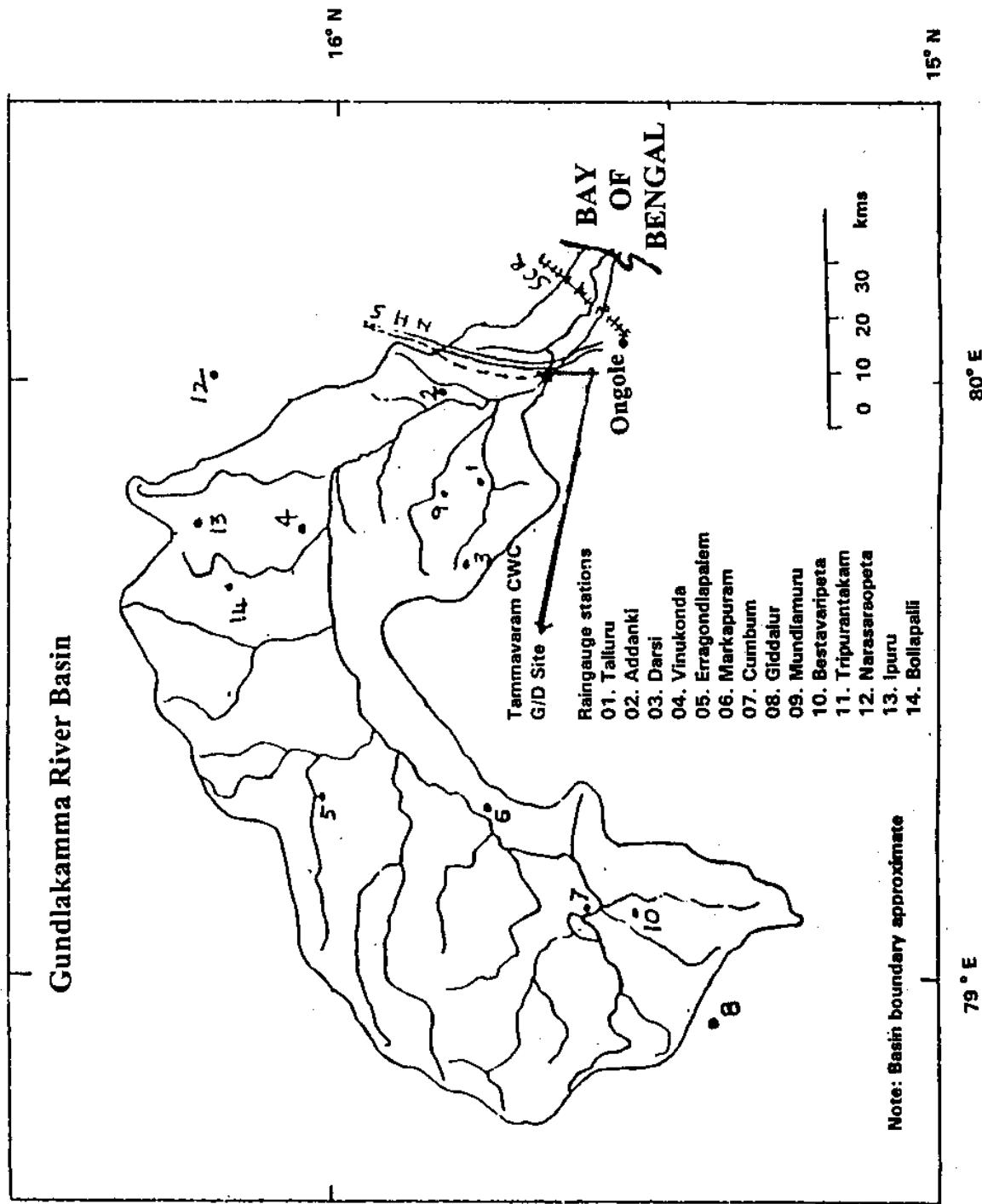
The Gundlakamma river originates and initially flows over different formations of Cuddapah super group which occupies more than half of the basin. From about Vinukonda onwards the river cuts across the rocks and enters the coastal plains. The predominant drainage patterns in the Gundlakamma are parallel, sub-parallel, radial and peripheral. The annular drainage is observed around dome structures of Eshwarakuppam, Vellatur and Ipur. In the northern part of Yandrapalli and around Darsi dendritic patterns are observed. The important physiographic features of the basin are Nallamalai Range, Sagileru Valley, Veligonda range, Nellore payanghat (Pediment low land), East Coastal Plain, Palco-channels and palco beaches (ancient beach ridges). The Gundlakamma is a 9<sup>th</sup> order stream according to Strahler's classification according to Rao & Babu (1995). The main tributaries of the Gundlakamma are, the Ralla Vagu, the Mekaleru the Vemuleru, the Jampaleru, the Tegaleru, the Konduleru, the Duvvaleru. The basin has an 'axe' shape (Fig.2). The maximum length of the crescent shaped basin is 201 km and maximum width is 91.73 km in the middle. From source upto 29<sup>th</sup> km the gradient is 23.675 m/km. There are three falls in bed level in this stretch. From 29<sup>th</sup> km to the mouth the gradient is 7.136 m/km. The catchment area upto Tammavaram G/D site is about 7831 sq.km.

During monsoon season Gundlakamma occasionally swells into floods. The maximum flow recorded at CWC G/D site at Tammavaram is 3607 cumecs and minimum flow recorded is 0.10 cumecs.

### **3.2 Climate :**

The Climate of coastal part of the study area may be broadly classified under tropical coastal type and rest is of steppe type. According to Koppan the climate is tropical Savannah in upper part and dry season in high sun period in the rest of the area. The daily mean temperature is about 27.5 0C. Mean maximum temperature is around 32.5 0C.

**Fig. 02** Basin map of the Gundlakamma river



Mean minimum temperature is about 22.5 °C. Highest maximum temperature is about 47 °C and lowest minimum temperature is about 14 °C. The mean diurnal range of temperature is about 10 °C.

A rainfall of 25 mm between January and February; about 75 mm between March to May; about 400 mm between June to September and about 300 mm between October to December is experienced in the area. Annual rainy days are about 40, Southwest Monsoon is set during 1<sup>st</sup> week of June and retreats by middle of November, normally. The annual runoff is about 200 mm. Also the area under study gets heavy rainfall due to cyclones forming in Bay of Bengal.

#### **4.0 DATA**

As mentioned earlier, the modelling study is a data driven application. The more the recorded data on various observations such as rainfall, flows and evaporation, the more realistic the success of modelling.

##### **4.1 Rainfall data:**

Daily rainfall from 10 stations in Prakasam district and 4 stations in Guntur district totalling to 14 stations from 1<sup>st</sup> January 1989 to 30<sup>th</sup> November 1997 are collected in consequence to the availability of flow records at Tammavaram site of Central Water Commission. The location of raingauge stations used in the study are shown at Fig.2. The details rainfall data used and the respective Thiessen's Weights adopted are shown at Annexure – I.

##### **4.2 Flow data:**

The mean daily flow data is measured using current meter at Tammavaram site. Due to reasons unknown, only gauge readings are available over some days and some time during extraordinary floods. In such cases estimated flow from stage discharge relations are substituted. The details of streamflow records at Tammavaram CWC site used in the study is at Annexure – I. The catchment area upto the site is about 7831 sq.km.

##### **4.3 Evaporation Data:**

Efforts were made to collect evaporation data representative of the basin. The agriculture research station, ANGRAU at Darsi has provided the Pan evaporation data for about 3 years period. This data is used to estimate average daily mean monthly Pan evaporation data as shown at Table .1 and is utilised in the modelling study.

Table .1 Average daily mean monthly Pan evaporation data (mm/day) at ARS, Darsi.

Month	Jan	Feb	Mar	Apr	May	June
Evaporation (mm)	3.233	4.40	5.667	5.80	9.60	9.90
Month	July	Aug	Sep	Oct	Nov	Dec
Evaporation (mm)	7.133	5.267	5.00	3.25	3.20	2.667

## 5.0 ANALYSIS & RESULTS

In the present study, an attempt is made to simulate the daily rainfall-runoff for the Gundlakamma river in Prakasam district of Andhra Pradesh at Tammavaram CWC and Gauge Discharge site. The period of study is from 1989 to 1997. Data of the first 5 year period of 1<sup>st</sup> January, 1989 to 31<sup>st</sup> December, 1993 is used for calibration of the model and the data of later 4 year period of 1<sup>st</sup> January, 1994 to 30<sup>th</sup> November, 1997 is used for validation of the calibrated model. The details of analysis and results are presented here.

### 5.1 Analysis

Rainfall data for 14 stations within and near the catchment is used to derive the basin average rainfall using the Theissen method. This procedure distorts the original rainfall intensity pattern if the rainfall distribution is not uniform over the entire catchment. The effect of storms uniformly distributed over the catchment can be simulated properly. Thus, the spatial averaging brings in certain error into the modelled flows if storms are not uniformly distributed. It is noticed that there are some rainfall events which recorded high rainfall in some parts and low rainfall at some other parts. Such local storm events of heavy intense rainfall on the lower reaches of catchment resulted in high-observed discharges, which were difficult to be simulated properly with the lumping of data, as the storms are not uniformly distributed over the catchment.

Average daily flow data as recorded at the Tammavaram CWC G/D site is used in the study. The discharge data was analysed and processed as for some days gauge data was only recorded. This has been undertaken mainly using rating curve information. It is noticed that during 24<sup>th</sup> and 25<sup>th</sup> September, 1997 discharges as high as 2348 cumecs and 2697 cumecs were measured which are not in consonance with the basin average rainfall

of 45mm and 86 mm. As stated earlier, this is due to local high intense rainfall events within the catchment and is difficult for any lumped model to simulate perfectly. Compared to calibration data set, validation data set has more such events. It is to be mentioned here that such events have an effect on the value of objective functions and thus on efficiency of the model.

The daily mean monthly evaporation is worked out from the observed data from December 1995 to August 1998, provided by Agricultural research station of ANGRAU at Darsi within the study area. Daily mean monthly evaporation data with a Pan Coefficient of 0.7 is used in the model to evaluate the potential evaporation, which in turn is used to estimate actual evapotranspiration as explained in the earlier section. This daily mean monthly data is used for the entire period of modelling. It is assumed that this information of evaporation at Darsi station represents the whole basin.

## **5.2 Calibration**

As the modelling procedure requires information on catchment data, rainfall, flow and evaporation data, respective data files were prepared for the 5-year period. The number of parameters to be optimized in the model and the maximum number of iterations of optimization are also to be specified. On successful completion of the optimization run the program gives the objective function value, the efficiency value, the modelled daily flows and the monthly flows. The program may be extended to validation part of the study by specifying the period of validation in the catchment file to obtain the results for validation data set. In the present case the optimization resulted in the best parameter set as listed at Table 2 for the first objective function.

Table.2 Best Model Parameter Set for Gundlakamma at Tammavaram

Parameter	Parameter Name	Value
1	Cmax	394.4653
2	Smax	260.8219
3	Kb	1.388142
4	Ground	1.158575
5	Srount	0.597486

The objective function obj-1 resulted is 382.0793 and the efficiency is 72.14%. The resulting simulated daily runoff along with observed runoff and spatial average rainfall are listed at Annexure – II. The monthly modelled and observed runoff is shown in Table.3. The modelled runoff over the entire 5-year period of calibration is presented at Fig.3. The same is shown year wise from Fig.4 to 8. The modelled and observed monthly runoff for calibration period is shown as Bar Chart in Fig. 9. As 1989 is first year of the run and is used for warming of the model simulated flows are different from the observed flows. The efficiency and the response of the modelled runoff to the rainfall as observed visually from the figures plotted suggested that the model could simulate the flows reasonably well. The peaks could not be simulated satisfactorily.

### 5.3 Validation

With the parameter set optimized from the calibration run, the program is extended to validate the model by specifying the 4 year period of validation from 1994 to 1997 and the respective data files for rainfall, evaporation and baseflow. The validation resulted in an efficiency of 68.25% which is close to the efficiency obtained for the calibration run. The model response to the rainfall pattern in general is proper as observed from the modelled and observed runoff plots. The model could not simulate the peak flows properly may be due to error because of lumping the rainfall, which is common with any lumped model. The modelled and observed daily runoff for the entire validation period is plotted at Fig.10 and for individual years it is plotted from Fig. 11 to 14. The simulated and observed runoff along with spatial rainfall is presented at Annexure – III and the monthly runoff in Table 4. The modelled and observed monthly runoff values for validation period is shown

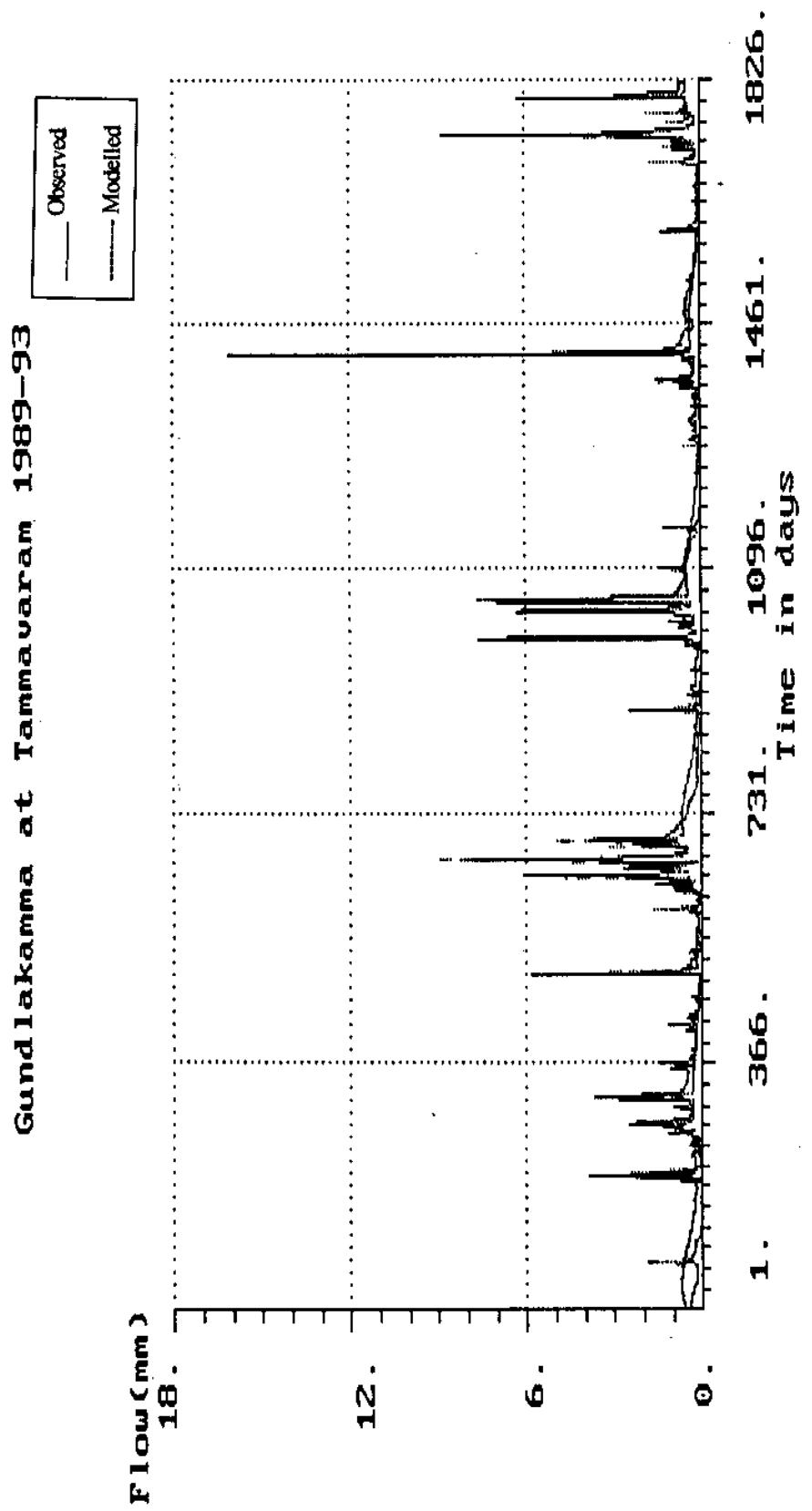


Fig.03 Modelled and observed daily flow hydrograph for calibration

Gundlakamma at Tammavaram 1989

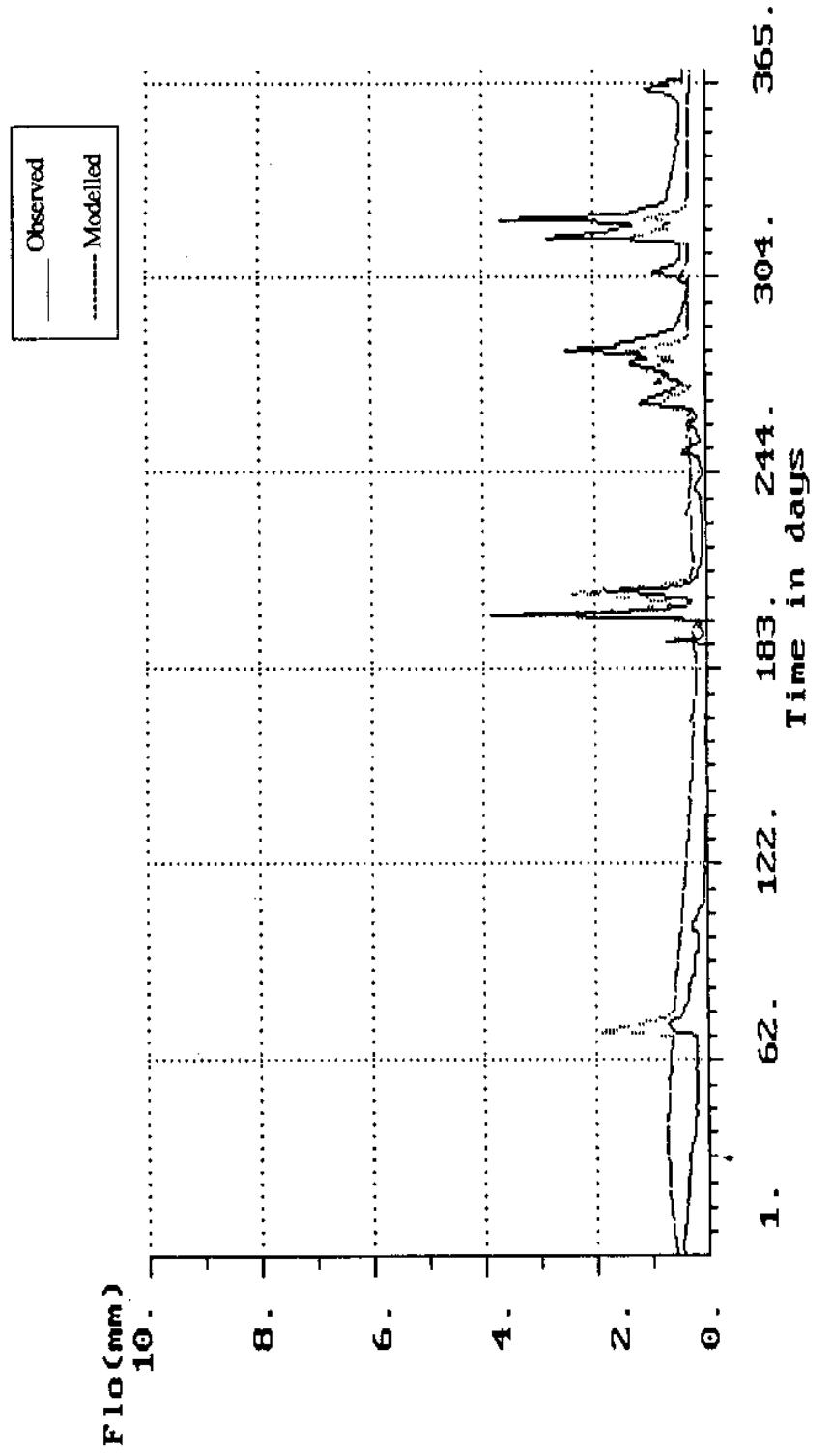
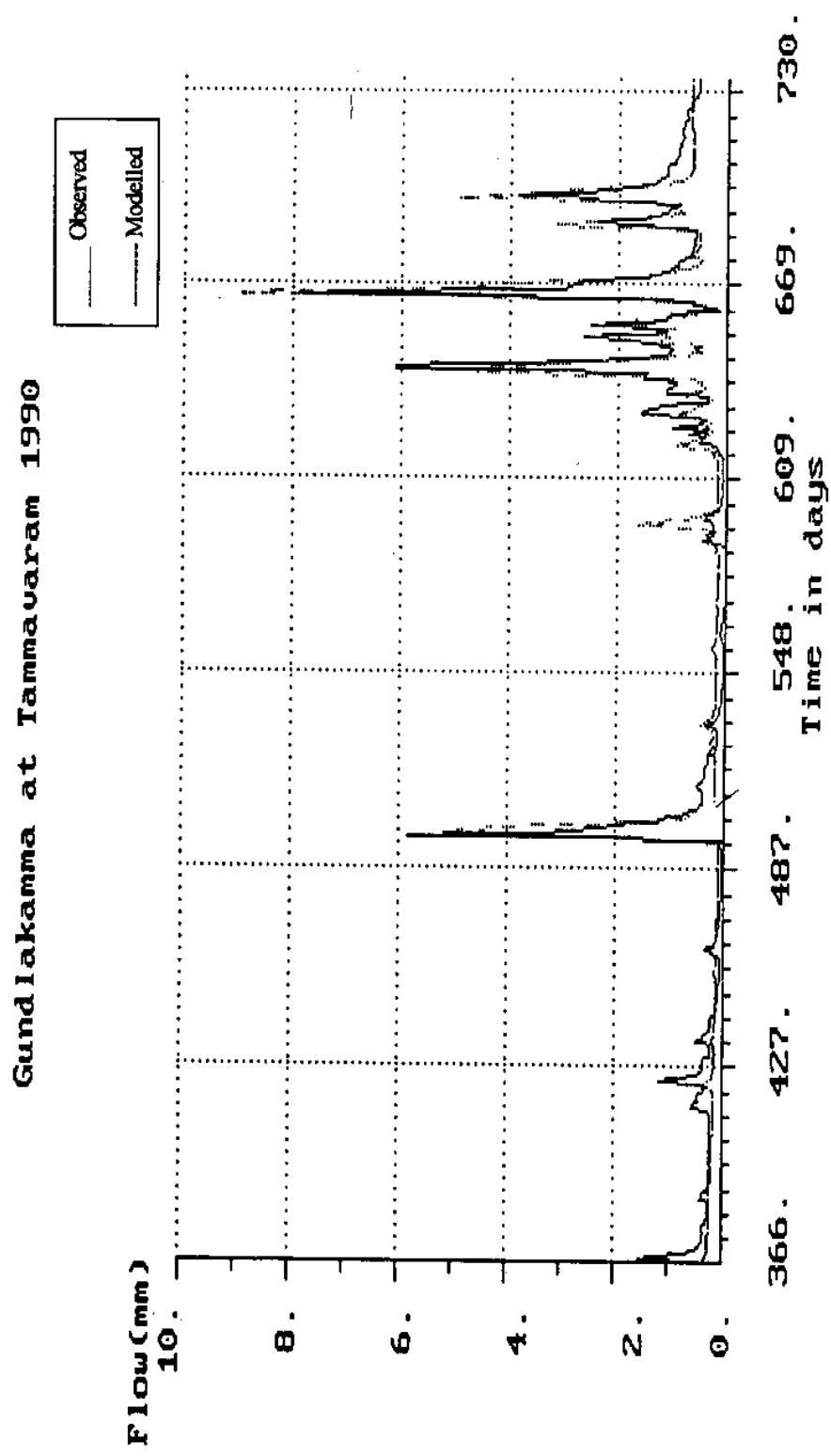


Fig.04 Modelled and observed daily flow hydrograph for 1989



**Fig.05** Modelled and observed daily flow hydrograph for 1990

Gundlakamma at Tammavaram 1991

— Observed  
- - - Modelled

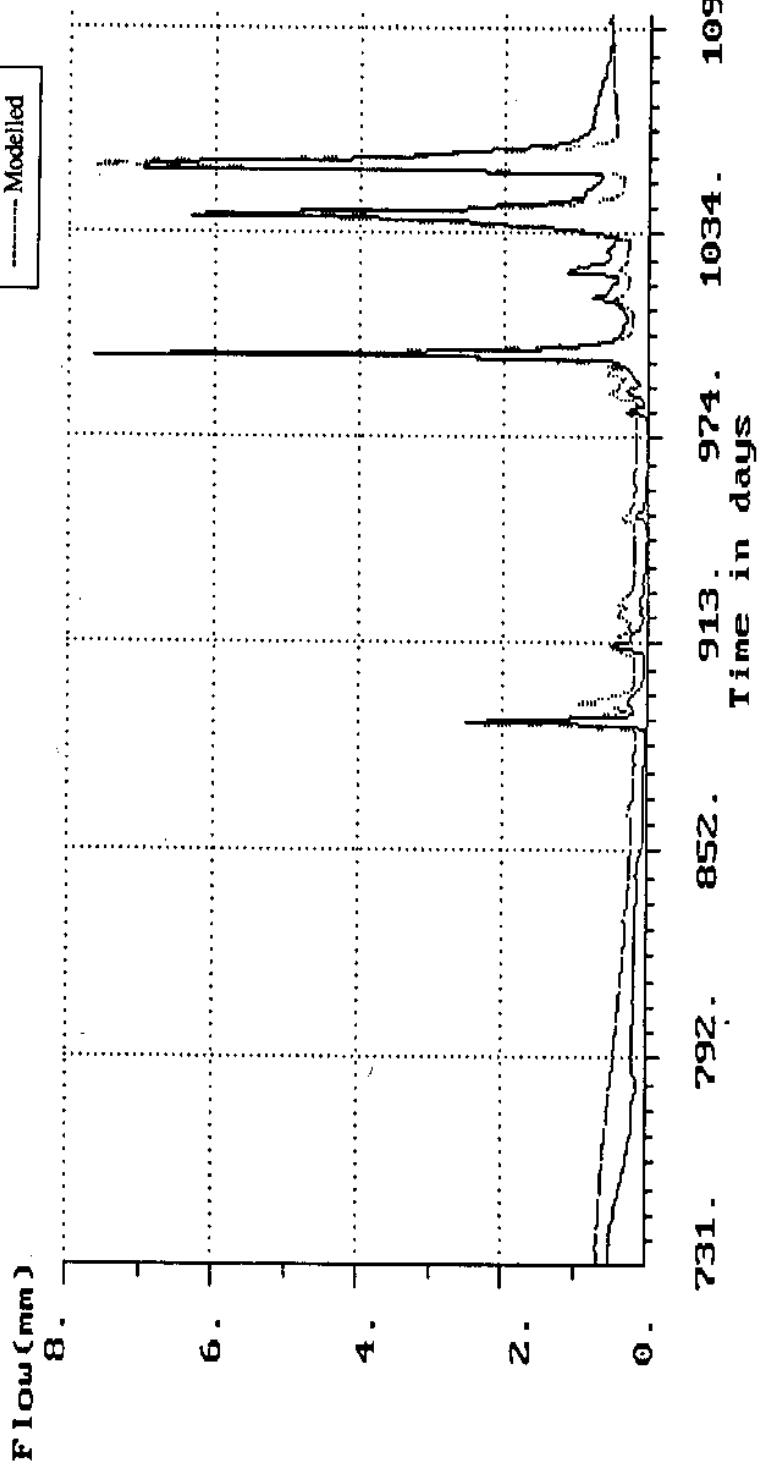


Fig.06 Modelled and observed daily flow hydrograph for 1991

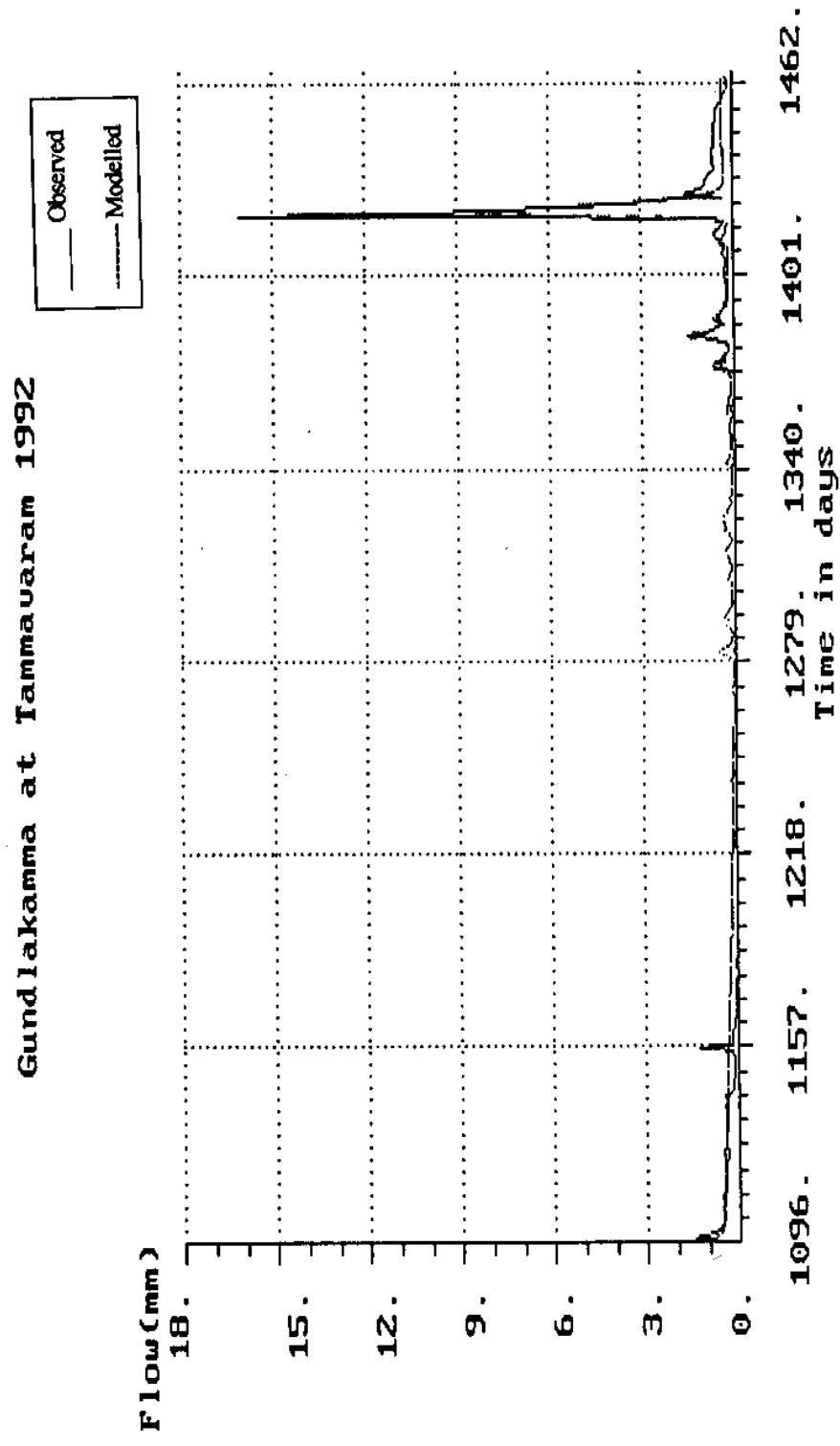


Fig.07 Modelled and observed daily flow hydrograph for 1992

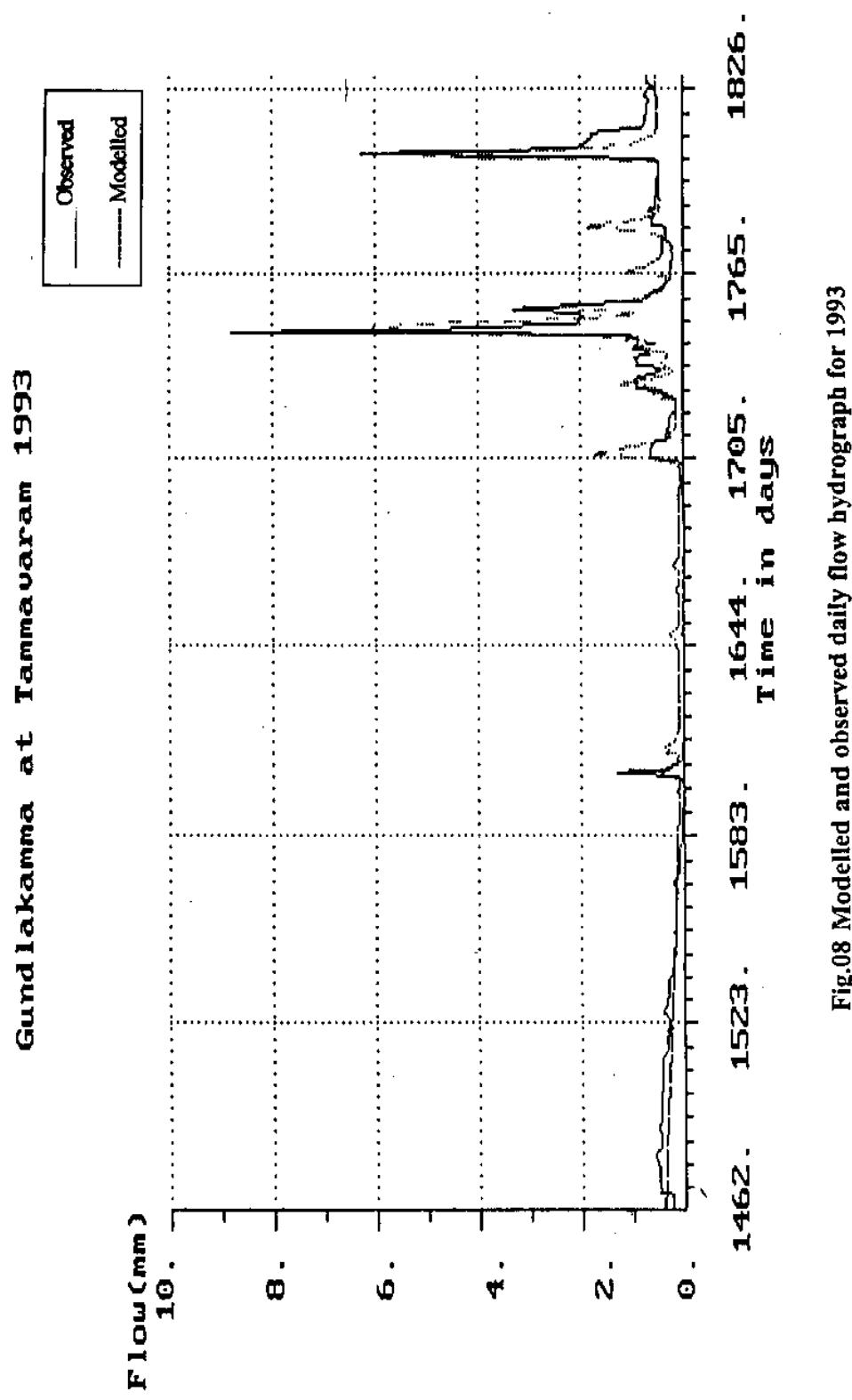


Fig.08 Modelled and observed daily flow hydrograph for 1993

Monthly observed and modelled runoff at Tammavaram on Gundlakamma river for calibration period 1989-93

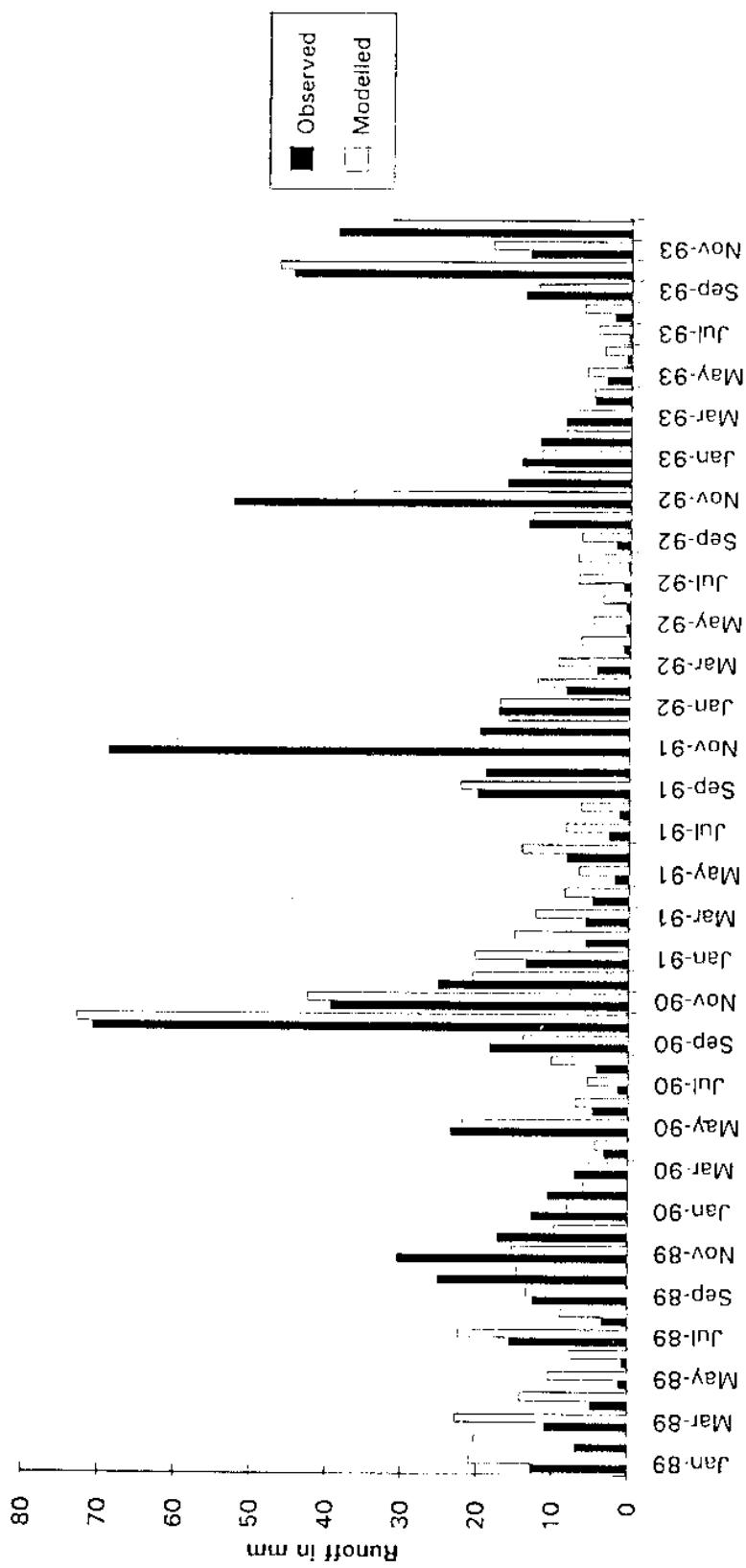


Fig.09 Modelled and observed monthly runoff for calibration

TABLE 3: Monthly Observed and Modelled Runoff for Gundlakamma at Tammavaram for Calibration

Monthly flows (mm) 1989

Month	Observed	Modelled
1	12.77	20.97
2	6.93	20.30
3	10.96	22.86
4	4.86	14.28
5	1.20	10.53
6	.78	7.67
7	15.61	22.46
8	3.43	8.87
9	12.54	13.41
10	25.17	14.68
11	30.59	15.37
12	17.24	9.67

Monthly flows (mm) 1990

Month	Observed	Modelled
1	12.77	8.05
2	10.57	5.90
3	7.03	5.27
4	3.19	4.42
5	23.49	21.95
6	4.79	7.00
7	1.44	5.41
8	4.28	10.24
9	18.41	13.96
10	70.92	72.97
11	39.58	42.58
12	25.25	20.65

Monthly flows (mm) 1991

Month	Observed	Modelled
1	13.58	20.33
2	5.69	15.15
3	5.73	12.36
4	4.86	8.59
5	1.91	6.60

6	8.27	14.17
7	2.68	8.33
8	1.30	6.41
9	20.11	22.30
10	19.00	13.23
11	69.00	59.95
12	19.88	16.03

Monthly flows (mm)                    1992

Month	Observed	Modelled
1	17.30	17.15
2	8.43	12.21
3	4.39	9.50
4	.82	6.45
5	.61	4.88
6	.49	3.58
7	.96	6.82
8	.29	6.94
9	1.93	6.44
10	13.46	12.88
11	52.68	36.74
12	16.29	11.64

Monthly flows (mm)                    1993

Month	Observed	Modelled
1	14.46	11.89
2	12.06	8.67
3	8.68	7.02
4	4.81	4.94
5	3.31	5.88
6	.58	3.53
7	.40	4.38
8	2.28	6.22
9	13.96	12.20
10	44.77	46.60
11	13.43	18.30
12	38.96	31.29

TABLE 4: Monthly Observed and Modelled Runoff for Gundlakamma at Tammavaram for Validation

Monthly flows (mm)		1994
Month	Observed	Modelled
1	16.67	20.97
2	10.35	23.78
3	5.86	19.66
4	4.34	14.33
5	2.65	11.06
6	.60	7.60
7	.14	6.91
8	1.05	6.27
9	.92	4.88
10	35.08	48.69
11	63.01	65.53
12	13.71	18.22
Monthly flows (mm)		1995
Month	Observed	Modelled
1	19.63	20.07
2	8.89	13.60
3	5.83	11.13
4	3.64	7.58
5	11.05	16.76
6	1.18	6.11
7	12.04	14.96
8	10.48	21.25
9	7.03	13.62
10	18.08	27.67
11	10.53	13.67
12	14.37	12.64
Monthly flows (mm)		1996
Month	Observed	Modelled
1	18.12	9.84
2	9.67	6.48
3	9.40	5.11
4	5.67	3.81
5	.65	2.93

6	6.80	14.72
7	.75	5.30
8	4.45	13.40
9	14.73	23.85
10	76.12	82.45
11	26.85	25.24
12	29.23	21.14

Monthly flows (mm)                  1997

Month	Observed	Modelled
1	30.72	21.22
2	13.86	14.13
3	6.42	11.57
4	6.40	9.19
5	1.80	6.65
6	.55	4.77
7	.25	4.51
8	.34	4.13
9	72.14	58.64
10	24.58	30.39
11	35.41	30.12
12	.00	.00

Gundlakurra at Tammavaram 1994-97

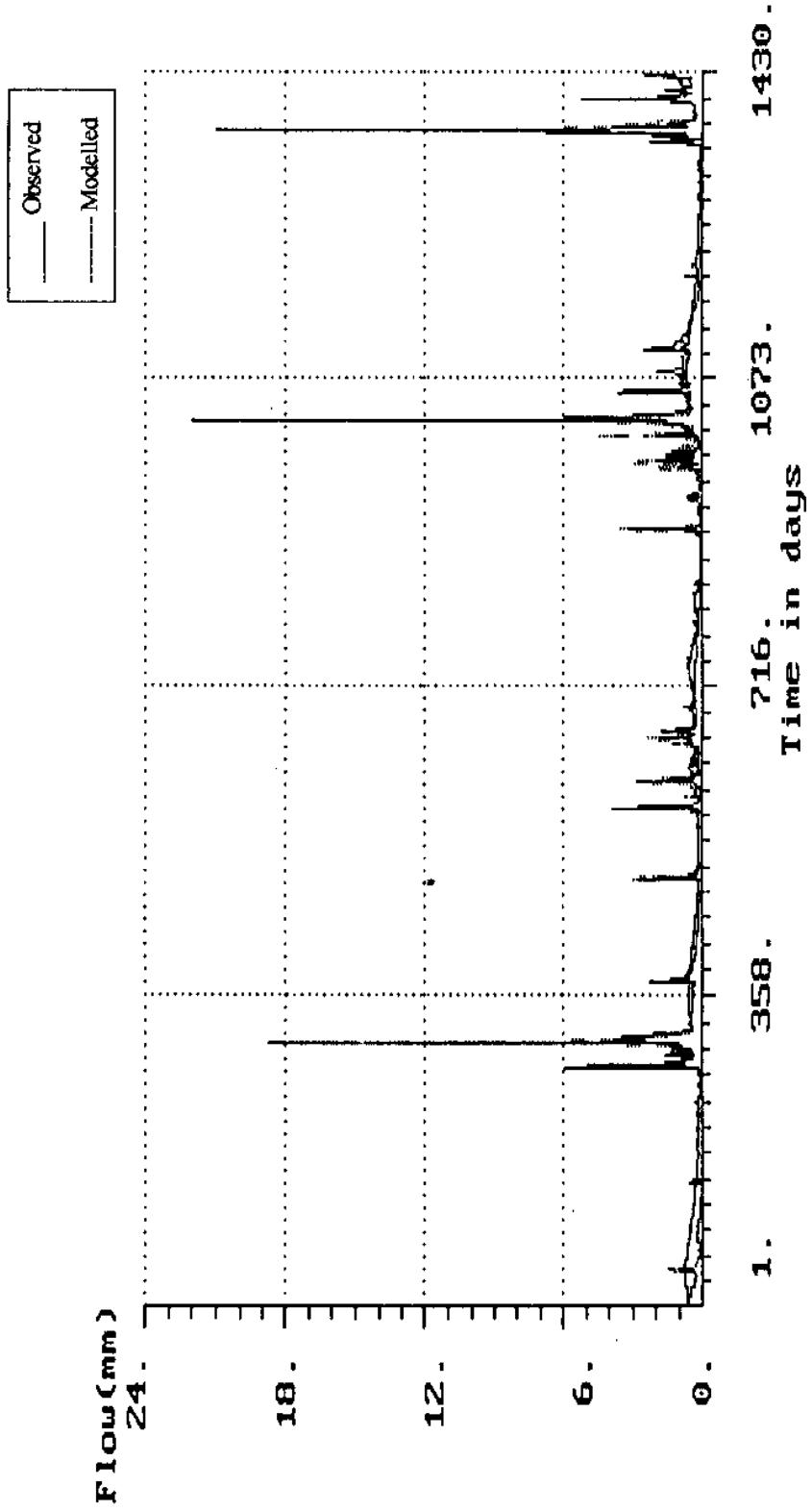


Fig.10 Modelled and observed daily flow hydrograph for validation

Gundlakamma at Tamma uaram 1994

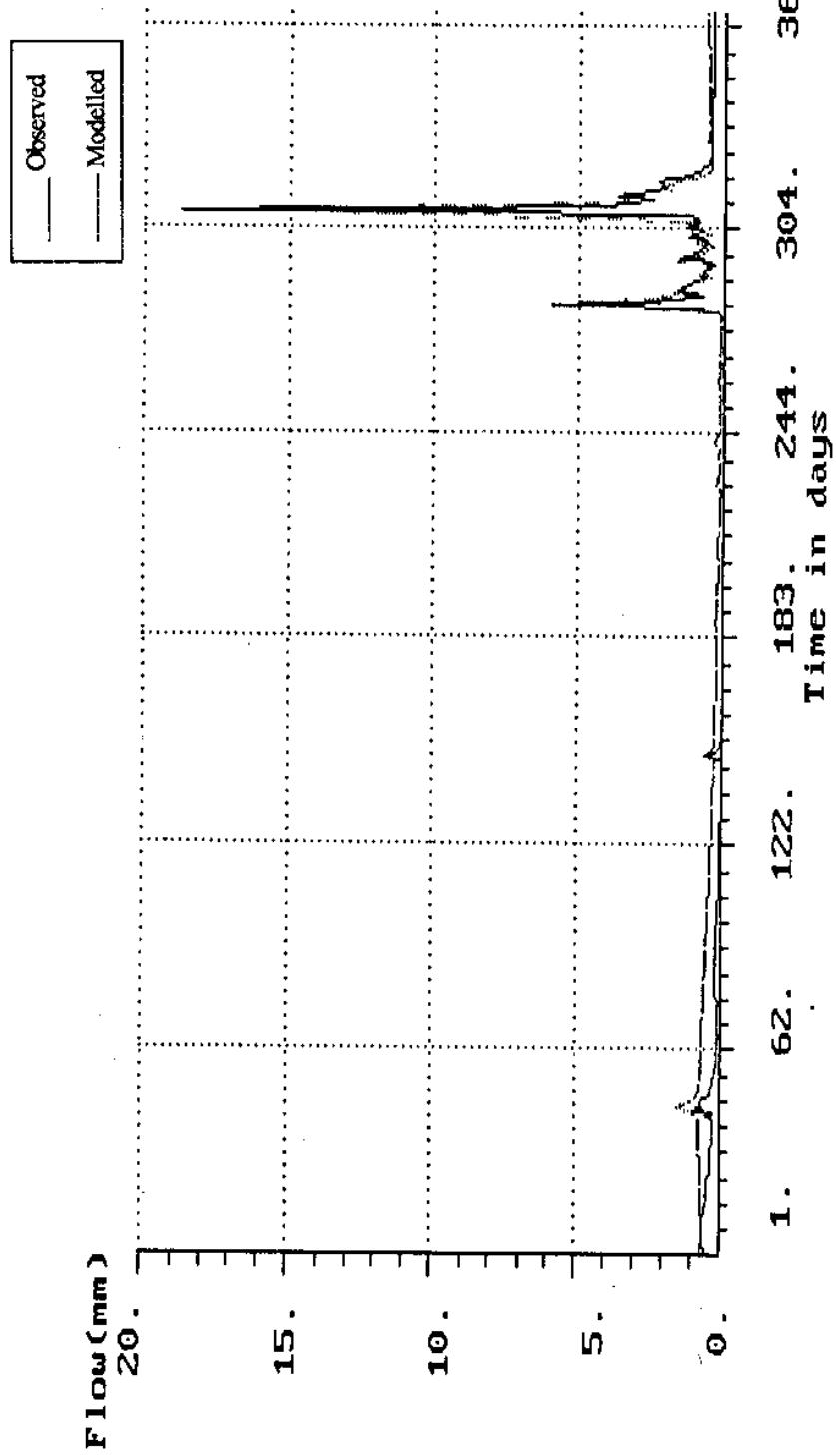


Fig.11 Modelled and observed daily flow hydrograph for 1994

Gundlakamma at Tammavaram 1995

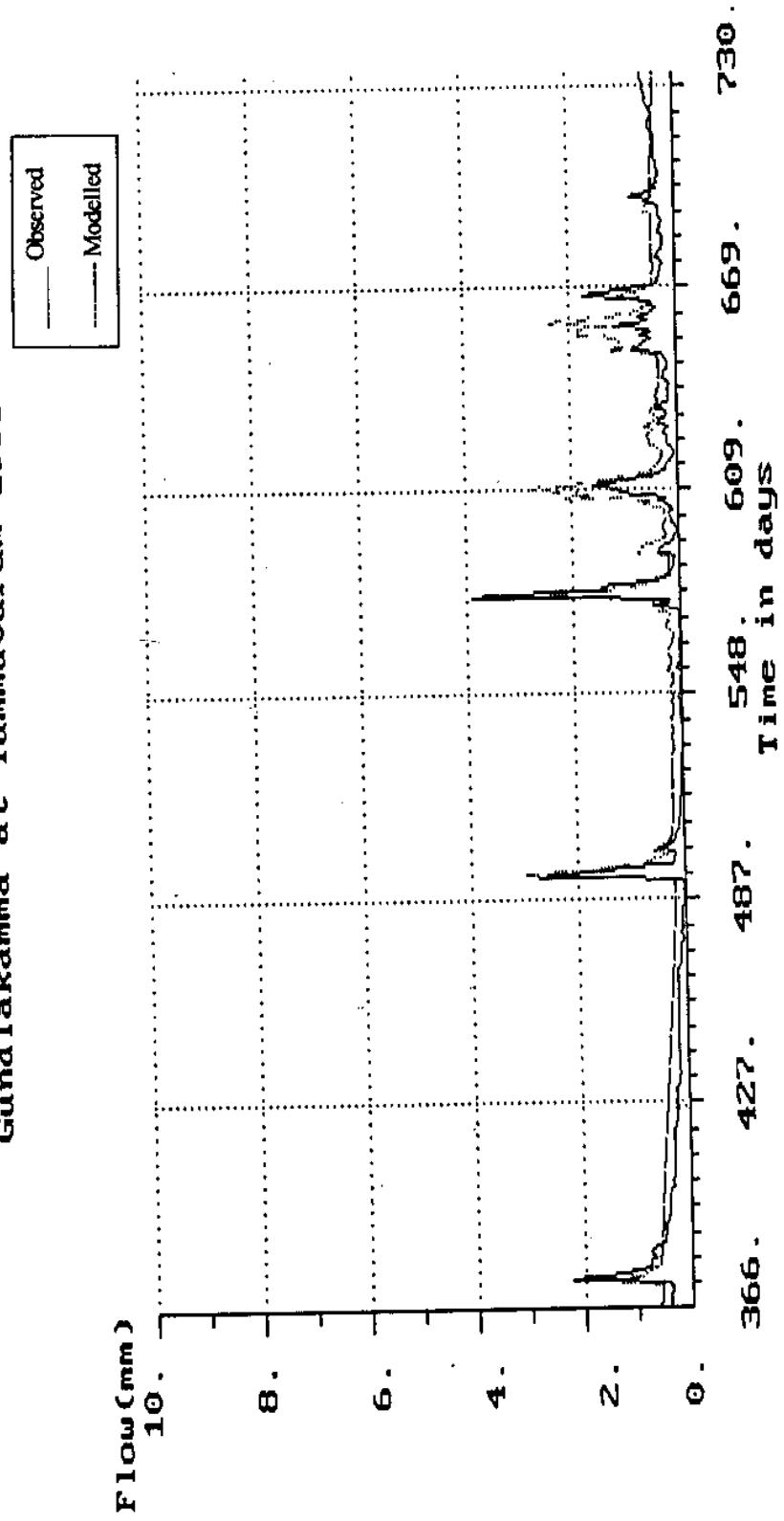


Fig.12 Modelled and observed daily flow hydrograph for 1995

Gundlakamma at Tammavaram 1996

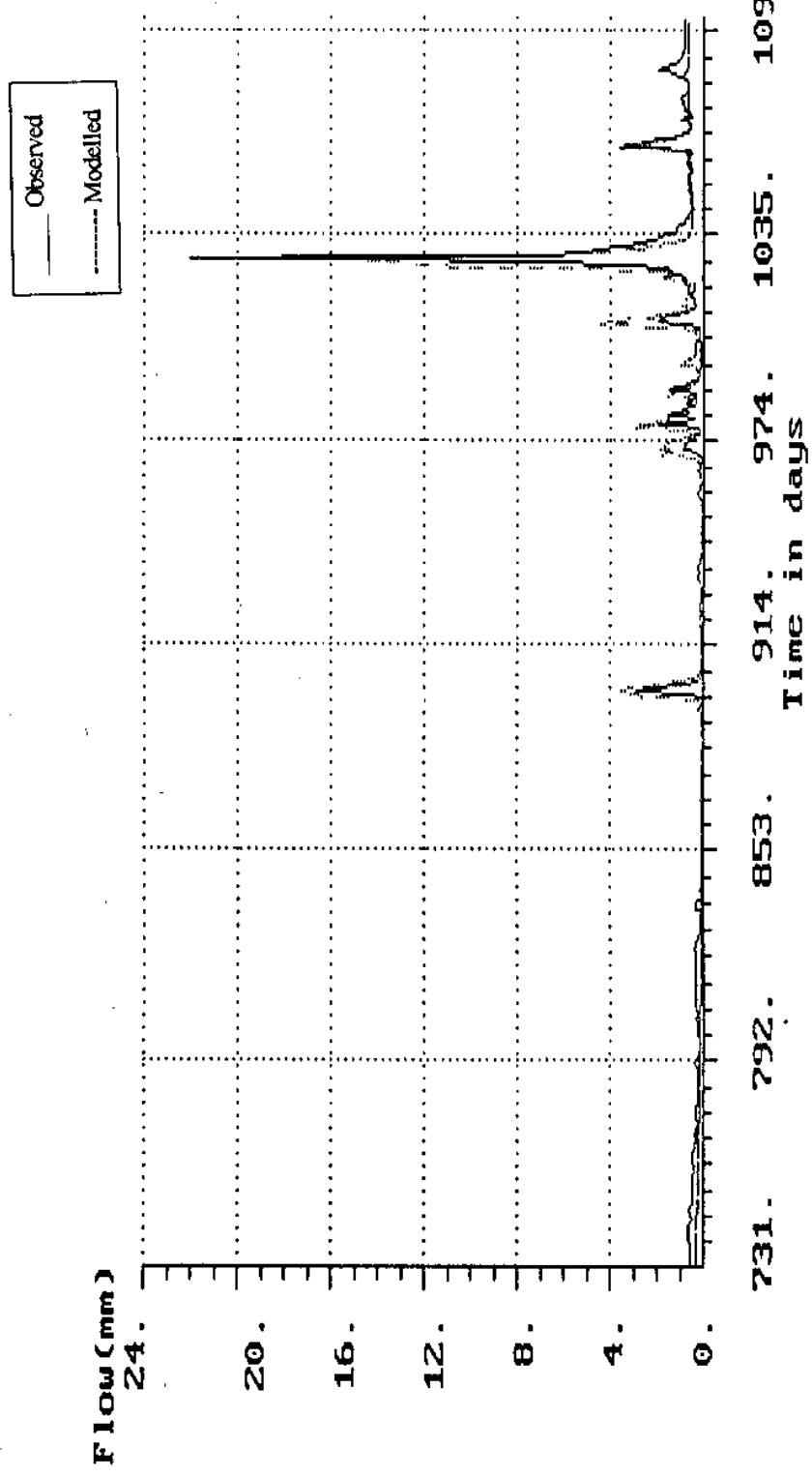


Fig.13 Modelled and observed daily flow hydrograph for 1996

Gundlakamma at Tamavaram 1997

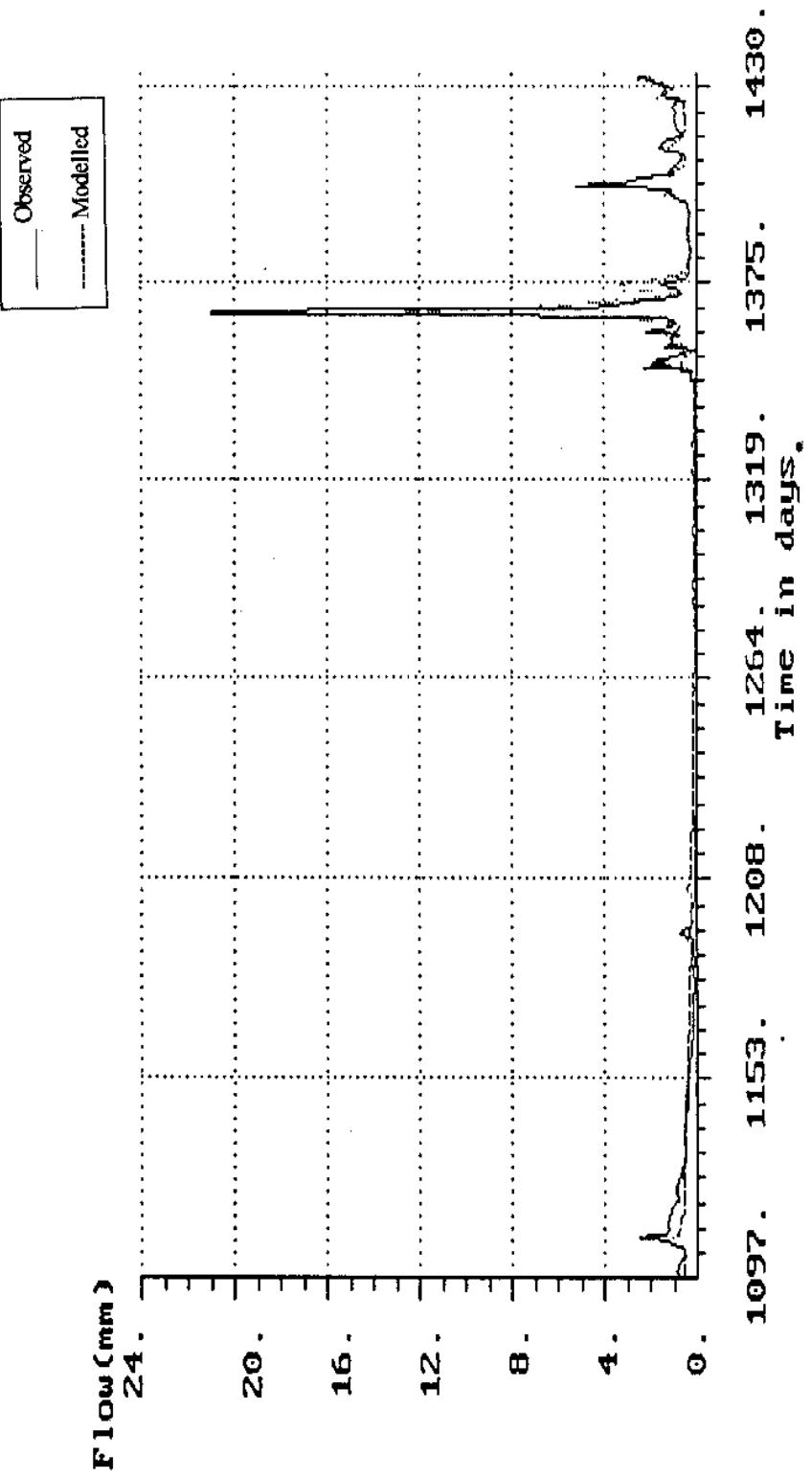


Fig.14 Modelled and observed daily flow hydrograph for 1997

as bar chart at Fig. 15. The peak monthly flows of monsoon season at Tammavaram site are modelled reasonably well by the model over both calibration and validation periods. In 1989 the data being used for warming up of the model. The observed flows of October to December are on higher side than the modelled flows. In contrast during validation period the observed monsoon flows of September 1995 to November 1995 are on lower side than the modelled flows. This may be because the year appears to be a drought year and the moisture distribution might not have been properly taken care by the model parameters appropriately. Otherwise the simulation seems to be close to the observed data.

Modelled non-monsoon flows are consistently on higher side over both calibration and validation periods. This reflects that the expected flows are not being realized due to diversions upstream of the site or in other words due to man's influence. Otherwise over all the model performance is reasonably well from the few parameters and lumping nature of the 5-parameter model used in the study.

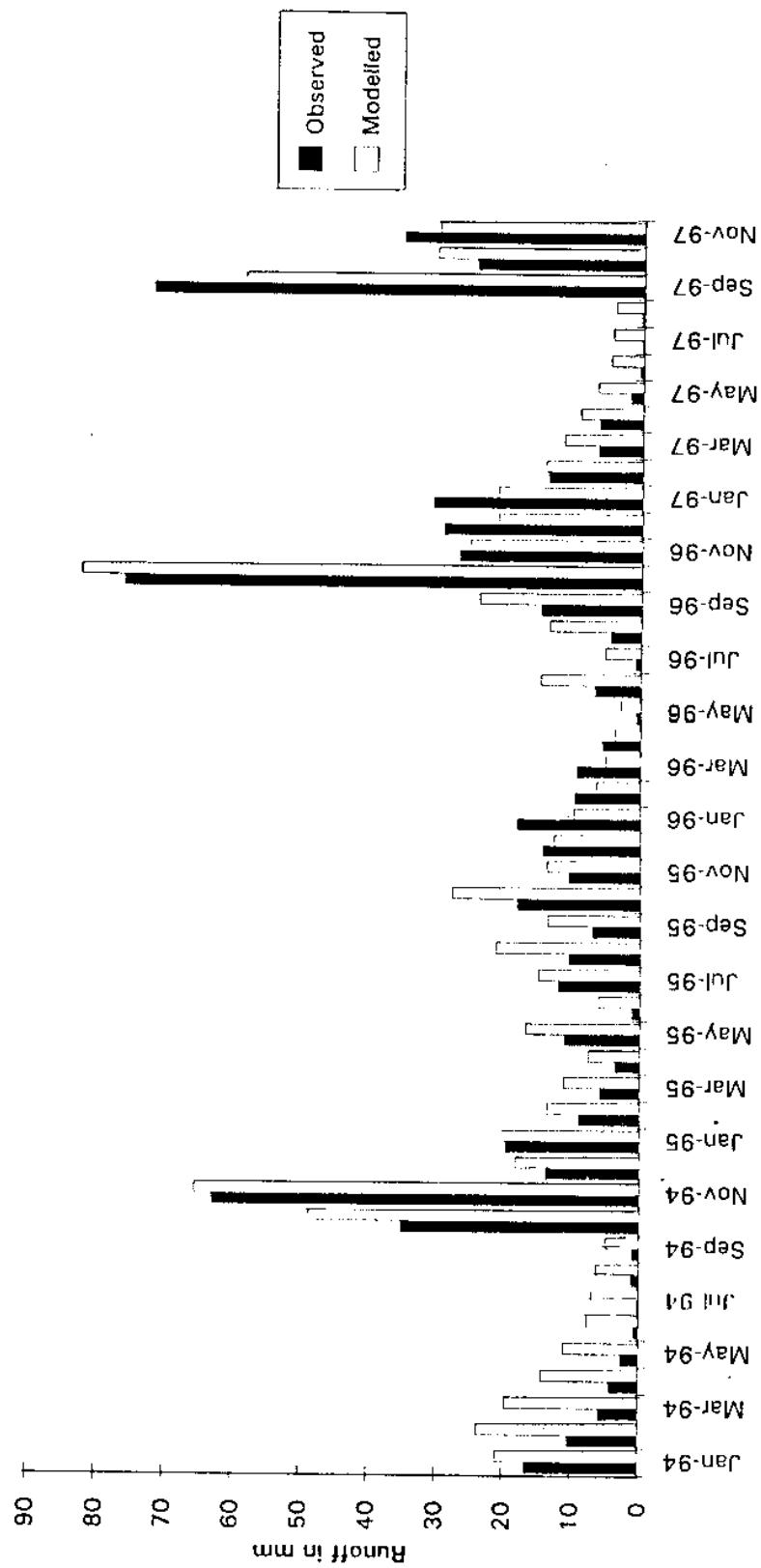
## 6.0 CONCLUSIONS AND RECOMMENDATIONS

From the calibration and validation of the modelling study, it is found that the model, though a five parameter one, could respond properly to the rainfall and resulted in an acceptably good efficiency of 72.14% in calibration and 68.25% in validation. As observed in other modelling studies on the Nagavali and the Sarada rivers (Vijayakumar, 1995), the model could simulate the flows acceptably well in the Gundlakamma basin too. The optimized parameter values are also in conformity with the parameter set obtained in the other studies on the Sarada and the Nagavali.

This study wherein a 5-parameter simple conceptual model was applied on the Gundlakamma may be extended by applying it to few more basins in the region to standardize the different parameters for different river basins in the region. Also, a slight variation of the model by reducing the number of parameter to 3 or 4 may be attempted to further simplify the model.

It is recommended that the model with the modelled parameter set can be used for various purposes like daily flow generation, hydrologic design, flood forecasting etc., over the basin, provided the obtained efficiency is acceptable. To simulate the peak flows more accurately, modelling study may be undertaken with much finer rainfall data, say hourly, and corresponding flow data of individual events.

**Monthly observed and modelled runoff at Tammavaram on Gundlakamma river for validation period 1994-97**



**Fig.15 Modelled and observed monthly runoff for validation**

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5. Acharya N.G.Ranga Agricultural University, ARS, Darsi, Prakasam District.

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### STATUS OF DATA USED IN THE MODELLING STUDY

**A. RAINFALL DATA AT**

	Weight	1989	1990	1991	1992	1993	1994	1995	1996	1997
01.Addanki	0.067	< -----	daily	-----	-----	-----	-----	-----	-----	>
02.Darsi	0.036	< -----	daily	-----	-----	-----	-----	-----	-----	>
03.Markapur	0.117	< -----	daily	-----	-----	-----	-----	-----	-----	>
04.Erragondlapalem	0.119	< -----	daily	-----	-----	-----	-----	-----	-----	>
05.Giddaluru	0.045	< -----	daily	-----	-----	-----	-----	-----	-----	>
06.Cumbum	0.149	< -----	daily	-----	-----	-----	-----	-----	-----	>
07.Tallur	0.037	< -----	daily	-----	-----	-----	-----	-----	-----	>
08.Mundlamuru	0.031	< -----	daily	-----	-----	-----	-----	-----	-----	>
09.Tripurantakam	0.122	< -----	daily	-----	-----	-----	-----	-----	-----	>
10.Bestavaripet	0.059	< -----	daily	-----	-----	-----	-----	-----	-----	>
11.Narasaraopet	0.015	< -----	daily	-----	-----	-----	-----	-----	-----	>
12.Vinukonda	0.066	< -----	daily	-----	-----	-----	-----	-----	-----	>
13.Ipur	0.052	< -----	daily	-----	-----	-----	-----	-----	-----	>
14.Bollapalli	0.085	< -----	daily	-----	-----	-----	-----	-----	-----	>

**B. FLOW DATA AT**

Tammavaram CWC Site      < ----- daily ----- >

**C. EVAPORATION DATA AT**

Darsi ARS                      Average of mean monthly data of Dec.95 to Aug.98

**Daily observed and modelled runoff for Gundlakamma at Tammavaram for Calibration with catchment average rainfall**

1828	Calibration from 1 Jan 1989 to 31 dec 1993			96	0.189	0.825	0
Day No	Observed Runoff (mm)	Modelled (mm)	Rainfall (mm)	97	0.187	0.815	0
1	0.462	0.579	0	98	0.188	0.808	0
2	0.466	0.589	0	99	0.188	0.804	0
3	0.498	0.598	0	100	0.189	0.809	0
4	0.469	0.608	0	101	0.29	0.499	0
5	0.478	0.615	0	102	0.298	0.483	0
6	0.479	0.623	0	103	0.288	0.486	0
7	0.463	0.631	0	104	0.221	0.483	0
8	0.462	0.638	0	105	0.702	0.476	0
9	0.461	0.645	0	106	0.177	0.472	0
10	0.48	0.652	0	107	0.173	0.467	0
11	0.438	0.659	0	108	0.121	0.462	0
12	0.431	0.665	0	109	0.094	0.457	0
13	0.425	0.671	0	110	0.094	0.452	0
14	0.413	0.677	0	111	0.092	0.447	0
15	0.406	0.682	0	112	0.061	0.442	0
16	0.4	0.687	0	113	0.08	0.437	0
17	0.398	0.692	0	114	0.088	0.432	0
18	0.406	0.697	0	115	0.084	0.427	0
19	0.397	0.701	0	116	0.081	0.422	0
20	0.384	0.705	0	117	0.08	0.417	0
21	0.381	0.709	0	118	0.077	0.413	0
22	0.385	0.712	0	119	0.068	0.408	0
23	0.371	0.718	0	120	0.068	0.403	0
24	0.37	0.719	0	121	0.068	0.398	0
25	0.372	0.723	0	122	0.067	0.394	0
26	0.388	0.724	0	123	0.058	0.39	0.357
27	0.38	0.727	0	124	0.048	0.385	0
28	0.342	0.729	0	125	0.048	0.381	0
29	0.341	0.731	0	126	0.046	0.376	0
30	0.339	0.733	0	127	0.046	0.372	0.3676
31	0.338	0.734	0	128	0.046	0.368	0
32	0.339	0.739	0	129	0.046	0.364	0
33	0.332	0.737	0	130	0.046	0.358	0
34	0.318	0.738	0	131	0.045	0.355	0
35	0.302	0.738	0	132	0.043	0.351	0
36	0.287	0.739	0	133	0.041	0.347	0
37	0.271	0.738	0	134	0.041	0.343	0
38	0.268	0.739	0	135	0.039	0.339	0
39	0.262	0.719	0	136	0.036	0.335	0
40	0.239	0.738	0	137	0.031	0.331	0
41	0.236	0.737	0	138	0.032	0.328	0
42	0.234	0.736	0	139	0.03	0.324	0
43	0.234	0.735	0	140	0.03	0.32	0
44	0.233	0.734	0	141	0.03	0.318	0.207
45	0.233	0.732	0	142	0.028	0.326	0.838
46	0.238	0.73	0	143	0.03	0.328	0
47	0.236	0.728	0	144	0.028	0.317	0
48	0.232	0.726	0	145	0.03	0.308	0
49	0.228	0.724	0	146	0.027	0.303	0
50	0.226	0.721	0	147	0.027	0.298	0
51	0.223	0.718	0	148	0.027	0.294	0
52	0.216	0.718	0	149	0.028	0.291	0
53	0.213	0.713	0	150	0.028	0.288	0.3914
54	0.211	0.71	0	151	0.028	0.288	3.0812
55	0.228	0.706	0	152	0.027	0.285	0
56	0.227	0.703	0	153	0.024	0.281	0.298
57	0.224	0.699	0	154	0.023	0.277	0.027
58	0.222	0.695	0	155	0.024	0.273	0.8
59	0.238	0.691	0	156	0.024	0.282	7.413
60	0.231	0.687	0	157	0.024	0.284	0
61	0.239	0.683	0	158	0.028	0.295	5.8207
62	0.228	0.679	0	159	0.048	0.284	0
63	0.228	0.674	0	160	0.042	0.272	0.1629
64	0.224	0.67	0	161	0.041	0.284	1.8174
65	0.222	0.665	0	162	0.038	0.282	2.4262
66	0.227	0.66	0	163	0.035	0.287	0.4229
67	0.22	0.655	0	164	0.023	0.253	1.5713
68	0.22	0.65	0	165	0.023	0.306	10.3553
69	0.218	0.644	0	166	0.051	0.292	2.0074
70	0.596	1.905	49.6257	167	0.04	0.272	0.124
71	0.651	1.651	0	168	0.028	0.257	0
72	0.706	1.246	0	169	0.023	0.247	0.1428
73	0.654	0.955	0	170	0.019	0.241	0
74	0.53	0.781	0	171	0.018	0.237	0
75	0.483	0.702	0	172	0.017	0.234	0
76	0.458	0.656	0	173	0.016	0.232	0
77	0.452	0.632	0	174	0.016	0.228	0
78	0.413	0.616	0	175	0.013	0.227	1.0424
79	0.374	0.61	0	176	0.012	0.225	0
80	0.358	0.606	0	177	0.012	0.222	0
81	0.351	0.599	0	178	0.012	0.22	0.218
82	0.382	0.594	0	179	0.013	0.219	1.2882
83	0.344	0.589	0.416	181	0.013	0.218	0.0728
84	0.337	0.58	3.3748	182	0.012	0.214	0.773
85	0.328	0.592	0	183	0.013	0.214	2.072
86	0.322	0.593	0	184	0.013	0.214	1.816
87	0.302	0.575	0	185	0.012	0.211	0.4768
88	0.284	0.568	0	186	0.012	0.207	0
89	0.252	0.562	0	187	0.013	0.216	4.5013
90	0.25	0.566	0	188	0.012	0.24	6.4406
91	0.256	0.551	0	189	0.012	0.241	3.2985
92	0.255	0.546	0	190	0.03	0.238	1.5091
93	0.254	0.541	0	191	0.156	0.281	7.8855
94	0.194	0.538	0	192	0.073	0.256	0.7865
95	0.19	0.53	0	193	0.09	0.255	4.6015
96						0.295	7.3385

194	0.195	0.264	2.1728	292	0.415	0.308	0
195	0.128	0.233	0	293	0.395	0.307	0
196	0.061	0.375	13.4398	294	0.374	0.308	0
197	1.611	2.24	82.2654	295	0.343	0.309	0
198	3.881	2.623	70.6802	298	0.339	0.31	0
199	1.578	1.92	6.9537	297	0.334	0.311	0
200	0.765	1.193	0.24	298	0.328	0.312	0
201	0.351	0.724	2.2808	299	0.322	0.312	0
202	0.312	0.67	8.9727	300	0.465	0.313	0
203	0.291	0.867	12.081	301	0.444	0.313	0
204	1.049	2.425	31.9188	302	0.654	0.443	8.3928
205	1.808	2.055	7.7593	303	0.586	0.417	0
206	0.773	1.344	1.2194	304	0.861	0.378	0
207	0.467	0.833	0	305	0.859	0.347	0
208	0.326	0.538	0	306	0.509	0.33	0
209	0.242	0.388	1.0525	307	0.454	0.321	0
210	0.195	0.312	0.4521	308	0.459	0.316	0
211	0.182	0.291	5.4472	309	0.459	0.314	0
212	0.167	0.275	0	310	0.445	0.312	0
213	0.139	0.268	0	311	0.443	0.311	0
214	0.108	0.263	0	312	0.434	0.31	0
215	0.102	0.263	0	313	0.764	1.312	35.971
216	0.093	0.264	0	314	2.863	1.313	7.3167
217	0.092	0.265	0	315	1.758	0.855	0
218	0.092	0.267	0	316	1.6	0.888	0.009
219	0.09	0.269	0.225	317	1.324	0.758	8.9467
220	0.092	0.27	0.3285	318	1.335	0.686	3.6158
221	0.088	0.272	0	319	3.686	1.074	14.5287
222	0.098	0.273	0.1072	320	2.326	0.87	0
223	0.085	0.274	1.104	321	1.412	0.84	0
224	0.091	0.275	1.2209	322	1.214	0.489	0
225	0.091	0.276	1.404	323	1.147	0.405	0
226	0.089	0.276	1.8134	324	0.84	0.362	0
227	0.089	0.277	0.551	325	0.698	0.342	0
228	0.084	0.277	0.5215	326	0.693	0.333	0
229	0.087	0.28	6.8008	327	0.674	0.329	0
230	0.103	0.38	1.3328	328	0.887	0.328	0
231	0.115	0.327	2.1428	329	0.564	0.327	0
232	0.115	0.304	1.119	330	0.655	0.327	0
233	0.126	0.291	0	331	0.635	0.327	0
234	0.117	0.312	4.0303	332	0.623	0.328	0
235	0.134	0.313	3.3221	333	0.625	0.328	0
236	0.202	0.3	2.3438	334	0.827	0.328	0
237	0.202	0.29	0.296	335	0.588	0.327	0
238	0.169	0.263	0.7122	336	0.559	0.327	1.154
239	0.148	0.28	0	337	0.558	0.327	0
240	0.116	0.278	0	338	0.554	0.328	0
241	0.098	0.276	0	339	0.558	0.326	0
242	0.087	0.275	1.2346	340	0.543	0.325	0
243	0.086	0.274	2.0578	341	0.521	0.324	0
244	0.113	0.273	0.7602	342	0.506	0.324	0
245	0.134	0.272	1.1764	343	0.498	0.323	0
246	0.154	0.311	4.8132	344	0.498	0.322	0
247	0.441	0.302	0	345	0.514	0.321	0
248	0.378	0.319	4.0578	346	0.488	0.32	0
249	0.272	0.303	0	347	0.489	0.318	0
250	0.176	0.287	0	348	0.485	0.317	0
251	0.132	0.278	0	349	0.485	0.316	0
252	0.112	0.263	0.7868	350	0.485	0.314	0
253	0.149	0.314	8.7418	351	0.486	0.313	0
254	0.195	0.317	1.2501	352	0.486	0.311	0
255	0.331	0.294	0.9465	353	0.475	0.31	0
256	0.355	0.277	0.8442	354	0.491	0.308	0
257	0.209	0.287	0.2016	355	0.482	0.308	0
258	0.167	0.261	0	356	0.528	0.304	0
259	0.169	0.31	5.8437	357	0.572	0.303	0
260	0.225	0.297	0.089	358	0.642	0.301	0
261	0.28	0.518	18.5145	359	1.001	0.299	0
262	0.09	0.804	17.1672	360	1.092	0.297	0
263	1.183	0.817	8.6358	361	0.642	0.295	0
264	0.933	0.686	4.7172	362	0.774	0.293	0
265	0.802	0.496	0.2144	363	0.421	0.291	0.027
266	0.844	0.392	0.7432	364	0.415	0.295	1.547
267	0.563	0.318	0.067	365	0.41	0.292	0.036
268	0.472	0.285	0	366	0.722	0.351	8.8889
269	0.41	0.921	24.2655	367	1.545	0.335	0
270	0.651	0.806	3.8334	368	1.123	0.312	0
271	0.673	0.871	5.4552	369	0.691	0.298	0
272	0.673	0.719	8.9419	370	0.516	0.286	0
273	0.881	1.036	14.4405	371	0.439	0.279	0
274	1.346	0.812	2.4903	372	0.41	0.275	0
275	1.346	0.581	0	373	0.398	0.272	0
276	1.035	0.791	10.1962	374	0.363	0.27	0
277	1.117	0.639	0	375	0.375	0.267	0
278	1.608	1.481	21.5786	376	0.366	0.265	0
279	2.518	1.278	4.25	377	0.372	0.263	0
280	1.621	0.889	1.3824	378	0.332	0.281	0
281	1.8	0.81	1.546	379	0.311	0.259	0
282	1.325	0.448	0	380	0.288	0.257	0
283	1.105	0.366	0	381	0.271	0.255	0
284	0.818	0.326	0	382	0.279	0.252	0
285	0.584	0.309	0	383	0.28	0.25	0
286	0.541	0.302	1.6182	384	0.28	0.248	0
287	0.531	0.3	0	385	0.281	0.246	0
288	0.456	0.3	0	386	0.415	0.243	0
289	0.479	0.301	0	387	0.37	0.241	0
290	0.447	0.303	0	388	0.299	0.239	0
291	0.421	0.304	0	389	0.28	0.237	0

390	0.266	0.234	0	488	0.053	0.116	0
391	0.262	0.237	0	489	0.052	0.115	0
392	0.251	0.23	0	490	0.05	0.113	0
393	0.251	0.227	0	491	0.05	0.112	0
394	0.251	0.225	0	492	0.05	0.111	0
395	0.252	0.223	0	493	0.074	0.112	2.6139
396	0.221	0.221	0	494	0.076	0.125	5.7729
397	0.253	0.218	0	495	0.066	1.211	80.8987
398	0.253	0.216	0	496	5.848	2.678	44.8367
399	0.251	0.214	0	497	3.255	5.085	51.8984
400	0.251	0.212	0	498	2.207	4.09	12.212
401	0.252	0.209	0	499	2.041	2.519	2.1862
402	0.253	0.207	0	500	1.214	1.414	0
403	0.251	0.205	0	501	1.17	0.782	1.074
404	0.258	0.203	0	502	0.772	0.454	0.177
405	0.251	0.201	0	503	0.717	0.294	0
406	0.251	0.198	0	504	0.517	0.221	0
407	0.242	0.195	0	505	0.485	0.189	1.1286
408	0.242	0.194	0	506	0.417	0.178	5.8052
409	0.241	0.192	0	507	0.407	0.173	0.7495
410	0.239	0.19	0	508	0.422	0.173	3.3071
411	0.254	0.188	0	509	0.407	0.175	0
412	0.252	0.186	0	510	0.491	0.178	0.294
413	0.171	0.186	2.1568	511	0.52	0.18	4.8714
414	0.572	0.183	0.3474	512	0.463	0.183	0
415	0.543	0.181	0	513	0.41	0.185	0.9417
416	0.441	0.193	5.6198	514	0.395	0.187	0
417	0.47	0.188	0	515	0.383	0.189	0
418	0.392	0.182	0	516	0.375	0.19	0.5802
419	0.362	0.207	6.8595	517	0.371	0.191	0
420	0.311	0.301	12.3978	518	0.329	0.191	0
421	0.722	0.335	8.6582	519	0.32	0.192	0
422	1.174	0.282	0.6764	520	0.321	0.192	0
423	0.719	0.233	0	521	0.224	0.31	11.4592
424	0.484	0.202	0	522	0.191	0.285	0.0976
425	0.431	0.185	0.3328	523	0.187	0.248	0
426	0.179	0.176	0	524	0.149	0.221	0
427	0.174	0.172	0	525	0.146	0.202	11.300
428	0.174	0.189	0	526	0.153	0.258	0
429	0.257	0.187	0	527	0.153	0.21	0
430	0.247	0.186	0	528	0.149	0.28	7.4943
431	0.234	0.185	1.948	529	0.179	0.326	9.7329
432	0.242	0.195	1.238	530	0.355	0.457	13.5818
433	0.259	0.193	2.4634	531	0.215	0.382	0.03
434	0.521	0.221	5.5658	532	0.189	0.3	1.3833
435	0.183	0.208	2.2546	533	0.145	0.247	0
436	0.193	0.189	0.9742	534	0.113	0.217	0.9577
437	0.249	0.187	2.8414	535	0.107	0.201	0.648
438	0.249	0.177	0.1452	536	0.1	0.193	0
439	0.25	0.169	0	537	0.096	0.188	0.3018
440	0.241	0.164	0	538	0.095	0.188	0
441	0.237	0.161	0	539	0.082	0.184	0
442	0.12	0.159	0	540	0.075	0.183	0
443	0.183	0.158	0	541	0.069	0.181	0.2475
444	0.142	0.157	0	542	0.061	0.18	0
445	0.136	0.156	0	543	0.057	0.178	0
446	0.135	0.155	0	544	0.051	0.176	0.59
447	0.128	0.154	0	545	0.051	0.175	0
448	0.125	0.153	0	546	0.05	0.18	3.3136
449	0.125	0.151	0	547	0.051	0.177	0
450	0.118	0.15	0	548	0.049	0.176	1.4885
451	0.104	0.149	0	549	0.05	0.178	2.5776
452	0.091	0.148	0	550	0.05	0.174	0.0714
453	0.089	0.146	0	551	0.051	0.17	0.177
454	0.088	0.183	5.4855	552	0.049	0.182	4.6944
455	0.087	0.186	5.7018	553	0.052	0.2	6.1514
456	0.089	0.174	0	554	0.052	0.238	7.5811
457	0.088	0.16	0	555	0.065	0.238	4.2722
458	0.088	0.151	-1.595	556	0.064	0.21	0
459	0.086	0.145	0.9368	557	0.081	0.187	1.6386
460	0.108	0.141	0.298	558	0.098	0.173	1.0906
461	0.21	0.265	15.8385	559	0.106	0.174	3.012
462	0.154	0.239	0	560	0.097	0.171	2.3989
463	0.21	0.199	0	561	0.063	0.169	2.5044
464	0.17	0.179	2.718	562	0.07	0.197	5.332
465	0.15	0.181	0	563	0.054	0.187	0.236
466	0.118	0.149	0	564	0.052	0.174	0
467	0.122	0.142	0	565	0.048	0.165	0.144
468	0.118	0.139	0	566	0.048	0.159	1.2689
469	0.083	0.137	0	567	0.044	0.181	2.4269
470	0.109	0.135	0	568	0.028	0.175	3.8841
471	0.094	0.134	0	569	0.015	0.169	0.106
472	0.095	0.133	0	570	0.013	0.181	0.4086
473	0.076	0.132	0	571	0.012	0.158	0.218
474	0.077	0.131	0	572	0.012	0.153	0
475	0.074	0.131	0	573	0.014	0.15	0
476	0.087	0.13	0	574	0.012	0.149	0
477	0.067	0.128	0	575	0.012	0.147	0
478	0.063	0.127	0	576	0.008	0.146	0
479	0.063	0.128	0	577	0.008	0.145	0.218
480	0.059	0.125	0	578	0.005	0.144	0
481	0.057	0.124	0	579	0.005	0.142	0
482	0.057	0.123	0	580	0.004	0.144	1.4922
483	0.056	0.122	0	581	0.004	0.142	0.0924
484	0.056	0.12	0	582	0.005	0.146	2.2348
485	0.054	0.119	0	583	0.004	0.157	4.0424
486	0.053	0.118	0	584	0.005	0.212	9.3545
487	0.053	0.117	0.6932	585	0.005	0.193	0.6756

586	0.095	0.205	5.2344	684	1.141	2.673	19.0046
587	0.227	0.353	14.2942	685	1.999	3.142	10.29
588	0.311	0.442	10.1037	685	2.393	2.291	1.3475
589	0.245	0.348	0.105	687	1.535	1.531	0
590	0.227	0.257	1.181	688	1.271	1.06	0
591	0.241	0.092	23.3159	689	1.106	0.805	0
592	0.215	1.620	12.4142	690	1.012	0.987	5.7366
593	0.28	1.248	3.6684	691	0.996	0.807	2.8473
594	0.405	0.794	2.1618	692	2.393	2.515	17.168
595	0.388	0.491	0	693	2.416	4.961	23.8528
596	0.255	0.322	0	694	3.873	3.756	3.2024
597	0.141	0.236	2.0863	695	2.549	3.444	9.89
598	0.134	0.195	1.921	696	2.037	2.371	0
599	0.13	0.176	0.7401	697	1.699	1.567	0.078
600	0.119	0.169	0	698	1.365	1.095	0
601	0.095	0.157	0	699	1.271	0.847	0
602	0.091	0.167	0	700	1.112	0.728	0
603	0.088	0.168	0.18	701	1.103	0.87	0
604	0.079	0.17	0.054	702	1.128	0.648	0
605	0.095	0.129	3.667	703	1.101	0.638	0
606	0.095	0.187	0.021	704	0.996	0.618	0
607	0.097	0.182	0	705	0.989	0.638	0.3492
608	0.093	0.179	1.1142	706	0.934	0.641	2.5038
609	0.091	0.178	0	707	0.928	0.644	1.1088
610	0.088	0.178	0	708	0.927	0.647	0
611	0.083	0.178	0	709	0.92	0.651	0
612	0.083	0.178	0	710	0.886	0.654	0
613	0.091	0.249	6.1674	711	0.851	0.657	0
614	0.142	0.215	1.3471	712	0.824	0.66	0
615	0.14	0.213	2.0446	713	0.847	0.862	0
616	0.173	0.61	23.2878	714	0.849	0.665	0
617	0.201	0.92	15.9345	715	0.839	0.667	0
618	0.525	0.707	0.458	716	0.821	0.659	0
619	0.419	0.489	3.2599	717	0.814	0.671	0
620	0.71	0.346	0.3606	718	0.754	0.673	0
621	0.38	0.267	6.4968	719	0.764	0.674	0
622	1.003	0.462	10.5452	720	0.769	0.678	0
623	0.549	0.397	1.5524	721	0.72	0.77	0
624	0.459	0.314	0.705	722	0.691	0.678	0
625	0.389	0.473	8.134	723	0.675	0.678	0
626	0.888	0.71	12.9015	724	0.642	0.679	0
627	1.581	0.889	11.1395	725	0.573	0.68	0
628	1.512	0.673	2.8548	726	0.573	0.68	0
629	1.101	0.471	3.4746	727	0.563	0.68	0
630	0.385	0.345	3.5176	728	0.563	0.68	0
631	0.373	0.276	0	729	0.544	0.68	0
632	0.36	0.75	15.3548	730	0.544	0.69	0.2205
633	1.111	0.644	3.6147	731	0.546	0.678	0.1945
634	1.108	0.473	3.0185	732	0.521	0.679	0
635	1.013	0.406	4.6752	733	0.52	0.678	0
636	0.965	0.468	6.5152	734	0.52	0.677	0
637	0.865	0.484	5.5235	735	0.52	0.676	0
638	1.545	1.019	15.5182	736	0.521	0.718	3.4179
639	1.491	4.621	3.5283	737	0.521	0.708	0.2049
640	6.12	4.893	14.83	738	0.506	0.693	0
641	8.115	3.37	9.1518	739	0.508	0.682	0
642	3.652	3.124	10.1317	740	0.506	0.675	0
643	2.428	1.982	0	741	0.514	0.67	0
644	1.535	1.186	0	742	0.503	0.667	0
645	1.106	0.732	0	743	0.482	0.664	0
646	1.05	0.458	0.6976	744	0.459	0.662	0
647	1.008	0.572	5.7046	745	0.449	0.659	0
648	1.217	0.485	0	746	0.445	0.651	0
649	1.451	1.295	12.4926	747	0.444	0.654	0
650	2.647	1.074	0.3918	748	0.433	0.652	0
651	1.387	1.326	8.8768	749	0.428	0.649	0
652	1.106	1.325	6.2687	750	0.425	0.646	0
653	1.525	0.968	1.5928	751	0.414	0.643	0
654	2.510	2.364	19.1649	752	0.384	0.64	0
655	1.418	1.883	0	753	0.379	0.637	0
656	1.104	1.234	1.2174	754	0.361	0.633	0
657	1.08	0.83	0	755	0.348	0.63	0
658	0.592	0.593	0	756	0.333	0.626	0
659	0.14	0.473	0	757	0.333	0.623	0
660	0.65	0.416	0	758	0.335	0.619	0
661	0.61	1.132	10.7318	759	0.317	0.615	0
662	2.116	3.061	22.8555	760	0.306	0.612	0
663	7.862	8.966	51.5544	761	0.293	0.608	0
664	8.092	8.877	3.4515	762	0.276	0.604	0
665	2.975	4.684	6.4254	763	0.268	0.6	0
666	2.882	4.631	15.182	764	0.258	0.598	0
667	2.189	1.721	3.7419	765	0.26	0.591	0
668	2.13	2.479	1.3775	766	0.252	0.582	0
669	1.406	1.513	0	767	0.247	0.583	0
670	1.094	0.952	0	768	0.238	0.578	0
671	1.013	0.717	0.8754	769	0.231	0.573	0
672	0.933	0.577	0	770	0.21	0.569	0
673	0.933	0.516	0	771	0.2	0.564	0
674	0.844	0.472	0	772	0.188	0.559	0
675	0.697	0.7	4.8562	773	0.185	0.554	0
676	0.675	0.658	1.4754	774	0.189	0.55	0
677	0.647	0.593	0	775	0.189	0.545	0
678	0.65	0.549	2.0785	776	0.204	0.54	0
679	0.615	0.522	0	777	0.198	0.535	0
680	0.616	0.518	0	778	0.193	0.53	0
681	0.59	0.516	0.168	779	0.19	0.525	0
682	0.593	0.518	0.275	780	0.168	0.52	0
683	0.612	0.702	5.2297	781	0.165	0.515	0

782	0 157	0 51	0	880	0 033	0 182	0
783	0 16	0 504	0	881	0 032	0 178	0
784	0 159	0 499	0	882	0 032	0 175	0
785	0 159	0 494	0	883	0 03	0 171	D 238
786	0 153	0 489	0	884	0 028	0 171	0
787	0 192	0 484	0	885	0 027	0 17	1 1588
788	0 193	0 479	0	886	0 038	0 19	7 5757
789	0 194	0 474	0	887	0 048	2,249	84 3792
790	0 19	0 469	0	888	7 52	1 837	1 8014
791	0 195	0 464	0	889	1 347	1.177	1 622
792	0 196	0 459	0	890	0 29	0 712	1 5176
793	0 195	0 454	0	891	0 195	0 446	0 3724
794	0 197	0 449	0	892	0 191	0 308	4 6866
795	0 197	0 444	0	893	0 273	0 956	24 8033
796	0 195	0 439	0	894	0 281	0 375	0 3098
797	0 181	0 416	0	895	0 245	0 544	0
798	0 19	0 41	0	896	0 202	0 378	0
799	0 19	0 425	0	897	0 189	0 284	0
800	0 19	0 42	0	898	0 124	0 236	0
801	0 189	0 415	0	899	0 1	0 213	0
802	0 186	0 411	0	900	0 087	0 202	0 27
803	0 185	0 406	0	901	0 078	0 197	0 3852
804	0 178	0 402	0	902	0 074	0 198	4 6706
805	0 178	0 397	0	903	0 075	0 197	0 342
806	0 172	0 393	0	904	0 074	0 195	3 2884
807	0 184	0 388	0	905	0 064	0 194	0
808	0 169	0 384	0	906	0 062	0 193	0
809	0 186	0 378	0	907	0 058	0 192	1 6295
810	0 186	0 375	0	908	0 057	0 306	11 9479
811	0 182	0 371	0	909	0 138	0 388	10 3187
812	0 178	0 365	0	910	0 439	0 498	12 7028
813	0 179	0 362	0	911	0 521	0 408	0
814	0 18	0 358	0	912	0 289	0 475	10 8948
815	0 178	0 354	0	913	0 248	0 385	1 7278
816	0 178	0 35	0	914	0 168	0 302	0
817	0 178	0 346	0	915	0 12	0 25	0 8088
818	0 172	0 342	0	916	0 109	0 276	8 1531
819	0 172	0 338	0	917	0 105	0 251	2 2475
820	0 173	0 334	0	918	0 088	0 302	7 0892
821	0 175	0 33	0	919	0 079	0 417	9 8898
822	0 178	0 328	0	920	0 111	0 408	5 634
823	0 161	0 223	0	921	0 111	0 378	5 6174
824	0 172	0 319	0	922	0 106	0 309	0
825	0 172	0 315	0	923	0 109	0 412	9 7651
826	0 17	0 311	0	924	0 108	0 352	0 0488
827	0 17	0 308	0 62	925	0 097	0 288	1 575
828	0 172	0 305	1 4436	926	0 077	0 28	4 3719
829	0 171	0 302	0	927	0 074	0 234	3 6783
830	0 175	0 298	0 5144	928	0 075	0 219	2 1543
831	0 186	0 295	0	929	0 096	0 21	0 5066
832	0 169	0 327	10 7155	930	0 066	0 206	0
833	0 165	0 317	0	931	0 068	0 204	0
834	0 163	0 303	0	932	0 055	0 203	0
835	0 161	0 292	0	933	0 045	0 203	0
836	0 157	0 285	0	934	0 037	0 202	0
837	0 154	0 279	0	935	0 037	0 202	0
838	0 154	0 276	0	936	0 038	0 201	0
839	0 151	0 272	0	937	0 028	0 2	0
840	0 157	0 289	0	938	0 029	0 199	0
841	0 157	0 296	0	939	0 029	0 188	0
842	0 158	0 284	0	940	0 029	0 197	0
843	0 159	0 261	0	941	0 029	0 186	0
844	0 161	0 258	0	942	0 025	0 194	0
845	0 154	0 255	0	943	0 025	0 207	3 3542
846	0 155	0 253	0	944	0 025	0 203	1 125
847	0 151	0 25	0	945	0 027	0 199	1 519
848	0 149	0 247	0	946	0 027	0 194	0 6322
849	0 131	0 244	0	947	0 07	0 324	14 9406
850	0 123	0 242	0	948	0 168	0 363	6 6381
851	0 1	0 239	0	949	0 168	0 306	0 119
852	0 091	0 238	0	950	0 097	0 264	0 9327
853	0 077	0 234	0	951	0 087	0 282	4 9208
854	0 069	0 211	0	952	0 057	0 235	0 1584
855	0 068	0 276	0	953	0 087	0 213	0
856	0 087	0 226	0 27	954	0 037	0 199	0 3744
857	0 065	0 223	0	955	0 034	0 191	0
858	0 064	0 221	0	956	0 035	0 186	0
859	0 061	0 218	0	957	0 03	0 184	1 0434
860	0 064	0 216	1 071	958	0 031	0 198	2 9579
861	0 061	0 214	1 1128	959	0 028	0 192	1 4612
862	0 061	0 281	15 405	960	0 028	0 204	3 3092
863	0 064	0 265	0	961	0 025	0 197	0 7384
864	0 063	0 241	0	962	0 025	0 189	0 7274
865	0 062	0 224	0	963	0 028	0 183	0 2775
866	0 062	0 213	0	964	0 026	0 18	0
867	0 072	0 207	0	965	0 026	0 178	0
868	0 07	0 203	0	966	0 028	0 176	0
869	0 07	0 2	0	967	0 025	0 175	0
870	0 052	0 197	0 119	968	0 024	0 174	0
871	0 064	0 195	0 9952	969	0 024	0 172	0 072
872	0 064	0 193	0	970	0 016	0 171	0 16
873	0 064	0 191	0	971	0 016	0 17	0
874	0 063	0 189	0	972	0 016	0 169	0
875	0 063	0 188	0 9238	973	0 016	0 167	0
876	0 05	0 185	0	974	0 018	0 166	0
877	0 037	0 189	8 702	975	0 016	0 165	0 5124
878	0 035	0 194	0	976	0 017	0 163	0 4888
879	0 034	0 187	0	977	0 029	0 169	2 473

978	0.084	0.245	12.0/84	1076	0.653	0.615	0
979	0.239	0.228	1.7182	1077	0.64	0.517	0
980	0.181	0.2	0	1078	0.64	0.52	0
981	0.087	0.18	0	1079	0.637	0.522	0
982	0.087	0.169	0.5058	1080	0.624	0.524	0
983	0.081	0.388	19.6752	1081	0.623	0.526	0
984	0.278	0.547	12.8/58	1082	0.608	0.527	0
985	0.303	0.434	2.1524	1083	0.574	0.529	0
986	0.174	0.41	6.7043	1084	0.576	0.53	0
987	0.118	0.423	7.0124	1085	0.583	0.531	0
988	0.181	0.355	3.739	1086	0.583	0.532	0
989	0.201	0.322	4.6332	1087	0.559	0.533	0
990	0.224	0.584	13.7885	1088	0.558	0.534	0
991	0.241	0.539	5.034	1089	0.553	0.534	0
992	0.307	0.395	1.245	1090	0.548	0.535	0
993	0.389	0.403	6.4022	1091	0.529	0.535	0
994	0.573	1.794	32.4604	1092	0.548	0.535	0
995	7.657	4.225	42.1586	1093	0.546	0.535	0
996	3.547	3.775	11.704	1094	0.592	0.535	0
997	1.628	2.422	0.897	1095	0.554	0.534	0
998	1.027	1.409	0.2928	1096	0.581	0.969	0
999	0.705	0.814	0	1097	1.453	0.863	F1 1654
1000	0.525	0.501	0	1098	1.12	0.744	D 3126
1001	0.444	0.348	0.7106	1099	0.819	0.646	0
1002	0.4	0.277	0	1100	0.708	0.589	0
1003	0.388	0.246	0	1101	0.597	0.559	0
1004	0.36	0.234	0	1102	0.574	0.544	0
1005	0.3	0.231	2.1314	1103	0.576	0.536	0
1006	0.3	0.232	0	1104	0.586	0.532	0
1007	0.3	0.234	0.1206	1105	0.558	0.529	0
1008	0.323	0.238	0	1106	0.561	0.527	0
1009	0.355	0.241	0	1107	0.541	0.526	0
1010	0.392	0.414	5.7752	1108	0.522	0.524	0
1011	0.443	0.384	1.0378	1109	0.574	0.522	0
1012	0.607	0.512	5.9126	1110	0.568	0.52	0
1013	0.788	0.442	0.0432	1111	0.541	0.518	0
1014	0.598	0.367	0.4914	1112	0.45	0.516	0
1015	0.549	0.316	0	1113	0.454	0.514	0
1016	0.525	0.292	0	1114	0.454	0.512	0
1017	0.44	0.28	0	1115	0.43	0.51	0
1018	0.449	0.28	2.6246	1116	0.457	0.507	0
1019	0.452	0.278	0.4304	1117	0.448	0.505	0
1020	1.123	0.339	3.8314	1118	0.438	0.502	0
1021	1.044	0.413	4.3185	1119	0.431	0.419	0
1022	0.89	0.378	1.2.192	1120	0.427	0.490	0
1023	0.629	0.339	0.3498	1121	0.425	0.493	0
1024	0.573	0.313	0.1944	1122	0.418	0.491	0
1025	0.554	0.3	0	1123	0.414	0.487	0
1026	0.606	0.294	0.7046	1124	0.383	0.484	0
1027	0.542	0.292	0	1125	0.383	0.481	0
1028	0.499	0.292	0	1126	0.429	0.478	0
1029	0.49	0.292	0	1127	0.432	0.475	0
1030	0.419	0.293	0	1128	0.429	0.471	0
1031	0.543	0.72	13.1378	1129	0.424	0.468	0
1032	0.914	0.873	7.8158	1130	0.403	0.464	0
1033	1.163	0.946	7.9826	1131	0.392	0.481	0
1034	1.844	2.166	28.7066	1132	0.384	0.457	0
1035	2.852	4.13	36.6208	1133	0.375	0.453	0
1036	6.327	5.819	33.0206	1134	0.375	0.449	0
1037	5.583	4.128	1.789	1135	0.37	0.448	0
1038	2.598	2.929	7.3224	1136	0.369	0.442	0
1039	2.361	1.807	0.117	1137	0.363	0.438	0
1040	1.489	1.1	0	1138	0.367	0.434	0
1041	1.152	0.715	0	1139	0.367	0.43	0
1042	0.93	0.522	0	1140	0.367	0.428	0
1043	0.658	0.43	0	1141	0.348	0.422	0
1044	0.688	0.39	0	1142	0.278	0.418	0
1045	0.747	0.373	0	1143	0.24	0.414	0
1046	0.695	0.369	0	1144	0.228	0.41	0
1047	0.691	0.369	0	1145	0.199	0.405	0
1048	0.661	0.371	0	1146	0.196	0.401	0
1049	0.67	0.687	6.6507	1147	0.172	0.397	0
1050	7.005	4.825	48.0004	1148	0.159	0.393	0
1051	6.851	7.641	34.6501	1149	0.159	0.389	0
1052	8.663	7.412	17.4121	1150	0.154	0.385	0
1053	4.397	5.369	6.8102	1151	0.154	0.381	0
1054	3.398	3.269	0	1152	0.157	0.377	0
1055	2.33	1.912	0	1153	0.156	0.373	0
1056	1.785	1.183	0	1154	0.212	0.369	0
1057	1.347	0.782	0	1155	0.209	0.365	0
1058	1.106	0.599	0	1156	1.312	0.361	0
1059	0.998	0.515	0	1157	0.207	0.357	0
1060	0.948	0.48	0	1158	0.205	0.353	0
1061	0.879	0.487	0	1159	0.207	0.349	0
1062	0.842	0.485	0	1160	0.21	0.345	0
1063	0.797	0.486	0	1161	0.201	0.342	0
1064	0.801	0.47	0	1162	0.171	0.338	0
1065	0.783	0.474	0	1163	0.164	0.334	0
1066	0.774	0.479	0	1164	0.144	0.33	0
1067	0.764	0.483	0	1165	0.128	0.327	0
1068	0.774	0.488	0	1166	0.115	0.323	0
1069	0.76	0.492	0	1167	0.11	0.319	0
1070	0.739	0.498	0	1168	0.088	0.318	0
1071	0.73	0.499	0	1169	0.088	0.312	0
1072	0.72	0.503	0	1170	0.087	0.308	0
1073	0.71	0.506	0	1171	0.068	0.305	0
1074	0.695	0.509	0	1172	0.066	0.301	0
1075	0.68	0.512	0	1173	0.068	0.298	0

1174	0.067	0.295	0	1272	0.008	0.108	0.003
1175	0.063	0.291	0	1273	0.004	0.105	0
1176	0.061	0.288	0	1274	0.004	0.104	0
1177	0.061	0.285	0	1275	0.005	0.102	0.12
1178	0.061	0.281	0	1276	0.004	0.103	1.459
1179	0.053	0.278	0	1277	0.004	0.102	1.0572
1180	0.053	0.275	0	1278	0.004	0.111	4.0401
1181	0.053	0.272	0	1279	0.023	0.478	33.4039
1182	0.061	0.269	0	1280	0.082	0.59	12.1592
1183	0.061	0.265	0	1281	0.083	0.434	0
1184	0.061	0.262	0	1282	0.055	0.29	0
1185	0.053	0.259	0	1283	0.035	0.201	0
1186	0.043	0.258	0	1284	0.037	0.152	2.0096
1187	0.045	0.253	0	1285	0.023	0.128	1.6986
1188	0.044	0.25	0	1286	0.024	0.116	1.319
1189	0.042	0.248	0	1287	0.019	0.149	5.2954
1190	0.04	0.245	0	1288	0.019	0.24	6.6587
1191	0.033	0.242	0	1289	0.021	0.351	10.1602
1192	0.03	0.239	0	1290	0.016	0.294	4.172
1193	0.03	0.236	0	1291	0.03	0.362	9.5199
1194	0.078	0.234	0	1292	0.055	0.375	5.4768
1195	0.029	0.231	0	1293	0.035	0.245	1.9418
1196	0.029	0.228	0	1294	0.03	0.187	2.5318
1197	0.028	0.226	0	1295	0.044	0.154	0.1742
1198	0.027	0.223	0	1296	0.061	0.137	0
1199	0.026	0.22	0	1297	0.044	0.13	0
1200	0.025	0.218	0	1298	0.034	0.128	0
1201	0.025	0.215	0	1299	0.028	0.125	0.081
1202	0.024	0.213	0	1300	0.027	0.125	0.1872
1203	0.024	0.21	0	1301	0.017	0.125	0.3833
1204	0.025	0.208	0	1302	0.017	0.126	0.298
1205	0.025	0.206	0	1303	0.018	0.267	11.7584
1206	0.025	0.203	0	1304	0.017	0.232	2.2346
1207	0.023	0.201	0	1305	0.017	0.19	0.162
1208	0.022	0.198	0	1306	0.017	0.181	0
1209	0.022	0.196	0	1307	0.016	0.145	0
1210	0.022	0.194	0	1308	0.011	0.138	0.0624
1211	0.022	0.192	0	1309	0.005	0.189	7.3698
1212	0.021	0.189	0	1310	0.005	0.208	3.7672
1213	0.02	0.187	0	1311	0.005	0.249	6.5874
1214	0.02	0.185	0	1312	0.017	0.35	9.8708
1215	0.019	0.183	0	1313	0.024	0.288	2.0418
1216	0.019	0.181	0	1314	0.024	0.222	2.147
1217	0.019	0.179	0	1315	0.017	0.179	0.9182
1218	0.018	0.177	0	1316	0.017	0.156	0
1219	0.019	0.175	0.7064	1317	0.017	0.21	8.0149
1220	0.019	0.173	0.2285	1318	0.009	0.191	2.0531
1221	0.019	0.171	0.476	1319	0.009	0.385	11.6094
1222	0.02	0.170	0	1320	0.013	0.324	3.3958
1223	0.019	0.167	0	1321	0.013	0.389	7.6073
1224	0.019	0.166	2.7886	1322	0.013	0.373	5.9108
1225	0.019	0.165	0	1323	0.009	0.38	6.2221
1226	0.019	0.163	0	1324	0.009	0.296	0.8417
1227	0.019	0.16	0.238	1325	0.013	0.248	3.7784
1228	0.018	0.158	0	1326	0.006	0.204	0.059
1229	0.016	0.156	0	1327	0.007	0.177	0
1230	0.016	0.155	0	1328	0.004	0.163	1.4815
1231	0.011	0.153	0	1329	0.004	0.184	4.0278
1232	0.011	0.151	0	1330	0.004	0.176	0.9108
1233	0.011	0.15	0	1331	0.004	0.167	0.26
1234	0.012	0.148	1.19	1332	0.004	0.161	0.3782
1235	0.011	0.147	0	1333	0.003	0.158	0
1236	0.012	0.145	0	1334	0.002	0.157	0.024
1237	0.011	0.143	0	1335	0.002	0.157	0.008
1238	0.012	0.143	0	1336	0.002	0.157	0
1239	0.012	0.14	0	1337	0.002	0.157	0
1240	0.012	0.185	13.5417	1338	0.002	0.157	0
1241	0.025	0.174	0	1339	0.021	0.187	0.009
1242	0.061	0.158	0	1340	0.083	0.318	12.3817
1243	0.062	0.147	0.225	1341	0.043	0.285	0.7086
1244	0.028	0.14	0	1342	0.068	0.734	0.0045
1245	0.022	0.138	0	1343	0.043	0.199	0
1246	0.019	0.146	4.3854	1344	0.025	0.178	0.117
1247	0.012	0.141	0	1345	0.021	0.168	0.6034
1248	0.012	0.146	3.8787	1346	0.01	0.162	0.7124
1249	0.012	0.14	0.111	1347	0.01	0.159	0
1250	0.078	0.143	3.3326	1348	0.01	0.158	0.3094
1251	0.081	0.138	0.5812	1349	0.01	0.178	3.3308
1252	0.055	0.132	0	1350	0.01	0.223	5.8456
1253	0.019	0.129	0	1351	0.012	0.207	0.45
1254	0.019	0.128	0	1352	0.011	0.186	0.033
1255	0.018	0.124	0	1353	0.029	0.172	1.1128
1256	0.017	0.123	0	1354	0.029	0.178	3.0144
1257	0.017	0.121	0	1355	0.081	0.247	7.4574
1258	0.013	0.12	0	1356	0.164	0.289	6.0612
1259	0.011	0.119	0	1357	0.13	0.287	4.5166
1260	0.011	0.118	0	1358	0.119	0.24	0.8775
1261	0.01	0.118	0	1359	0.077	0.203	0.149
1262	0.01	0.115	0.5474	1360	0.055	0.18	0.8015
1263	0.01	0.114	0	1361	0.031	0.168	0.009
1264	0.009	0.113	0	1362	0.029	0.162	0.1388
1265	0.01	0.112	0	1363	0.026	0.159	0
1266	0.01	0.11	0.0345	1364	0.011	0.158	0
1267	0.011	0.109	0	1365	0.007	0.157	0
1268	0.011	0.129	3.0048	1366	0.007	0.156	0.1072
1269	0.009	0.125	1.0056	1367	0.022	0.205	6.0284
1270	0.008	0.117	0	1368	0.075	0.38	14.1646
1271	0.008	0.111	0	1369	0.682	0.447	8.4083

1370	0.652	0.455	0.315	1488	0.5	0.399	0
1371	0.43	0.35	1.5442	1469	0.491	0.398	0
1372	0.311	0.442	0.47	1470	0.519	0.397	0
1373	0.418	0.388	0.148	1471	0.674	0.186	0
1374	0.271	0.273	0.2478	1472	0.627	0.395	0
1375	0.193	0.236	2.5458	1473	0.528	0.393	0
1376	0.222	0.289	5.161	1474	0.522	0.392	0
1377	0.432	0.31	4.0686	1475	0.524	0.39	0
1378	0.732	1.427	34.1823	1476	0.527	0.389	0
1379	1.51	1.275	5.0408	1477	0.538	0.387	0
1380	0.683	0.658	0.849	1478	0.538	0.385	0
1381	0.688	0.69	5.5889	1479	0.575	0.384	0
1382	0.578	0.481	1.2605	1480	0.568	0.382	0
1383	0.449	0.341	2.142	1481	0.569	0.379	0
1384	0.431	0.614	9.863	1482	0.51	0.377	0
1385	0.548	0.685	5.6964	1483	0.486	0.375	0
1386	0.511	0.506	0	1484	0.492	0.373	0
1387	0.375	0.37	0	1485	0.485	0.371	0
1388	0.351	0.288	0	1486	0.484	0.368	0
1389	0.326	0.245	0	1487	0.485	0.366	0
1390	0.299	0.225	0	1488	0.519	0.363	0
1391	0.286	0.218	0	1489	0.509	0.361	0
1392	0.248	0.214	0	1490	0.512	0.358	0
1393	0.245	0.214	0	1491	0.498	0.355	0
1394	0.254	0.215	0	1492	0.494	0.353	0
1395	0.283	0.217	0	1493	0.491	0.35	0
1396	0.288	0.218	0	1494	0.492	0.347	0
1397	0.298	0.22	0	1495	0.487	0.344	0
1398	0.332	0.222	0	1496	0.491	0.342	0
1399	0.324	0.223	0	1497	0.482	0.339	0
1400	0.305	0.225	0	1498	0.486	0.336	0
1401	0.287	0.228	0	1499	0.485	0.333	0
1402	0.293	0.227	0	1500	0.479	0.33	0
1403	0.287	0.228	0	1501	0.483	0.327	0
1404	0.326	0.229	0.084	1502	0.464	0.324	0
1405	0.38	0.229	0	1503	0.46	0.321	0
1406	0.359	0.21	0	1504	0.454	0.317	0
1407	0.359	0.23	0	1505	0.452	0.314	0
1408	0.384	0.444	10.3184	1506	0.452	0.311	0
1409	0.548	0.402	1.3684	1507	0.455	0.308	0
1410	0.607	0.335	0	1508	0.452	0.305	0
1411	0.611	0.288	1.3432	1509	0.453	0.302	0
1412	0.493	0.261	1.1482	1510	0.449	0.299	0
1413	0.471	0.247	0	1511	0.44	0.296	0
1414	0.397	0.24	0	1512	0.41	0.293	0
1415	0.441	0.48	11.3748	1513	0.364	0.289	0
1416	0.824	1.197	24.7596	1514	0.356	0.286	0
1417	16.057	5.655	79.892	1515	0.343	0.283	0
1418	9.686	0.348	44.0184	1516	0.342	0.28	0
1419	5.012	5.98	3.9125	1517	0.341	0.277	0
1420	3.28	3.455	1.7955	1518	0.335	0.274	0
1421	2.743	2.512	7.9258	1519	0.333	0.271	0
1422	0.419	1.545	0.852	1520	0.342	0.268	0
1423	1.808	0.938	0	1521	0.327	0.265	0
1424	1.361	0.808	0	1522	0.327	0.267	3.2258
1425	1.037	0.444	0	1523	0.325	0.263	0
1426	1.015	0.367	0.173	1524	0.337	0.259	0
1427	0.927	0.334	0	1525	0.415	0.255	0
1428	0.905	0.322	0.117	1526	0.425	0.252	0
1429	0.861	0.32	0	1527	0.366	0.249	0
1430	0.71	0.322	0	1528	0.343	0.246	0
1431	0.856	0.328	0	1529	0.336	0.243	0
1432	0.842	0.331	0	1530	0.335	0.241	0
1433	0.701	0.335	0	1531	0.331	0.238	0
1434	0.692	0.34	0	1532	0.309	0.235	0
1435	0.688	0.345	0	1533	0.309	0.233	0
1436	0.662	0.349	0	1534	0.309	0.23	0
1437	0.661	0.333	0	1535	0.304	0.228	0
1438	0.68	0.357	0	1536	0.3	0.226	0
1439	0.651	0.361	0	1537	0.273	0.223	0
1440	0.641	0.365	0	1538	0.282	0.22	0
1441	0.651	0.368	0	1539	0.237	0.218	0
1442	0.651	0.371	0	1540	0.234	0.218	0
1443	0.651	0.374	0	1541	0.237	0.213	0
1444	0.657	0.377	0	1542	0.23	0.21	0
1445	0.638	0.38	0	1543	0.202	0.208	0
1446	0.622	0.382	0	1544	0.199	0.205	0
1447	0.578	0.345	0	1545	0.199	0.203	0
1448	0.574	0.387	0	1546	0.201	0.201	0
1449	0.558	0.389	0	1547	0.199	0.198	0
1450	0.552	0.391	0	1548	0.199	0.198	0
1451	0.543	0.392	0	1549	0.198	0.194	0
1452	0.453	0.394	0	1550	0.199	0.192	0
1453	0.392	0.395	0	1551	0.198	0.19	0
1454	0.359	0.397	0	1552	0.201	0.187	0
1455	0.342	0.398	0	1553	0.183	0.185	0
1456	0.276	0.399	0	1554	0.184	0.183	0
1457	0.232	0.399	0	1555	0.188	0.181	0
1458	0.229	0.4	0	1556	0.188	0.179	0
1459	0.224	0.4	0	1557	0.191	0.177	0
1460	0.224	0.401	0	1558	0.189	0.175	0
1461	0.252	0.401	0	1559	0.189	0.173	0
1462	0.257	0.401	0	1560	0.19	0.171	0
1463	0.258	0.401	0	1561	0.19	0.169	0
1464	0.257	0.401	0	1562	0.19	0.167	0
1465	0.257	0.401	0	1563	0.193	0.165	0.6875
1466	0.258	0.4	0	1564	0.195	0.163	0.036
1467	0.25	0.399	0	1565	0.195	0.164	2.8424

1566	0.195	0.195	10.9558	1654	0.007	0.107	0.6784
1567	0.215	0.169	0	1665	0.007	0.109	2.3441
1568	0.216	0.176	0	1666	0.008	0.109	0.0913
1569	0.188	0.168	0	1667	0.008	0.117	0.3411
1570	0.159	0.159	0	1668	0.007	0.212	7.1468
1571	0.12	0.156	0	1669	0.008	0.183	2.9206
1572	0.124	0.153	0	1670	0.008	0.149	0.5382
1573	0.122	0.151	0	1671	0.008	0.127	0.18
1574	0.124	0.15	0	1672	0.008	0.115	0.2834
1575	0.117	0.145	0	1673	0.008	0.108	0
1576	0.116	0.147	0	1674	0.008	0.122	3.3736
1577	0.116	0.145	0	1675	0.008	0.117	0.3868
1578	0.11	0.144	0	1676	0.008	0.111	0.204
1579	0.077	0.142	0	1677	0.008	0.107	0
1580	0.082	0.141	0	1678	0.008	0.104	0.2856
1581	0.061	0.14	0	1679	0.008	0.103	0
1582	0.082	0.138	0	1680	0.008	0.102	0.7104
1583	0.062	0.137	0	1681	0.008	0.107	1.9388
1584	0.062	0.135	0	1682	0.008	0.105	0.009
1585	0.056	0.134	0.7748	1683	0.008	0.103	1.0946
1586	0.053	0.133	0	1684	0.008	0.109	2.7432
1587	0.052	0.131	0	1685	0.008	0.108	0.0894
1588	0.038	0.13	0	1686	0.007	0.103	0.7962
1589	0.038	0.128	0	1687	0.008	0.108	2.1368
1590	0.038	0.127	0	1688	0.008	0.109	1.6748
1591	0.037	0.125	0.425	1689	0.008	0.123	1.7012
1592	0.03	0.124	0	1690	0.033	0.117	0.4158
1593	0.029	0.123	0	1691	0.054	0.109	0.045
1594	0.028	0.121	0	1692	0.042	0.104	0
1595	0.029	0.12	0	1693	0.038	0.101	0
1596	0.028	0.134	7.8989	1694	0.036	0.099	0
1597	0.078	0.129	0.024	1695	0.035	0.097	0.3054
1598	0.028	0.124	0	1696	0.035	0.096	0
1599	0.04	0.119	0	1697	0.033	0.098	0
1600	0.038	0.116	0	1698	0.028	0.095	0
1601	0.303	0.504	37.5194	1699	0.028	0.095	0
1602	1.372	0.427	0	1700	0.022	0.118	5.2870
1603	0.399	0.303	0	1701	0.03	0.167	8.7593
1604	0.154	0.216	0	1702	0.397	0.468	23.5681
1605	0.078	0.165	0	1703	0.893	1.018	27.0942
1606	0.081	0.14	0	1704	0.645	1.702	27.4521
1607	0.043	0.127	0	1705	0.646	1.242	0.278
1608	0.04	0.363	21.358	1706	0.621	0.941	7.5968
1609	0.036	0.312	0	1707	0.61	0.596	0
1610	0.035	0.378	12.1778	1708	0.349	0.368	0
1611	0.034	0.295	0	1709	0.342	0.242	3.3882
1612	0.033	0.219	0	1710	0.339	0.287	6.0708
1613	0.033	0.171	0	1711	0.331	0.236	3.3775
1614	0.032	0.145	0	1712	0.325	0.19	0.5211
1615	0.031	0.132	0	1713	0.289	0.162	0
1616	0.031	0.125	1.7235	1714	0.282	0.148	0
1617	0.031	0.122	0.025	1715	0.289	0.142	0
1618	0.031	0.12	0	1716	0.243	0.14	0
1619	0.031	0.119	0	1717	0.165	0.141	0
1620	0.03	0.118	0	1718	0.15	0.142	0
1621	0.03	0.117	0	1719	0.143	0.144	0.1456
1622	0.03	0.116	0.2574	1720	0.142	0.146	0
1623	0.03	0.115	0	1721	0.14	0.147	0
1624	0.024	0.115	0	1722	0.138	0.408	12.4668
1625	0.02	0.114	0.1888	1723	0.375	0.359	2.3884
1626	0.015	0.113	0.2092	1724	0.301	0.595	13.1064
1627	0.015	0.112	0.1872	1725	0.903	0.548	9.2836
1628	0.015	0.111	0.609	1726	0.912	1.221	23.619
1629	0.014	0.124	5.852	1727	0.938	0.857	1.5408
1630	0.014	0.12	0	1728	0.94	0.621	2.1354
1631	0.014	0.115	0.6776	1729	0.772	0.412	0.841
1632	0.014	0.111	0	1730	0.563	0.291	0.0792
1633	0.014	0.106	0.4148	1731	0.454	0.231	0
1634	0.01	0.106	0	1732	0.459	0.385	8.029
1635	0.01	0.105	0	1733	0.903	0.353	3.843
1636	0.01	0.103	0	1734	0.898	0.4	8.1892
1637	0.01	0.102	0	1735	0.957	0.331	0
1638	0.009	0.101	0	1736	0.662	0.3	3.1398
1639	0.008	0.101	0.702	1737	0.684	0.528	8.7653
1640	0.006	0.103	2.4488	1738	0.981	0.965	13.4602
1641	0.006	0.112	4.6572	1739	0.933	0.776	2.6838
1642	0.007	0.151	9.0113	1740	0.888	0.542	0.7576
1643	0.028	0.117	5.8254	1741	0.877	1.11	16.2915
1644	0.021	0.198	8.9798	1742	0.973	0.86	0.6842
1645	0.02	0.249	8.7448	1743	1.003	3.6	48.8952
1646	0.044	0.268	7.0054	1744	8.826	5.84	36.1903
1647	0.03	0.211	0.6384	1745	4.893	8.252	22.298
1648	0.016	0.182	0.202	1746	2.078	5.093	11.1437
1649	0.015	0.132	0	1747	2.058	3.179	3.2564
1650	0.01	0.116	0.0045	1748	1.98	1.825	0.9994
1651	0.01	0.106	1.2432	1749	1.941	1.047	2.7462
1652	0.01	0.104	0.471	1750	2.277	0.992	8.1814
1653	0.01	0.103	2.1916	1751	3.31	1.944	13.2374
1654	0.015	0.102	0.2344	1752	2.628	2.382	9.9803
1655	0.014	0.117	3.6253	1753	1.795	1.692	2.5164
1656	0.013	0.114	1.8008	1754	0.833	1.087	1.0048
1657	0.013	0.109	0.9256	1755	0.781	0.713	0.6948
1658	0.012	0.105	0.389	1756	0.807	0.511	0
1659	0.012	0.112	2.8422	1757	0.498	0.413	0
1660	0.011	0.144	5.6871	1758	0.43	0.369	0.354
1661	0.011	0.134	0	1759	0.349	0.352	0
1662	0.007	0.121	0.618	1760	0.308	0.347	0
1663	0.007	0.112	0.18	1761	0.25	0.349	0

1762	0.24	0.363	0
1763	0.244	1.120	10.4608
1764	0.243	0.882	0
1765	0.243	0.743	0
1766	0.237	0.578	0.4748
1767	0.232	0.482	1.4792
1768	0.23	0.436	1.1105
1769	0.229	0.415	0
1770	0.235	0.408	0
1771	0.23	0.407	0
1772	0.237	0.409	0
1773	0.317	0.413	1.2511
1774	0.394	0.418	0
1775	0.357	0.42	2.2892
1776	0.351	1.095	10.9088
1777	0.384	1.843	12.7385
1778	0.629	1.618	4.6882
1779	0.618	1.162	0
1780	0.618	0.812	0
1781	0.582	0.643	0
1782	0.585	0.544	0
1783	0.676	0.497	0
1784	0.561	0.472	0
1785	0.557	0.469	0
1786	0.557	0.465	0
1787	0.545	0.467	0
1788	0.53	0.469	0
1789	0.531	0.471	0
1790	0.526	0.473	0
1791	0.501	0.475	0
1792	0.501	0.476	0
1793	0.5	0.476	0
1794	0.5	0.48	0
1795	0.499	0.461	0
1796	0.495	0.462	0
1797	0.489	0.463	0
1798	0.485	0.464	0
1799	0.487	0.464	0
1800	0.84	3.799	52.5474
1801	3.882	5.057	24.4718
1802	6.289	3.907	5.5695
1803	3.235	2.504	0
1804	2.058	1.561	0
1805	1.952	1.031	0
1806	1.806	0.759	0
1807	1.798	0.626	0
1808	1.788	0.595	0
1809	1.336	0.537	0
1810	0.808	0.528	0
1811	0.778	0.523	0
1812	0.759	0.522	0
1813	0.753	0.523	0
1814	0.734	0.525	0
1815	0.731	0.528	0
1816	0.714	0.528	0
1817	0.708	0.529	0
1818	0.682	0.531	0
1819	0.678	0.532	0
1820	0.75	0.533	0
1821	0.739	0.534	0
1822	0.724	0.534	0
1823	0.592	0.535	0
1824	0.635	0.535	0
1825	0.721	0.538	0
1826	0.722	0.538	0

**Annexure - JII**

**Daily observed and modelled runoff for Gundlakamma at Tammavaram for Validation with catchment average rainfall**

Day No	Validation from 1 Jan 1994 to 30 Nov 1997	97	98	99	0 218	0 218	0 189
Day No	Observed runoff (mm)	Modelled runoff	Rainfall (mm)	97	98	99	0 218
1	0.73	0	100				0.185
2	0.73	0	101				0.185
3	0.679	0	102				0.179
4	0.676	0	103				0.174
5	0.646	0	104				0.175
6	0.653	0	105				0.141
7	0.658	0	106				0.117
8	0.652	0	107				0.104
9	0.651	0	108				0.088
10	0.63	0	109				0.087
11	0.607	0	110				0.087
12	0.613	0	111				0.088
13	0.583	0	112				0.088
14	0.579	0	113				0.085
15	0.552	0	114				0.085
16	0.508	0	115				0.084
17	0.492	0	116				0.084
18	0.491	0.2195	117				0.067
19	0.491	0.315	118				0.103
20	0.498	0	119				0.117
21	0.498	0	120				0.115
22	0.485	0	121				0.116
23	0.485	0	122				0.116
24	0.441	0	123				0.103
25	0.375	0	124				0.101
26	0.397	0	125				0.01
27	0.375	0	126				0.004
28	0.39	0	127				0.099
29	0.374	0	128				0.089
30	0.359	0	129				0.033
31	0.348	0	130				0.03
32	0.337	0	131				0.029
33	0.32	0	132				0.028
34	0.274	0	133				0.03
35	0.319	0	134				0.03
36	0.315	0	135				0.03
37	0.314	0	136				0.03
38	0.314	0	137				0.028
39	0.312	0	138				0.029
40	0.319	0	139				0.029
41	0.329	3.7518	140				0.029
42	0.384	5.8488	141				0.029
43	0.938	7.8568	142				0.02
44	0.682	8.6541	142				0.02
45	0.712	0	143				0.019
46	0.704	0	144				0.018
47	0.475	0	145				0.018
48	0.395	0	146				0.209
49	0.389	0	147				0.638
50	0.384	0	148				0.218
51	0.77	0	149				0.18
52	0.268	0	150				0.105
53	0.297	0	151				0.088
54	0.258	0	152				0.065
55	0.21	0	153				0.059
56	0.173	0	154				0.058
57	0.172	0	155				0.052
58	0.165	0	156				0.039
59	0.163	0	157				0.027
60	0.161	0	158				0.028
61	0.148	0	159				0.018
62	0.137	0	160				0.017
63	0.128	0	161				0.025
64	0.124	0	162				0.024
65	0.152	0	163				0.024
66	0.175	0	164				0.018
67	0.165	0	165				0.018
68	0.167	0	166				0.019
69	0.155	0	167				0.017
70	0.151	0	168				0.017
71	0.145	0	169				0.017
72	0.134	0	170				0.017
73	0.134	0	171				0.017
74	0.138	0	172				0.018
75	0.133	0	173				0.009
76	0.159	0	174				0.009
77	0.702	0	175				0.009
78	0.227	0	176				0.008
79	0.241	0	177				0.008
80	0.215	0	178				0.008
81	0.224	0	179				0.008
82	0.247	0	180				0.008
83	0.246	0	181				0.007
84	0.246	0	182				0.006
85	0.243	0	183				0.006
86	0.243	0	184				0.006
87	0.745	0	185				0.006
88	0.235	0	186				0.007
89	0.232	0	187				0.008
90	0.231	0	188				0.006
91	0.229	0	189				0.006
92	0.227	9.3472	190				0.006
93	0.226	0.8244	191				0.006
94	0.226	2.5186	192				0.006
95	0.244	0	193				0.006
96	0.242	0	194				0.006

195	0.006	3.163	293	1.542	1.371	3.66
196	0.006	0.624	294	1.155	0.93	0
197	0.005	0	295	0.842	0.015	0
198	0.003	0	296	0.708		0
199	0.005	0.0104	297	0.537		10.3624
200	0.004	0.9718	298	0.681		5.3176
201	0.004	0.6036	299	1.329	0.737	0.9116
202	0.004	0.8765	300	0.979		0.3418
203	0.004	0	301	0.769	1.178	12.0445
204	0.003	0.6038	302	1.35	1.148	5.098
205	0.003	11.4086	303	1.131	0.942	4.1888
206	0.003	2.1532	304	0.905	1.502	11.9604
207	0.003	3.5368	305	1.371	11.819	87.0108
208	0.003	0.6812	306	18.756	16.92	47.8965
209	0.003	7.1582	307	8.275	11.683	3.6292
210	0.003	0.1645	308	3.995	6.945	1.832
211	0.003	0	309	3.06	3.79	1.9066
212	0.003	0.1162	310	2.482	2.778	7.316
213	0.003	0.135	311	3.68	3.73	13.8044
214	0.002	0	312	2.986	2.975	4.9298
215	0.002	0.1788	313	2.281	1.929	1.9858
216	0.002	0.0476	314	2.112	2.114	7.5906
217	0.002	0	315	2.327	1.535	3.1136
218	0.002	0	316	1.65	1.043	0
219	0.002	0	317	1.158	0.744	0
220	0.002	0.024	318	0.894		0.971
221	0.002	0.731	319	0.851		0
222	0.002	0.1666	320	0.631		0
223	0.002	0.9364	321	0.564		1.848
224	0.09	2.008	322	0.603		0
225	0.004	1.813	323	0.476		0
226	0.001	16.1148	324	0.474		0.0824
227	0.06	0	325	0.479		0.1468
228	0.039	0	326	0.528		0
229	0.024	3.9038	327	0.607		0
230	0.022	0.4486	328	0.582		0
231	0.019	2.0371	329	0.542		0
232	0.014	0.0804	330	0.534		0
233	0.051	1.1542	331	0.531		0
234	0.06	8.4527	332	0.53		0
235	0.062	0	333	0.524		0
236	0.058	0.9238	334	0.524		0
237	0.058	2.759	335	0.525		0
238	0.064	10.5718	336	0.518		0
239	0.066	7.0358	337	0.524		0
240	0.081	0.8912	338	0.524		0
241	0.048	0.298	339	0.518		0
242	0.037	0	340	0.498		0
243	0.036	0	341	0.454		0
244	0.037	0.037	342	0.442		0
245	0.016	2.3152	343	0.465		0
246	0.019	0.6846	344	0.458		0
247	0.019	0	345	0.456		0
248	0.019	0	346	0.456		0
249	0.013	0	347	0.452		0
250	0.012	0	348	0.442		0
251	0.01	0.325	349	0.44		0
252	0.006	0.149	350	0.436		0
253	0.004	0.324	351	0.428		0
254	0.004	0	352	0.418		0
255	0.004	2.0198	353	0.416		0
256	0.019	0.2474	354	0.413		0
257	0.019	1.959	355	0.413		1.206
258	0.05	0.127	356	0.408		0.087
259	0.047	0	357	0.409		0
260	0.03	0.108	358	0.412		0
261	0.028	0.7784	359	0.412		0
262	0.03	0	360	0.412		0
263	0.028	0	361	0.412		0
264	0.028	0.1298	362	0.41		0
265	0.027	0	363	0.401		0
266	0.025	0	364	0.404		0
267	0.04	0	365	0.427		0
268	0.04	0.3332	366	0.427		0
269	0.043	8.6034	367	0.412		0
270	0.066	1.3855	368	0.409		0
271	0.066	0	369	0.407		0
272	0.056	0	370	0.41		0
273	0.094	3.0227	371	0.398		0
274	0.056	2.6553	372	0.398		0
275	0.116	1.809	373	0.398		0.1844
276	0.146	3.4549	374	0.655	1.083	19.108
277	0.366	22.6583	375	2.256	1.21	0.126
278	1.783	2.193	376	1.538	0.982	0.6189
279	5.978	5.103	377	0.918		0.033
280	2.379	3.806	378	0.797		0.6666
281	1.535	2.294	379	0.785		0
282	0.772	2.013	380	0.785		0.0744
283	1.53	1.32	381	0.7		0.2469
284	1.532	1.633	382	0.747		1.206
285	1.283	1.166	383	0.774		0
286	0.914	0	384	0.708		0
287	0.829	0	385	0.599		0
288	0.809	10.0682	386	0.501		0
289	0.723	1.0942	387	0.501		0
290	0.656	0	388	0.49		0
291	0.441	0.3726	389	0.47		0
292	0.477	1.605	390	0.471		0

391	0.471	0	489	0.036	0
392	0.449	0	490	0.033	1.395
393	0.464	0	491	0.038	4.975
394	0.431	0	492	0.112	21.7724
395	0.411	0	493	2.736	21.8861
396	0.428	0	494	2.191	27.1814
397	0.428	0	495	1.437	2.108
398	0.423	0	496	0.904	0.3198
399	0.401	0	497	0.251	3.8798
400	0.394	0	498	0.223	0
401	0.382	0	499	0.178	5.7934
402	0.333	0	500	0.299	12.7968
403	0.343	0	501	0.446	0
404	0.343	0	502	0.299	0
405	0.327	0	503	0.21	0
406	0.327	0	504	0.189	0
407	0.327	0	505	0.185	0
408	0.314	0	506	0.186	0
409	0.314	0	507	0.121	0
410	0.32	0	508	0.115	0
411	0.32	0	509	0.111	0
412	0.303	0	510	0.094	0
413	0.328	0	511	0.094	0
414	0.321	0	512	0.079	0
415	0.307	0	513	0.079	0
416	0.307	0	514	0.078	0
417	0.309	0	515	0.078	0
418	0.3	0	516	0.069	0
419	0.284	0	517	0.059	0
420	0.277	0	518	0.055	0
421	0.265	0	519	0.045	0
422	0.261	0	520	0.044	0
423	0.261	0	521	0.041	0
424	0.251	0	522	0.038	0
425	0.249	0	523	0.034	0
426	0.249	0	524	0.034	0
427	0.245	0	525	0.034	0
428	0.245	0	526	0.036	0
429	0.243	0	527	0.035	0
430	0.245	0	528	0.034	0
431	0.202	0	529	0.03	0
432	0.193	0	530	0.028	1.112
433	0.177	0	531	0.028	0.4602
434	0.173	0	532	0.024	0
435	0.165	0	533	0.022	6.2754
436	0.168	0	534	0.022	1.5298
437	0.167	0	535	0.022	0.268
438	0.171	0	536	0.022	0
439	0.167	0	537	0.026	5.8071
440	0.178	0	538	0.048	8.4258
441	0.182	0	539	0.046	0
442	0.182	0	540	0.043	0.728
443	0.183	0	541	0.044	2.8838
444	0.187	0	542	0.044	1.612
445	0.184	0	543	0.044	2.7132
446	0.178	0	544	0.055	5.4084
447	0.177	0	545	0.072	0.7628
448	0.176	0	546	0.072	2.7241
449	0.176	0	547	0.053	5.7026
450	0.178	0	548	0.045	0
451	0.176	0	549	0.042	0
452	0.174	0	550	0.038	0
453	0.171	0	551	0.034	0
454	0.171	0	552	0.028	2.4978
455	0.171	0	553	0.045	13.3128
456	0.18	0	554	0.11	1.9073
457	0.18	0	555	0.047	0
458	0.176	0	556	0.044	3.5552
459	0.177	0	557	0.04	5.0172
460	0.178	0	558	0.055	7.294
461	0.178	0	559	0.054	2.8006
462	0.175	0	560	0.04	0
463	0.175	0	561	0.039	2.4839
464	0.175	0	562	0.036	0.054
465	0.17	0	563	0.028	0.8536
466	0.173	0	564	0.024	1.521
467	0.134	0	565	0.025	8.7588
468	0.126	0	566	0.035	9.219
469	0.115	0	567	0.047	5.3685
470	0.113	0	568	0.047	2.6142
471	0.112	0	569	0.046	7.4208
472	0.103	0	570	0.046	15.2331
473	0.102	0	571	0.168	1.2508
474	0.099	0	572	0.445	13.2468
475	0.094	0	573	0.225	7.7151
476	0.081	0	574	0.202	17.035
477	0.112	0	575	3.905	2.983
478	0.097	0	576	3.21	2.334
479	0.085	0	577	1.413	1.46
480	0.077	0	578	1.478	0.862
481	0.075	0	579	0.408	0.5908
482	0.073	0	580	0.282	0
483	0.075	0	581	0.198	0.7352
484	0.067	0	582	0.172	0
485	0.065	0	583	0.185	0
486	0.083	0	584	0.115	0.128
487	0.05	0	585	0.109	3.6884
488	0.043	0	586	0.111	0

587	0.092		0.27	685	0.282	0
588	0.431		17.0482	686	0.257	0
589	0.329		0.8312	687	0.271	0.3764
590	0.193		1.9129	688	0.309	0
591	0.109		0.0792	689	0.305	5.5418
592	0.11		0	690	0.313	0.803
593	0.074		0	691	0.512	
594	0.057		4.3348	692	0.517	2.0684
595	0.056		5.2226	693	0.863	0
596	0.068		3.0353	694	0.804	0
597	0.154		0.9312	695	0.441	0
598	0.165		3.3334	696	0.361	0
599	0.18		4.6764	697	0.389	0
600	0.122		0.4248	698	0.33	0
601	0.186		9.4828	699	0.349	0
602	0.242		9.1284	700	0.308	0
603	0.393		1.823	701	0.303	0
604	0.265	2.112	37.5986	702	0.335	0
605	0.887	1.721	4.38	703	0.343	0
606	1.103	2.284	21.9235	704	0.385	0
607	1.22	2.833	20.1735	705	0.389	0
608	1.611	2.006	3.4468	706	0.384	0
609	0.877	1.252	1.809	707	0.397	0
610	0.533		0	708	0.39	
611	0.364		0	709	0.388	0
612	0.26		6.8898	710	0.38	0
613	0.258		0	711	0.39	0
614	0.2	0	0	712	0.399	0
615	0.146		0	713	0.435	0
616	0.122		0	714	0.487	0
617	0.093		0.54	715	0.485	0
618	0.094		0	716	0.485	0
619	0.186		7.4002	717	0.438	0
620	0.204		5.3218	718	0.415	0
621	0.205		5.228	719	0.408	0
622	0.206		5.5798	720	0.477	0
623	0.284		5.0058	721	0.509	0
624	0.243		0.4208	722	0.536	0
625	0.193		7.2555	723	0.52	
626	0.379		3.7813	724	0.537	0
627	0.36		0	725	0.537	0
628	0.235		0.03	726	0.578	0
629	0.23		6.1546	727	0.599	0
630	0.421		2.7378	728	0.587	0
631	0.305		0	729	0.615	0
632	0.182		0	730	0.628	0
633	0.181		0.8506	731	0.629	0
634	0.17		4.6398	732	0.625	0
635	0.179		0.0792	733	0.628	0
636	0.162		0	734	0.625	0
637	0.167		0.6125	735	0.639	0
638	0.157		2.7008	736	0.638	0
639	0.296		1.1334	737	0.639	0
640	0.249		0	738	0.636	0
641	0.249		0	739	0.681	0
642	0.177		0.3278	740	0.663	0
643	0.17		0	741	0.659	0
644	0.187		0.792	742	0.68	
645	0.224		0.143	743	0.677	0
646	0.254		2.5885	744	0.639	0
647	0.39		5.7223	745	0.557	0
648	0.851	1.205	19.9435	746	0.598	0
649	0.705	1.026	2.639	747	0.639	0
650	0.58	1.078	9.1147	748	0.658	0
651	0.476	1.161	8.9509	749	0.598	0
652	0.698	1.858	19.3408	750	0.54	
653	0.496	1.858	9.2644	751	0.557	0
654	0.612	1.858	10.2769	752	0.557	0
655	1.178	1.313	2.7848	753	0.555	0
656	0.677	2.391	22.8058	754	0.556	0
657	0.542	1.848	0.2911	755	0.511	0
658	0.73	1.238	1.0968	756	0.511	0
659	0.523		0	757	0.529	0
660	0.386		1.2776	758	0.497	0
661	0.546		2.2934	759	0.452	0
662	0.487		4.13	760	0.431	0
663	1.179	1.147	11.1673	761	0.475	0
664	1.763	0.982	1.3948	762	0.491	0
665	1.325	0.752	0	763	0.502	0
666	0.96	1	0.1632	764	0.521	0
667	0.408		0	765	0.477	0
668	0.359		0	766	0.405	0
669	0.16		0	767	0.407	0
670	0.332		0	768	0.375	0
671	0.261		2.2858	769	0.391	0
672	0.279		0	770	0.401	0
673	0.261		2.411	771	0.349	0
674	0.27		0	772	0.349	0
675	0.392		0	773	0.318	0
676	0.353		0	774	0.357	0
677	0.327		0	775	0.368	0
678	0.252		0	776	0.348	0
679	0.266		0	777	0.339	0
680	0.265		0.2856	778	0.349	0
681	0.259		0	779	0.304	0
682	0.331		0	780	0.304	0
683	0.309		0	781	0.298	0
684	0.273		0	782	0.281	0

783	0.267	0	881	0.009	0
784	0.267	0	882	0.009	0.4788
785	0.266	0	883	0.008	0.021
786	0.255	0	884	0.008	0
787	0.264	0	885	0.005	1.1271
788	0.264	0	886	0.003	7.484
789	0.254	0	887	0.006	1.1239
790	0.395	0	888	0.003	1.3912
791	0.419	0	889	0.003	3.7358
792	0.266	0	890	0.003	0
793	0.254	0	891	0.003	1.9928
794	0.203	0	892	0.003	2.2864
795	0.205	0	893	0.016	19.7272
796	0.206	0	894	0.023	0
797	0.209	0	895	0.082	2.155
798	0.215	0	896	0.043	15.19
799	0.264	0	897	0.054	74.81
800	0.254	0	898	2.885	2.874
801	0.297	0	899	1.86	31.029
802	0.297	0	900	0.871	2.476
803	0.299	0	901	0.298	1.445
804	0.325	0	902	0.228	0.4791
805	0.312	0	903	0.139	0.132
806	0.346	0	904	0.108	0
807	0.346	0	905	0.075	0
808	0.344	0	906	0.062	0
809	0.34	0	907	0.033	0
810	0.322	0	908	0.033	0.603
811	0.321	0	909	0.033	0.3834
812	0.326	0	910	0.033	0
813	0.327	0	911	0.031	0
814	0.327	0	912	0.03	0
815	0.327	0	913	0.035	0
816	0.327	0	914	0.032	0
817	0.33	0	915	0.028	0
818	0.332	0	916	0.009	0
819	0.343	0	917	0.007	2.7816
820	0.344	0	918	0.008	4.7549
821	0.344	0	919	0.008	5.5422
822	0.345	1.8538	920	0.028	0.5618
823	0.348	0	921	0.028	0
824	0.423	0	922	0.027	4.0916
825	0.335	0	923	0.031	4.5447
826	0.268	0	924	0.039	0
827	0.252	0	925	0.031	0.018
828	0.229	0	926	0.028	0.252
829	0.208	0	927	0.009	0.3248
830	0.192	0	928	0.01	0
831	0.194	0	929	0.009	0
832	0.19	0	930	0.023	10.3924
833	0.182	3.8246	931	0.024	10.2788
834	0.135	1.2864	932	0.036	2.4608
835	0.344	4.0348	933	0.031	0.488
836	0.354	0	934	0.038	10.2669
837	0.226	0	935	0.032	2.499
838	0.155	5.8587	936	0.039	3.1692
839	0.149	4.8293	937	0.033	3.2358
840	0.162	0.83	938	0.031	0
841	0.132	0	939	0.028	1.5728
842	0.109	3.8154	940	0.024	0
843	0.086	0	941	0.023	0
844	0.089	0	942	0.013	0
845	0.088	0	943	0.01	0
846	0.089	0.1788	944	0.01	0.4848
847	0.087	0	945	0.007	1.0572
848	0.087	1.109	946	0.008	0
849	0.073	0	947	0.01	0
850	0.073	0	948	0.002	0
851	0.081	0	949	0.002	1.1408
852	0.057	0.7722	950	0.002	0.38
853	0.05	0	951	0.002	0.08
854	0.046	0	952	0.002	1.8472
855	0.0461	0	953	0.002	3.3118
856	0.027	0	954	0.002	1.1712
857	0.025	0	955	0.011	8.2813
858	0.023	0	956	0.022	10.0228
859	0.024	0	957	0.05	0
860	0.024	0	958	0.061	0.087
861	0.023	0	959	0.079	2.1397
862	0.023	0	960	0.08	2.0014
863	0.018	0	961	0.068	7.8819
864	0.018	0	962	0.073	3.6954
865	0.018	0	963	0.072	6.5904
866	0.016	0	964	0.07	0
867	0.018	0	965	0.071	5.2998
868	0.011	0	966	0.113	7.4491
869	0.018	0	967	0.113	10.3794
870	0.011	0.3178	968	0.243	1.773
871	0.011	0.2016	969	0.443	38.7654
872	0.011	0	970	0.896	1.422
873	0.011	0.5622	971	0.872	1.054
874	0.011	7.4105	972	0.487	2.1552
875	0.01	0	973	0.404	1.004
876	0.019	0	974	0.215	1.212
877	0.019	0	975	0.221	1.14
878	0.019	0	976	0.35	2.931
879	0.008	0	977	1.978	2.325
880	0.009	0	978	0.787	1.524
				4.88	

979	0.433	1.55	11 8214	1077	0.677	0.85	0.366
980	1.674	1.072	1 2498	1078	0.819	0.84	5.2728
981	1.023		0.685	1 581	1079	1.174	0.468
982	0.519			2 523	1080	1.269	0.608
983	0.726			2 4998	1081	1.922	0.774
984	0.498			3 603	1082	1.548	0.717
985	0.373		1 561	18 4652	1083	1.279	0.8978
986	0.392		1.346	5.0716	1084	1.109	0
987	1.481		0.978	0.244	1085	0.984	0.68
988	0.877			1 682	1086	0.935	0
989	0.574			2.071	1087	0.819	0
990	0.293			3 9542	1088	0.866	0
991	0.261			2.2251	1089	0.854	0
992	0.232			0 3539	1090	0.85	0
993	0.208			5 3171	1091	0.846	0
994	0.154			11 5078	1092	0.845	0
995	0.149			2 8539	1093	0.876	0
996	0.165			1.0806	1094	0.873	0
997	0.152			3.3954	1095	0.885	0
998	0.144			0.8231	1096	0.829	0
999	0.21			4 5688	1097	0.885	0.83
1000	0.151		0.351	1.8448	1098	0.857	0
1001	0.151		0.33	0.072	1099	0.922	0.63
1002	0.25		0.325	0	1100	0.809	0
1003	0.177		0.32	0.089	1101	0.839	0.63
1004	0.205		0.32	2 0306	1102	0.588	0.62
1005	0.24	2.03	28 0536	1103	0.557	0.62	0
1006	1.434		4.47	33 8888	1104	0.587	0.62
1007	1.923		3 721	8.386	1105	0.812	0
1008	1.795		2.398	0	1106	0.843	0.99
1009	1.187		1.453	0	1107	1.385	1.248
1010	0.662		0.91	0	1108	2.538	1.07
1011	0.456		0.82	0.234	1109	1.398	0.876
1012	0.391		0.94	7 952	1110	1.304	0.859
1013	0.449		0.79	0.9636	1111	1.288	0.765
1014	0.553		0.82	2 933	1112	1.343	0.783
1015	0.717		0.51	0.268	1113	1.275	0.72
1016	0.654		0.45	0	1114	1.237	0.666
1017	0.662		0.42	1.5444	1115	1.181	0.632
1018	0.85		0.405	0	1116	1.132	0.612
1019	0.836		1.312	13 4206	1117	1.006	0.601
1020	0.831		1.752	9 7315	1118	0.84	0.594
1021	1.429		1.428	1 9331	1119	0.829	0.59
1022	1.368		1.68	11 9385	1120	0.885	0.581
1023	1.808		10 614	76 5427	1121	0.884	0.58
1024	7.21		14 433	39 6378	1122	0.885	0.58
1025	2.068	10.866	7 9836	1123	0.878	0.57	0
1026	8.324		6 802	4 652	1124	0.839	0.57
1027	4.855		4 577	7 2029	1125	0.71	0.571
1028	4.392		2.75	1.1927	1126	0.739	0.56
1029	3.175		1.847	4.5888	1127	0.648	0.58
1030	2.597		1.215	1.4206	1128	0.829	0.58
1031	2.052		0.856	1.2402	1129	0.826	0.55
1032	1.918		0.672	0	1130	0.624	0.55
1033	1.22		0.586	0	1131	0.54	0.55
1034	1.187		0.548	1.4331	1132	0.511	0.54
1035	0.818		0.53	0	1133	0.528	0.54
1036	0.827		0.53	0	1134	0.583	0.53
1037	0.706		0.53	0	1135	0.586	0.53
1038	0.682		0.54	0	1136	0.583	0.53
1039	0.518		0.54	0	1137	0.578	0.52
1040	0.431		0.55	0	1138	0.559	0.52
1041	0.502		0.55	0	1139	0.583	0.51
1042	0.536		0.58	0.244	1140	0.541	0.51
1043	0.554		0.58	1.5826	1141	0.492	0.50
1044	0.531		0.57	0.037	1142	0.488	0.50
1045	0.662		0.57	0	1143	0.483	0.49
1046	0.609		0.58	0	1144	0.483	0.49
1047	0.682		0.58	0	1145	0.44	0.49
1048	0.859		0.59	0	1146	0.425	0.48
1049	0.85		0.597	0	1147	0.42	0.461
1050	0.669		0.60	0 3932	1148	0.424	0.47
1051	0.558		0.60	0	1149	0.428	0.47
1052	0.552		0.60	0	1150	0.419	0.48
1053	0.702		0.61	0	1151	0.412	0.48
1054	0.755		0.61	0	1152	0.427	0.45
1055	0.698		0.61	0	1153	0.401	0.45
1056	0.517		0.61	0 6344	1154	0.383	0.44
1057	0.698	1.361	10 9379	1155	0.348	0.44	0
1058	3.626		3 118	21 781	1156	0.331	0.43
1059	2.758		2 515	0.082	1157	0.33	0.434
1060	2.411		1.748	0	1158	0.304	0.42
1061	1.354		1.225	0	1159	0.297	0.42
1062	1.093		0.931	0	1160	0.305	0.42
1063	0.671		0.78	0	1161	0.285	0.41
1064	0.63		0.707	0	1162	0.275	0.41
1065	0.63		0.672	0	1163	0.235	0.40
1066	1.015	0.658		0	1164	0.223	0.40
1067	0.547		0.65	0	1165	0.201	0.39
1068	0.648		0.65	0	1166	0.195	0.39
1069	0.833		0.65	0	1167	0.193	0.38
1070	0.877		0.65	0.773	1168	0.169	0.38
1071	0.913		0.65	1 0816	1169	0.177	0.38
1072	0.951		0.65	0	1170	0.178	0.37
1073	0.993		0.65	0	1171	0.198	0.37
1074	0.827		0.65	0	1172	0.198	0.36
1075	0.745		0.65	0	1173	0.193	0.36
1076	0.682		0.65	0	1174	0.177	0.35

1175	0.177	0.35	0	1273	0.008	0.14	0
1176	0.176	0.35	0	1274	0.007	0.13	0.045
1177	0.157	0.34	0	1275	0.007	0.13	0.0792
1178	0.156	0.34	0	1276	0.007	0.13	0
1179	0.154	0.33	0	1277	0.006	0.11	0.0935
1180	0.158	0.33	0	1278	0.006	0.13	0.012
1181	0.161	0.33	0	1279	0.006	0.13	0.9029
1182	0.189	0.32	0	1280	0.006	0.13	0.7132
1183	0.177	0.32	0	1281	0.006	0.13	4.4284
1184	0.151	0.32	0	1282	0.006	0.15	4.945
1185	0.145	0.31	0	1283	0.006	0.16	7.3001
1186	0.159	0.31	0	1284	0.007	0.16	1.517
1187	0.234	0.31	2.1214	1285	0.007	0.14	1.1978
1188	0.233	0.30	0	1286	0.018	0.14	2.1428
1189	0.219	0.30	0	1287	0.021	0.19	0.6955
1190	0.215	0.31	5.3916	1288	0.019	0.19	3.9826
1191	0.228	0.41	16.418	1289	0.016	0.17	0
1192	0.75	0.386	1.6074	1290	0.019	0.15	0.6986
1193	0.566	0.34	0	1291	0.011	0.13	0
1194	0.332	0.31	0	1292	0.011	0.13	0.09
1195	0.295	0.30	0	1293	0.011	0.12	0
1196	0.209	0.29	0	1294	0.006	0.12	0.1586
1197	0.293	0.30	3.6088	1295	0.005	0.12	0
1198	0.302	0.30	2.9924	1296	0.001	0.12	0.9498
1199	0.285	0.29	0.6834	1297	0.003	0.12	0.7386
1200	0.195	0.28	0	1298	0.003	0.12	0
1201	0.211	0.27	0	1299	0.003	0.11	0.5358
1202	0.157	0.3	4.8548	1300	0.007	0.13	4.9336
1203	0.144	0.28	1.9968	1301	0.005	0.14	2.8808
1204	0.137	0.40	11.9948	1302	0.005	0.21	10.3564
1205	0.134	0.41	5.13	1303	0.006	0.18	1.5758
1206	0.157	0.35	0	1304	0.004	0.16	2.5858
1207	0.143	0.31	0	1305	0.005	0.14	2.0481
1208	0.145	0.28	0	1306	0.005	0.12	0.8113
1209	0.137	0.27	0	1307	0.005	0.12	1.0272
1210	0.119	0.28	0	1308	0.004	0.11	0
1211	0.111	0.26	0	1309	0.004	0.11	0
1212	0.109	0.25	0	1310	0.004	0.12	2.4511
1213	0.097	0.25	0	1311	0.003	0.12	0
1214	0.085	0.25	0	1312	0.002	0.12	0.135
1215	0.084	0.25	0	1313	0.002	0.11	0.238
1216	0.07	0.248	0	1314	0.001	0.12	2.9078
1217	0.093	0.26	5.0074	1315	0.001	0.12	0.7668
1218	0.085	0.25	0	1316	0.001	0.12	1.9049
1219	0.081	0.25	0	1317	0.001	0.12	0
1220	0.081	0.24	0	1318	0.001	0.11	0.2449
1221	0.089	0.24	0	1319	0.001	0.17	5.9251
1222	0.088	0.24	2.1189	1320	0.001	0.17	3.0392
1223	0.087	0.23	0	1321	0.001	0.15	0
1224	0.087	0.23	0	1322	0.001	0.13	0
1225	0.077	0.23	0	1323	0.001	0.12	0.6698
1226	0.072	0.22	0	1324	0.001	0.11	0.136
1227	0.067	0.22	0	1325	0.002	0.15	5.8578
1228	0.066	0.22	0	1326	0.003	0.21	7.8482
1229	0.065	0.21	0	1327	0.068	0.18	0.057
1230	0.056	0.21	0	1328	0.05	0.152	0.1144
1231	0.058	0.21	0	1329	0.043	0.13	0.09
1232	0.055	0.21	0	1330	0.037	0.12	0.8236
1233	0.058	0.21	0	1331	0.025	0.11	0.225
1234	0.053	0.20	0.38	1332	0.017	0.11	0.1848
1235	0.047	0.20	0	1333	0.011	0.11	0
1236	0.047	0.20	0	1334	0.01	0.112	0
1237	0.048	0.20	0	1335	0.01	0.112	1.0372
1238	0.048	0.19	0	1336	0.01	0.122	2.8286
1239	0.046	0.19	0	1337	0.007	0.12	0.187
1240	0.041	0.19	0	1338	0.005	0.11	0
1241	0.041	0.19	0	1339	0.017	0.11	0
1242	0.031	0.18	0	1340	0.034	0.11	1.5339
1243	0.03	0.162	0	1341	0.038	0.11	0
1244	0.031	0.18	0	1342	0.054	0.11	0
1245	0.028	0.18	0	1343	0.052	0.12	3.7214
1246	0.024	0.18	0	1344	0.051	0.15	5.8535
1247	0.024	0.17	0	1345	0.276	0.18	5.776
1248	0.022	0.17	0	1346	0.243	0.27	10.414
1249	0.022	0.17	0	1347	0.238	0.26	4.0886
1250	0.022	0.17	0	1348	2.268	0.708	25.2372
1251	0.022	0.17	1.2441	1349	1.158	0.645	5.7036
1252	0.019	0.18	0	1350	1.877	0.641	9.4365
1253	0.018	0.16	0	1351	0.802	0.45	0
1254	0.018	0.16	0.0624	1352	0.573	0.30	0.6598
1255	0.017	0.16	0	1353	0.121	0.58	14.1504
1256	0.017	0.17	5.7158	1354	1.424	0.521	5.1642
1257	0.019	0.16	0.0938	1355	1.021	0.308	18.9491
1258	0.024	0.16	1.0358	1356	1.183	1.186	13.8966
1259	0.025	0.15	0.712	1357	0.777	1.319	13.0849
1260	0.025	0.20	11.0181	1358	2.228	0.923	0.9274
1261	0.023	0.19	0	1359	1.374	0.804	7.95
1262	0.019	0.17	0.8092	1360	1.048	0.749	7.3772
1263	0.032	0.16	0	1361	1.03	1.983	27.1878
1264	0.029	0.15	0	1362	2.037	4.921	45.8293
1265	0.026	0.15	0	1363	20.983	13.886	68.1097
1266	0.022	0.15	0	1364	20.983	11.671	12.5292
1267	0.023	0.14	0	1365	4.465	7.215	0
1268	0.021	0.14	0.1178	1366	2.733	3.99	0
1269	0.019	0.14	0	1367	1.577	2.119	0
1270	0.009	0.14	3.0222	1368	0.822	1.139	0
1271	0.011	0.14	0.3446	1369	0.714	0.851	2.44
1272	0.011	0.14	0.6958	1370	0.723	3.131	22.7316

1371	1.895	3.307	8.7791
1372	0.966	2.249	0
1373	0.523	1.371	0
1374	0.419	0.83	0.5612
1375	0.325	0.55	0.3094
1376	0.39	0.415	0.1323
1377	0.432	0.351	2.4812
1378	0.341	0.31	0.3898
1379	0.279	0.32	0
1380	0.342	0.32	1.126
1381	0.209	0.33	0
1382	0.339	0.33	0.217
1383	0.367	0.34	0.5084
1384	0.41	0.348	0.117
1385	0.391	0.35	0
1386	0.461	0.36	0
1387	0.456	0.38	1.668
1388	0.397	0.37	0
1389	0.377	0.38	0
1390	0.378	0.38	0
1391	0.378	0.39	0
1392	0.391	0.39	0
1393	0.432	0.40	0.829
1394	0.463	0.40	1.7444
1395	0.728	0.66	5.9084
1396	1.099	1.38	11.415
1397	1.307	1.358	5.2132
1398	1.17	1.79	10.9822
1399	5.203	3.682	24.5879
1400	3.183	3.154	6.1485
1401	2.274	2.105	0
1402	0.593	1.345	0.3332
1403	1.208	1.011	4.0914
1404	1.118	0.761	1.4538
1405	0.85	0.618	0
1406	0.645	0.54	0
1407	0.647	0.50	0
1408	0.591	0.58	3.8698
1409	1.434	1.433	11.5003
1410	1.604	1.234	1.288
1411	1.363	0.938	0
1412	1.048	0.734	0
1413	0.601	0.611	0
1414	0.723	0.58	0
1415	0.826	0.53	0
1416	0.905	0.52	0.4988
1417	0.964	0.511	0.8477
1418	1.016	0.52	1.0186
1419	1.013	0.521	1.8854
1420	0.851	0.611	4.056
1421	1.091	0.602	0.5693
1422	0.97	0.578	0
1423	0.552	0.75	5.3856
1424	1.323	1.75	14.9358
1425	1.592	1.478	0.2632
1426	1.419	1.101	0.586
1427	1.335	1.495	10.3534
1428	1.766	1.219	8.3856
1429	2.018	2.493	14.8405
1430	2.538	1.927	1.9768

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